## PLAN APPROVAL APPLICATION



Philadelphia Energy Solutions Refining and Marketing, LLC. (PES).

Supplement to Plan Approval Application Package for Heater Firing Rate Increase

August 31, 2012 (Submittal) September 6, 2012 (Completeness Determination) September 2013 (Supplement)

**Environmental Resources Management** 

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PLA.	N APP	ROVAL A	APPLICATION	1
1.0	INTI	RODUCTI	ION & OVERALL SUMMARY	1
	1.1	SINGLE	E SOURCE DETERMINATION	2
	1.2	SETTLE	EMENT WITH CLEAN AIR COUNCIL	2
	1.3	PROPC	OSED PERMITTING	3
2.0	PLA	N APPRO	OVAL OVERVIEW	5
	2.1	TARGE	T HEATERS	5
	2.2	SHUTD	OOWN SOURCES AT MARCUS HOOK REFINERY	6
	2.3	UPSTR	EAM/DOWNSTREAM ANCILLARY UNITS	6
	2.4	SCHED	ULE	8
3.0	PLA	N APPRO	OVAL EMISSIONS	11
	3.1	TARGE	T HEATERS	12
		3.1.1	Primary Pollutants VOC, PM/PM <sub>10</sub> /PM <sub>2.5</sub> , CO, and Lead	12
		3.1.2	<i>J</i>	13
		3.1.3	<i>J</i>	13
		3.1.4	Primary Pollutant $NO_x$	13
	3.2	UPSTR	EAM/DOWNSTREAM ANCILLARY UNITS	15
		3.2.1	Ancillary Process Heaters and Boilers	16
		3.2.2	Upstream/Downstream Ancillary Units (excluding Heaters and	<i>a</i> -
		2 2 2	Boilers)	17
		3.2.3 3.2.4	Unmodified Storage Tanks	18 18
		3.2.4	Unaffected Upstream/Downstream Ancillary Units	10
	3.3	TOTAL	PLAN APPROVAL EMISSION CHANGES	19
4.0	REG	ULATOR	Y OVERVIEW	21
	<b>4.1</b>	PREVE	NTION OF SIGNIFICANT DETERIORATION ANALYSIS	21
		4.1.1	Plan Approval Emissions Analysis (Step 1)	22
		4.1.2	PSD Emissions Netting Analysis (Step 2)	22
	4.2	NON-A	TTAINMENT NEW SOURCE REVIEW ANALYSIS	24

5.0	BAC	T ANALY	SIS FOR CO CONTROL	28
	5.1	METH	ODOLOGY	28
	5.2	IDENT	IFY ALL CONTROL TECHNOLOGIES	30
	5.3	ELIMI	NATE TECHNICALLY INFEASIBLE OPTIONS	31
	<b>5.4</b>		REMAINING CONTROL TECHNOLOGIES BY CONTROL TIVENESS	31
	<b>5.</b> 5		IATE MOST EFFECTIVE CONTROLS BASED ON ECONOMI GY, AND ENVIRONMENTAL IMPACTS	IC, 32
	5.6	SELEC	TION OF BACT	33
6.0	APP	LICABLE	ESTANDARDS	34
	6.1	PADEI	P REGULATIONS - BEST AVAILABLE TECHNOLOGY ANAI	LYSIS34
		6.1.1	$NO_x$ Controls	35
		6.1.2	CO Controls	37
		6.1.3	$PM/PM_{10}/PM_{2.5}$ Controls	37
		6.1.4	SO <sub>2</sub> Controls	38
		6.1.5	VOC Controls	38
	6.2	AIR M	ANAGEMENT SERVICES REGULATIONS	39
	6.3	FEDER	AL REGULATIONS	40
		6.3.1	New Source Performance Standards (NSPS)	40
		6.3.2	Maximum Achievable Control Technology (MACT)	40
7.0	PRC	POSED I	PLAN APPROVAL CONDITIONS	41
List	of Tab	les		
	Table	2-1	Proposed Firing Limits for Target Heaters	
	Table	2 3-1	Future Projected Actual Emissions Increases from Target He	aters
	Table	2 3-2	Ancillary Process Heaters	
	Table	2 3-3	Future Projected Actual Emissions from Ancillary Process Hand Boilers	leaters

Table 3-4	Future Projected Actual Emissions from Upstream/Downstream Ancillary Units
Table 3-5	Total Heater Firing Rate Increase Plan Approval Emission Increases
Table 4-1	PSD Emissions Analysis (Step 1)
Table 4-2	PSD Contemporaneous Netting Analysis (Step 2)
Table 4-3	$NA$ - $NSR$ $Netting$ $Analysis$ $for$ $VOC$ $and$ $NO_x$ $Emissions$ $(5-year)$
Table 4-4	$NA$ - $NSR$ $Netting$ $Analysis$ for $VOC$ and $NO_x$ $Emissions$ (10- $year$ )
Table 4-5	$NA$ - $NSR$ $Analysis$ for $SO_2$ , $NO_x$ , and $PM_{2.5}$ $Emissions$ ( $Step~1$ )
Table 4-6	NA-NSR Netting Analysis for $PM_{2.5}$ and $NO_x$ as $PM_{2.5}$ Precursor (Step 2)
Table 6-1	Target Heaters Construction Dates
Table 6-2	$NO_x$ BAT Determinations
Table 7-1	Revised Firing Rate Limits for Unmodified Target Heaters
Table 7-2	Revised Firing Rate Limits for Modified Target Heaters
Table 7-3	Proposed Emissions Limits for Unmodified Target Heaters (Based on Projected Actual Emissions)
Table 7-4	Proposed Emissions Limits for Modified Target Heaters (Based on Projected Actual Emissions)
List of Figures	
Figure 2-1	Girard Point Processing Area Process Flow Diagram
Figure 2-2	Point Breeze Processing Area Process Flow Diagram
List of Attachments	
Attachment A	Reasonably Achievable Control Technology (RACT) analysis
Attachment B	AMS Plan Approval Application Forms

Attachment C Compliance Review History

Attachment D Emission Calculations

Attachment E Process Flow Diagrams/Site Location Map

Attachment F CO Dispersion Modeling

Attachment G RBLC and BAAQMD BACT Search Results

Attachment H CO Cost Effectiveness Analysis

Attachment I BAT Cost Effectiveness Analysis

#### 1.0 INTRODUCTION & OVERALL SUMMARY

Philadelphia Energy Solutions Refining and Marketing, LLC (PES) owns and operates a petroleum refinery in Philadelphia, Pennsylvania. The Philadelphia Refinery (Refinery) consists of multiple processing areas, the Girard Point Processing Area (GP) near the Platt Bridge, the Point Breeze Processing Area (PB) located near the Passyunk Avenue Bridge, and permanently closed crude refining operations at Marcus Hook. The Refinery is made up of a number of processing units that are employed in the overall process of converting crude petroleum and other hydrocarbon feed stocks into finished hydrocarbon products and petrochemicals. Products include gasoline, home heating oil, diesel fuel and others.

PES is submitting this supplement to the Plan Approval application<sup>1</sup> to request approval for increase in the firing rate of seven target process heaters at the Refinery to facilitate a shift in production as a part of a strategic plan to shift crude oil refining operations to GP and PB and away from Marcus Hook. This supplement is provided in response to comments and questions from reviewing agencies. Since some of the comments were about clarity in the application, some content has been expanded and reorganized. As such, this supplement is provided in the form of a complete application package.

This plan approval seeks to increase the firing limitations of the seven target process heaters. This will help in shifting production from the shutdown Marcus Hook operations. In fact, this plan approval includes application of emission netting credits (emission reductions) that result in overall decreases for certain pollutants from the combined Philadelphia and Marcus Hook operations. Specifically, following this plan approval, there will be an **estimated net decrease** in emissions of 55.9 tons per year (TPY) of nitrogen oxides  $(NO_x)^2$ .

All Refinery processing units rely on the combustion of refinery fuel gas (consisting of a combination of refinery by-product gas and natural gas) in direct-fired process heaters and steam-producing boilers to provide the energy needed to drive hydrocarbon conversions and product

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Sunoco, Inc. originally submitted this Plan Approval application on August 31, 2012. PES took over ownership of the Refinery on September 8, 2012. PES submitted an updated Plan Approval application that included corrected data and other revisions requested by Philadelphia Air Management Services (AMS) on November 13, 2012. PES submits this further revision to the Plan Approval application in response to further comments from USEPA, AMS and Pennsylvania DEP.

 $<sup>^{2}</sup>$  NO<sub>x</sub> (TPY): increase = 140.1, credits applied = 195.9, overall reduction: 140.1 - 195.9 = 55.9.

separations. By this application, the Refinery is proposing to increase the firing limits on seven of its Philadelphia process heaters. This will allow the Refinery to process, on average, more crude into finished products, subject to other permit restrictions on various units. Specifically, this change will enable the Refinery to offset reductions of intermediate streams feeding Refinery processes that were previously provided to the Refinery from the Marcus Hook operations.

This application lays out the emissions analyses and regulatory impacts from the permit limit changes requested for the seven target heaters, including impacts on ancillary operations at the Refinery.

## 1.1 SINGLE SOURCE DETERMINATION

On August 7, 2012, the Pennsylvania Department of Environmental Protection (PADEP) issued an amendment to the Title V permit for the Marcus Hook Refinery, and Philadelphia Air Management Services (AMS) issued an administrative order for the Title V permit for the Philadelphia Refinery recognizing that the two locations were a single source, for the reasons set forth therein. Sunoco's retirement on August 15, 2012, of the permits for operating crude refining sources at the former Marcus Hook Refinery implemented the plan to shift that production to the Philadelphia Refinery as a part of the shutdown of crude refining operations at the Marcus Hook Refinery.

#### 1.2 SETTLEMENT WITH CLEAN AIR COUNCIL

On April 19, 2013, PES and the Clean Air Council (CAC) reached a settlement resolving CAC's appeal of the PADEP decision allowing emission reductions from the shut-down of the former Sunoco Inc. Marcus Hook Refinery to be credited to the Philadelphia Refining Complex, which PES obtained from Sunoco Inc. in September 2012.

As part of this settlement, PES agreed voluntarily to install ultra-low  $NO_x$  burners (ULNB) on the Unit 231-B101 Heater and Unit 865-11H1 Heater at the Refinery to further reduce emissions beyond the cuts achieved by the shut-down of the Marcus Hook Refinery. These ULNB are to be installed only upon approval of higher firing rates as discussed in this plan approval application.

## 1.3 PROPOSED PERMITTING

Other than the installation of ULNBs on Unit 231-B101 and Unit 865-11H1, there are no physical changes to the seven target heaters as a result of this project to increase firing rates. Moreover, the firing rates on the target heaters are limited by existing Reasonably Achievable Control Technology (RACT) requirements. To accommodate the increase in firing rates on the target heaters, PES is requesting revisions to the firing rate limits established as a part of the RACT permit (See Attachment A).

This Plan Approval application package includes the following:

- Detailed plan approval descriptions (Section 2.0);
- Air emission changes associated with the plan approval (Section 3.0);
- New Source Review (NSR) applicability analysis (Section 4.0);
- Best Available Control Technology (BACT) analysis for CO control (Section 5.0);
- Other Federal and State applicability analysis (Section 6.0); and
- Proposed permit conditions (Section 7.0).

Attachments to this Plan Approval application package include the following:

- Reasonably Achievable Control Technology (RACT) analysis (Attachment A);
- AMS Plan Approval Application forms (Attachment B);
- Compliance Review History (Attachment C);
- Emission Calculations (Attachment D);
- Process Flow Diagrams/Site Location Map (Attachment E);
- CO Dispersion Modeling (Attachment F);
- RBLC and BAAQMD BACT Search Results (Attachment G);
- CO Cost Effectiveness Analysis (Attachment H); and

BAT Cost Effectiveness Analysis (Attachment I).

#### 2.0 PLAN APPROVAL OVERVIEW

PES submits this plan approval application in order to allow the Philadelphia Refinery to accommodate increased production. It is necessary to increase the firing limitations of the seven target process heaters to enable an overall production increase and thus offset decreases in production from Marcus Hook operations.

The changes to the target heaters and the effects on ancillary Refinery sources are discussed in the sections that follow.

#### 2.1 TARGET HEATERS

Other than the installation of ULNBs on Unit 231-B101 and Unit 865-11H1, this project will not involve any physical changes to the target heaters. PES is seeking to remove the hourly average firing limits (million British thermal units per hour [MMBtu/hr]) of the target heaters and replace them with annual average firing limits (MMBtu/year). The new annual average firing rate limits are based on increases in the hourly average firing limits. The existing hourly firing limits and proposed annual firing limits for the heaters are shown in Table 2-1 below.

Table 2-1 Proposed Firing Limits for Target Heaters

Process Unit	Heater	Existing Hourly Firing Limit (MMBtu/hr) <sup>1</sup>	Proposed Annual Firing Limit (MMBtu/year) <sup>2</sup>
GP Unit 231 HDS	B101 Feed Heater	91.0	856,000
PB Unit 865 HDS	11H1 Feed Heater	72.2	699,000
PB Unit 865 HDS	11H2 Reboiler Heater	49.9	500,000
PB Unit 210 Crude	H101 Crude Heater	183.0	1,643,000
PB Unit 210 Crude	H201 Crude Heater	242.0	2,172,000
PB Unit 866 HDS	12H1 Feed Heater	43.0	456,000
PB Unit 868 FCCU	8H101 Recycle Heater	49.5	480,000

<sup>&</sup>lt;sup>1</sup> Compliance determined on a daily average basis.

<sup>&</sup>lt;sup>2</sup> Compliance determined on a rolling 365-day average basis.

#### 2.2 SHUTDOWN SOURCES AT MARCUS HOOK REFINERY

Sunoco's retirement on August 15, 2012, of the permits for operating crude refining sources at the former Marcus Hook Refinery was contemporaneous with a filing by the Sunoco Philadelphia Refinery<sup>3</sup> for emission reduction credits (ERCs) for the shutdown units listed below.

The shutdown sources at the Marcus Hook Refinery include4:

- Unit 12-3 Crude Heater H-3006;
- Unit 17-2A H-01, H-02, H-03 Heater;
- Unit 12-3 Crude Desulf Heater;
- Unit 15-1 Crude Heater;
- Unit 17-2A H-04 Heater; and
- Marcus Hook Cooling Towers including the 10 Plant A and B, 12 Plant North and South, 17-1A, 17-2, 17-2A and LSG towers.

The ERCs generated by the shutdown units listed above are included as contemporaneous emissions reductions. See Section 4.2 for details on the contemporaneous emissions analysis.

#### 2.3 UPSTREAM/DOWNSTREAM ANCILLARY UNITS

The annual firing rate limits sought for the target heaters are expected to allow for increased utilization of upstream/downstream ancillary units relative to the 2010-2011 baseline period.

As discussed in Section 3, the emissions increases associated with the upstream/downstream ancillary units are estimated based on potential incremental increase in crude throughput in the future. PES has estimated the future potential incremental increase in crude throughput at the

<sup>&</sup>lt;sup>3</sup> The Sunoco Philadelphia Refinery is now owned and operated by Philadelphia Energy Solutions Refining and Marketing, LLC (PES).

The sources shutdown listed here do not include shutdown sources listed in Consent Decree No. 05-02866 (Fourth Amendment, dated August 17, 2012). The sources listed in the Consent Decree are subject to specific requirements.

Philadelphia Refinery that is expected as a result of this plan approval and the shutdown of the Marcus Hook Refinery.

Figures 2-1 and 2-2 at the end of this section show the overall process flow diagrams for the Girard Point and Point Breeze Processing Areas.

The Refinery is designed such that process units can run on a combination of feedstocks – those produced on site through distillation and other Refinery units – as well as imported feedstocks. Feedstocks are imported from a number of outside sources, which included, prior to shutdown of operating units, the Marcus Hook Refinery. The types and amounts of imported feedstocks vary based on a number of factors, including economic drivers and overall product demand.

This plan approval will enable upstream and downstream ancillary units to operate with a greater portion of their feeds from other materials processed at the Refinery, thus offsetting feed materials previously available from the Marcus Hook operations. Prior to shutdown of operating units at Marcus Hook, the typical imports of Marcus Hook produced components to Philadelphia operations included the following:

- Butanes Marcus Hook provided about 1 thousand barrels per day (MBPD) of Butane/Butylene mix as incremental feed to the Alkylation units (Units 433 and 869);
- Naphtha Marcus Hook provided about 7 to 12 MBPD of naphtha as incremental feed to the Reformer units (Units 860 and 1332) to make hydrogen and reformate. The volume depended on crude mix/naphtha content.
- Light Cycle Oil (LCO) Marcus Hook provided about 10 MBPD of LCO as feed to Hydrodesulfurization units (Units 231, 866, and 859) to make ultra-low sulfur diesel.
- Benzene Marcus Hook sent all of its benzene production (approximately 3 to 4 MBPD) as feed to the Cumene unit to make cumene.

On a less frequent basis, Marcus Hook would also send untreated cat gasoline to the Philadelphia Refinery for processing through the Low Sulfur Gasoline unit to reduce the sulfur content.

## 2.4 SCHEDULE

PES seeks to implement this plan approval as soon as possible. Since this plan approval involves no physical modifications to five of the target heaters at the Refinery, PES intends to implement those firing rate increases immediately upon plan approval issuance. For the Unit 231-B101 Heater and Unit 865-11H1 Heater, PES will not implement the firing rate increases until the ultra-low  $NO_x$  burners have been installed (per the CAC settlement PES plans to install the burners within 18 months of plan approval issuance).

Process Flow Diagram Philadelphia Refinery Girard Point C3 PB 862 C4 to C2 / C3 431 Unit C3 / C4 Preprop Deprop Cumene 1733 C4 / C5 Debut Winter Cumene C5 Depent C4 / C5 Prefact 1332 Benz, Conc. 1732 LT Naphtha 1332 Reformer UDEX Premium HDS Crude Hvy Naphtha TX Gas Regular HVY Reformate Blending Prefract Btms 137 LT Furnace Oil to 870 LSD / #2 ATM F.O. Crude Stills #2 F.O 慧 LSD Jet / AV F.O 231 1 Kero HVY to 859 & 866 HVY Cat HDS Furnace Oil NC4 / C5 to 859 Naphtha 433 LSD Stock LT Cat Naphtha SHU ATM Gas Oil 8 431 DEP Alkylate Propane (down) 433 1232 PP Alky LT VGO 137 1232 HVY VGO  $^{\circ}$ VAC FCC 431 331 Slumy Oil DIB C4 C4 ISOM 137 N/I C4 IC4 #6 Fuel Oil VTB / Resid PB 210C PB PB

Figure 2-1 Girard Point Processing Area Process Flow Diagram

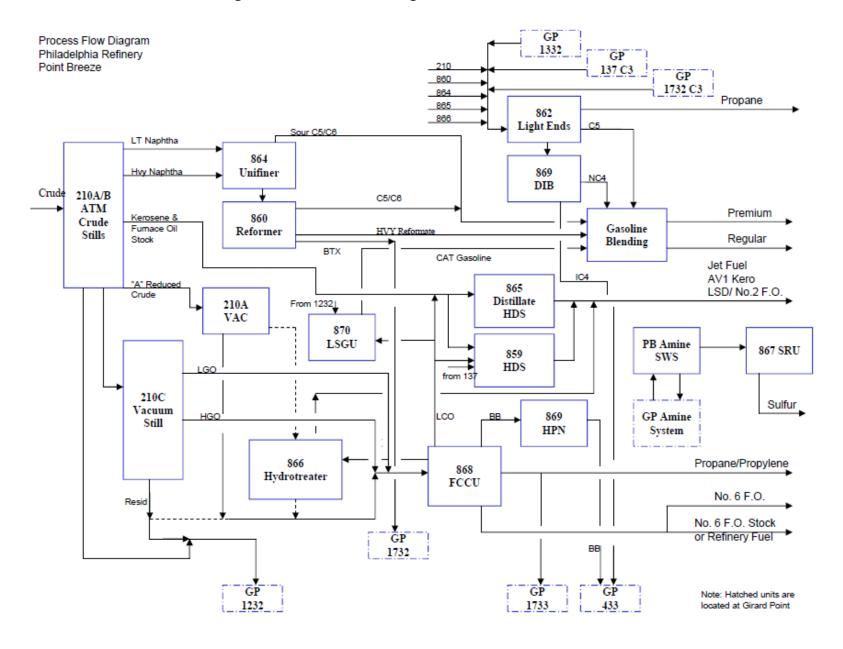
ERM

869 HPN

869 DIB

Note: Hatched units are located at Point Breeze

Figure 2-2 Point Breeze Processing Area Process Flow Diagram



#### PLAN APPROVAL EMISSIONS

3.0

In this plan approval application, the emissions from the target heaters and upstream/downstream ancillary units were calculated using the methodology described below.

Because this project will not require any changes beyond the installation of ULNBs to the target heaters or any other upstream/downstream ancillary units at the Refinery, the emissions changes associated with the target heaters are attributed to the incremental changes in firing rates from historic operation during a defined baseline period to rates projected for the future. Similarly, the emissions increases associated with the ancillary units are attributed to potential incremental increase in crude throughput in the future as compared to the baseline period. As referenced earlier, the baseline period is January 2010 through December 2011.

The emissions changes from both the target heaters and ancillary units are calculated through a step-wise process. Initially, the emissions changes are calculated as the difference between the baseline actual emissions (BAE) and the future projected actual emissions (PAE). As per 25 Pa Code \$127.203a(a)(4)(i) and 40 CFR §52.21(b)(48), BAE were estimated as the highest annual average "during a consecutive 24-month period selected by the owner or the operator within the 5-year period immediately prior to the date a complete plan approval application is received by the Department". Similarly, the projected actual emissions were estimated as the maximum emissions that the plan approval sources are projected to emit "in any one of the 5 years (12-month period) following the date the unit resumes regular operation after the project".

In addition, as per 25 Pa Code §127.203a(5)(i)(C), 40 CFR 52.21(b)(41)(c), and EPA guidance, the Refinery calculated and excluded any increase in emissions from sources affected by this plan approval that could have been accommodated in the 24-month period representing the baseline period, and that are unrelated to the plan approval<sup>5</sup>.

Table 3-5 shown at the end of this section shows the Total Heater Firing Rate Increase Plan Approval emission increases. Detailed emissions

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USEPA, 2010. Letter from Gregg M. Worley, Chief- Air Permits Section, USEPA Region IV to Mark Robinson, Georgia Pacific Wood Products LLC, re: PSD Emissions Calculation and Demand Growth; 18 March 2010. EPA concurred with Georgia Pacific that the "highest demonstrated average monthly operating level during the baseline period" could be used as an approximation for the level the unit could have accommodated during the baseline period.

calculations for all target heaters and upstream/downstream ancillary units can be found in Attachment D.

## 3.1 TARGET HEATERS

To calculate the annual emissions (tons per year) from the target heaters, the future annual firing duty must be established. All pollutant emission changes refer to the future projected annual firing rate as compared to the past actual annual firing rate calculated from the actual firing in 2010 and 2011.

Note that the projected annual firing rate (MMBtu/year, annual average) for the heaters is projected to be lower than the projected maximum annual firing based on design capacity, that is, the design MMBtu/hr rate, which is the basis for the RACT analysis in Attachment A. This approach to setting the basis for the annual firing rates reflects the reality of refining operations where operations can vary seasonally and in response to market demand and other factors. In fact, all heaters at the Refinery operate at annual average firing rates lower than their maximum design firing rate.

The annual emission changes in this plan approval application reflect the difference between past actual emissions and future projected actual emissions based on maximum expected annual firing duty.

The sections below discuss the methodology for calculating the target heater emissions for this plan approval for each pollutant. Table 3-1 below shows the future projected actual emissions for each target heater. Consistent with AMS practice of establishing annual emission limits corresponding to PAE values, Section 7 contains proposed permit conditions including annual emission limits (TPY) for the target heaters.

## 3.1.1 Primary Pollutants VOC, PM/PM<sub>10</sub>/PM<sub>2.5</sub>, CO, and Lead

Consistent with historic practices, the Refinery used EPA AP-42 emission factors for volatile organic compounds (VOC), particulate matter (PM), particulate matter less than 10 microns (PM<sub>10</sub>), particulate matter less than 2.5 microns (PM<sub>2.5</sub>), carbon monoxide (CO), and lead for the target heaters. The EPA AP-42 factors are expressed as pounds per million standard cubic feet (lb/MMscf) of natural gas burned as fuel. Based on refinery fuel gas testing data, the Refinery calculated the EPA AP-42 emission factor as pounds per million Btu by dividing the EPA AP-42 lb/MMscf factor by the current higher heating value for refinery fuel gas

for each heater. The future projected emissions are calculated using the future projected annual firing duty and the EPA AP-42 emission factors.

## 3.1.2 Primary Pollutant SO<sub>2</sub>

This plan approval will allow for an increase in firing of certain target heaters; however, it is not expected to have an impact on the amount of sulfur in the refinery fuel gas, which is the only fuel for refinery heaters. Sulfur dioxide (SO<sub>2</sub>) emissions have historically been estimated based on daily averages of the sulfur content in fuel gas; however, the target heaters only became subject to refinery fuel gas sulfur limits required by New Source Performance Standards Subpart J for Petroleum Refineries in 2011. Therefore, for this plan approval, the 2011 actual SO<sub>2</sub> emissions and 2011 actual fired rates for the each target heater were used to derive a heater-specific SO<sub>2</sub> emission factor. The 2011 actual SO<sub>2</sub> emissions rate (lb/MMBtu) varies for each heater because it is calculated as the daily weighted average based on heater firing (MMBtu/hr). The future projected SO<sub>2</sub> emissions were calculated using the future projected annual firing duty and the heater-specific SO<sub>2</sub> emission factor.

## 3.1.3 Primary Pollutant CO<sub>2</sub>e

The Philadelphia Refinery annually reports greenhouse gas (GHG) emissions in the units of carbon dioxide equivalents (CO<sub>2</sub>e) to the EPA as required by the Mandatory Greenhouse Gas Reporting rule codified at 40 CFR Part 98. The GHG emission factors used for this plan approval were derived following the methods described in 40 CFR 98 Subpart C for General Stationary Fuel Combustion Sources, which includes an analysis of the composition of the refinery fuel gas being combusted for each heater. The GHG emission factor for each heater was derived from the emission factors in Subpart C and the higher heating value of the refinery fuel gas being used. The future projected CO<sub>2</sub>e emissions for this plan approval were calculated using the future projected annual firing duty of each heater and the heater-specific CO<sub>2</sub>e emission factor. This method is at least as accurate as the EPA AP-42 emission factor for CO<sub>2</sub> as this factor only reflects the combustion of natural gas.

## 3.1.4 Primary Pollutant $NO_x$

The methodology used to select the  $NO_x$  emission factors for the target heaters is described below. As seen below, because some of the heaters already have RACT permit limits, the Refinery used the  $NO_x$  emission factors used to derive those limits for those heaters as opposed to EPA AP-42 emission factors used in the annual emissions reports to AMS. The Refinery proposes to amend reported Emission Inventories submitted to

AMS for 2010 and 2011, for heaters where the annual emissions used in this analysis are different from the emissions reported earlier. The  $NO_x$  emission factor used for each heater is discussed below:

- For the Unit 231-B101 Heater, the BAE shown in reported Emission Inventories are adjusted to recognize that this heater has an expected NO<sub>x</sub> emission factor of 0.122 lb/MMBtu. Future projected NO<sub>x</sub> emissions for this heater for this plan approval are based on expected NO<sub>x</sub> emission factor 0.03 lb/MMBtu based on the expected installation of ultra-low NO<sub>x</sub> burners and the future projected annual firing duty.
- For the Unit 865-11H1 Heater, the BAE was based on the RACT NO<sub>x</sub> limit of 0.113 lb/MMBtu, which is lower than the EPA AP-42 emission factor used in the reported Emission Inventories, as the baseline emissions could not be greater than an applicable emissions limit. Future projected NO<sub>x</sub> emissions for this heater for this plan approval are based on the expected NO<sub>x</sub> emission factor 0.03 lb/MMBtu based on the expected installation of ultra-low NO<sub>x</sub> burners and the future projected annual firing duty.
- For the Unit 865-11H2 Heater, the use of EPA AP-42 emission factor was specified by AMS for use in the reported Emission Inventories. To be conservative, the Refinery used the same current RACT NO<sub>x</sub> limit for the Unit 865 11H1, which is greater than the EPA AP-42 emission factor, to calculate the BAE for the plan approval. The Refinery proposes to amend the reported Emission Inventories to reflect the higher emission factor of 0.113 lb/MMBtu for this heater. Future projected NO<sub>x</sub> emissions for this heater for this plan approval are based on the RACT emission rate and the future projected annual firing duty.
- For the Unit 210-H101 Heater, the BAE was based on the RACT  $NO_x$  limit of 0.089 lb/MMBtu, which is lower than the EPA AP-42 emission factor used in the reported Emission Inventories, as the baseline emissions could not be greater than an applicable emissions limit. Future projected  $NO_x$  emissions for this heater for this plan approval are based on the RACT emission rate and the future projected annual firing duty.
- For the Unit 210-H201 Heater, the BAE was based on the average of actual CEMS data for the years 2010 and 2011. The future projected NO<sub>x</sub> emission rate is based on the permit limit for the heater of 0.03 lb/MMBtu. Future projected NO<sub>x</sub> emissions for this heater for this plan approval are based on the NO<sub>x</sub> permit limit and the future projected annual firing duty.

• For the Unit 866-12H1 and Unit 868-8H101 Heaters, the BAE and the future projected emissions were established using the same approach as that used for the Unit 865-11H2 Heater.

Table 3-1 Future Projected Actual Emissions Increases from Target Heaters

Target Heater	PM (TPY)	PM <sub>10</sub> (TPY)	PM <sub>2.5</sub> (TPY)	CO (TPY)	VOC (TPY)	NO <sub>x</sub> (TPY)	SO <sub>2</sub> (TPY)	Lead (TPY)	CO <sub>2</sub> e (TPY)
Unit 231-B101	1.4	1.4	1.4	15.9	1.0	0.0	0.4	9.5E-05	22,738
Unit 865-11H1	0.7	0.7	0.7	7.7	0.5	0.0	0.2	4.6E-05	10,978
Unit 865-11H2	0.6	0.6	0.6	6.3	0.4	8.7	0.2	3.8E-05	9,038
Unit 210-H101	0.9	0.9	0.9	10.0	0.7	11.0	0.5	5.9E-05	14,301
Unit 210-H201	2.1	2.1	2.1	23.2	1.5	12.5	0.8	1.4E-04	33,284
Unit 866-12H1	1.1	1.1	1.1	12.0	0.8	16.6	0.3	7.1E-05	17,156
Unit 868-8H101	0.3	0.3	0.3	3.4	0.2	4.9	0.1	2.0E-05	4,924
Total Target Heater Emission Increases <sup>1</sup>	<b>7.</b> 1	7.1	7.1	78.5	5.1	53.8	2.5	4.7E-04	112,420

<sup>&</sup>lt;sup>1</sup> The Refinery calculated the emissions from the target heaters that they were capable of accommodating in the 24-month baseline period and these are accounted for (subtracted from) future projected actual emissions shown in this table. See the Emissions Calculations in Attachment D for details.

## 3.2 UPSTREAM/DOWNSTREAM ANCILLARY UNITS

The increase in the firing rate limits sought for the target heaters is expected to increase utilization of upstream/downstream ancillary units on an annualized basis as compared to that achieved in the baseline period. PES has estimated the future potential incremental increase in crude throughput at the Philadelphia Refinery that is expected as a result of this plan approval. Following this project, PES conservatively estimated a level of crude processing of 346 MBPD. The average actual crude throughput during the 24-month baseline period was 284.4 MBPD, where the highest monthly throughput occurred in June 2010 at 316.5 MBPD. It is noted though that, while the use of crude processing rate provides a means to project emissions from ancillary units, it is a conservative approach and does not capture the potential impacts of changes in crude slate. Most notably, the refinery has achieved a monthly average throughput of 342.7 MBPD in June 2013, while still remaining in compliance with the existing, lower firing rate limits for the seven heaters.

The potential incremental increases in emissions from upstream/downstream ancillary units have been estimated by scaling the

potential incremental increase in crude throughput as compared to past actual crude throughput rates during the baseline period at the Refinery.

The sections below describe the emissions calculations for each type of upstream/downstream ancillary unit affected by this plan approval.

## 3.2.1 Ancillary Process Heaters and Boilers

Future emissions from the ancillary process heaters and boilers are calculated by scaling historical emissions from the ancillary units with the maximum expected crude increase, which is approximately 22%. All boilers at the No. 3 Boilerhouse are expected to increase utilization as a result of this plan approval, as are all of the ancillary heaters listed in Table 3-2 below.

Table 3-2 Ancillary Process Heaters

Ancillary Proc	<b>Ancillary Process Heaters</b>						
Unit 137 F-1 Heater	Unit 860 2H4 Heater						
Unit 137 F-2 Heater	Unit 860 2H5 Heater						
Unit 137 F-3 Heater	Unit 860 2H7 Heater						
Unit 210 13H-1 Heater	Unit 860 2H8 Heater						
Unit 1332 H-400 Heater	Unit 864 PH1 Heater						
Unit 1332 H-401 Heater	Unit 864 PH7 Heater						
Unit 1332 H-601 Heater	Unit 864 PH11 Heater						
Unit 1332 H-602 Heater	Unit 864 PH12 Heater						
Unit 1332 H-1 Heater	Unit 859 1H1 Heater						
Unit 1332 H-2 Heater	Unit 870 H-01 Heater						
Unit 1332 H-3 Heater	Unit 433 H-1 Heater						
Unit 860 2H2 Heater	Unit 1232 B-104 Heater						
Unit 860 2H3 Heater	Unit 870 H-02 Heater						

As discussed in Section 3.0 for the target heaters, the Refinery also excluded emissions increases that the ancillary process heaters and boilers were capable of accommodating in the baseline period and that are thus unrelated to the plan approval. Table 3-3 below shows the future projected actual emissions for the ancillary process heaters and boilers.

Table 3-3 Future Projected Actual Emissions from Ancillary Process Heaters and Boilers

Pollutant	Ancillary Process Heater and Boiler Emissions (TPY)
PM	6.1
$PM_{10}$	6.1
PM <sub>2.5</sub>	6.1
СО	94.2
VOC	6.3
NO <sub>x</sub>	82.1
SO <sub>2</sub>	3.2
Lead	6.1E-04
CO <sub>2</sub> e	138,640

## 3.2.2 Upstream/Downstream Ancillary Units (excluding Heaters and Boilers)

The emissions increases associated with other upstream/downstream ancillary units, except heaters and boilers, were calculated based on a projected increase in crude throughput over the baseline 24-month period. Similar to the ancillary process heaters and boilers, the emissions from other ancillary units were calculated by scaling the potential incremental increase in crude throughput as compared to past actual crude throughput rates during the baseline period at the Refinery. Ancillary units include:

- Point Breeze, Girard Point, and Schuylkill River Tank Farm Wastewater Treatment Plants;
- Girard Point and Point Breeze marine vessel loading;
- Girard Point butane/polypropylene truck loading; and
- Sulfur recovery units.

As discussed in Section 3.0 for the target heaters, the Refinery also excluded emissions increases that the upstream/downstream ancillary units were capable of accommodating in the baseline period and which are unrelated to the plan approval. Table 3-4 below shows the future projected actual emissions for the upstream/downstream ancillary units.

Table 3-4 Future Projected Actual Emissions from Upstream/Downstream Ancillary Units

Pollutant	Upstream/Downstream Ancillary Units Emissions (TPY)
PM	0.03
$\mathrm{PM}_{10}$	0.03
PM <sub>2.5</sub>	0.03
СО	18.9
VOC	11.7
NO <sub>x</sub>	4.2
SO <sub>2</sub>	1.3
Lead	0.0
CO₂e	4,312

## 3.2.3 *Unmodified Storage Tanks*

Typical light hydrocarbon (gasoline) tanks emit 96% of their VOC emissions from breathing losses and only 4% from working losses. However, only the working losses are affected by throughput. Therefore, only the VOC working losses from unmodified storage tanks associated with this plan approval were scaled by the potential incremental increase in overall Refinery crude throughput over the baseline - approximately 22% (0.96 + 0.04 x 1.22 = 1.009).

Note that no credits (emission reductions) are being taken for the cessation of processing Marcus Hook intermediates at the Refinery.

The future projected actual emissions for the unmodified storage tanks are included in the VOC emissions in Table 3-4 above.

## 3.2.4 Unaffected Upstream/Downstream Ancillary Units

The remaining sources at the Refinery are unaffected. That is, it is not appropriate to scale these sources' emissions based on expected changes in facility crude throughput because the emissions from these units are not rate dependent.

Specifically, such unaffected upstream and downstream ancillary units include:

Leak Detection and Repair emissions;

- Cooling tower emissions;
- Flare emissions;
- Sampling system emissions; and
- Reciprocating internal combustion engine emissions.

## 3.3 TOTAL PLAN APPROVAL EMISSION CHANGES

The total future projected actual emission increases from the Heater Firing Rate Increase Plan Approval are summarized in Table 3-5.

Table 3-5 Total Heater Firing Rate Increase Plan Approval Emission Increases

		Pollutant (TPY)										
Source	NO <sub>x</sub>	SO <sub>2</sub>	СО	VOC	PM	PM <sub>10</sub> /PM <sub>2.5</sub>	Sulfuric acid mist	Lead	HAP	CO₂e		
Target Heater Emissions	53.8	2.5	78.5	5.1	7.1	7.1	0	4.7E-04	0	112,420		
Ancillary Process Heaters and Boilers	82.1	3.2	94.2	6.3	6.1	6.1	0	6.1E-04	0	138,640		
Upstream/Downstream Ancillary Units	4.2	1.3	18.9	11.7	0.03	0.03	0	0	0	4,312		
Total Plan Approval Emissions	140.1	7.1	191.6	23.2	13.2	13.2	0.0	1.1E-03	0.0	255,372		

#### 4.0 REGULATORY OVERVIEW

PES must comply with all federal and state requirements applicable to this proposed plan approval. The existing units are subject to standards covered under the NSPS, MACT and state program requirements and will continue to be after the proposed plan approval. The existing facility is a major stationary source of emissions for all criteria pollutants and greenhouse gases; therefore, the plan approval is required to undergo a New Source Review (NSR) analysis. The Philadelphia Refinery is located in an area designated as moderate nonattainment for ozone; however, for NSR analysis, the area is treated as a severe nonattainment area. Additionally, Philadelphia County is designated a PM<sub>2.5</sub> nonattainment area. It is designated as attainment for other criteria pollutants.

PES must evaluate the plan approval for applicability of the nonattainment NSR program for VOC, NO<sub>x</sub>, and PM<sub>2.5</sub> emissions, and applicability of the Prevention of Significant Deterioration (PSD) program for NO<sub>2</sub>, SO<sub>2</sub>, CO, PM, PM<sub>10</sub>, lead, and sulfuric acid mist (SAM). In addition, PES is required to determine if GHG pollutants would be regulated as a part of the plan approval. The following sections provide the detailed regulatory analysis for the plan approval.

## 4.1 PREVENTION OF SIGNIFICANT DETERIORATION ANALYSIS

The PSD regulations (40 CFR 52.21) are federal regulations that apply to new major sources and "major modifications" of existing "major stationary sources" located in attainment or unclassifiable areas for a given pollutant. The PSD regulations are enforced by PADEP in accordance with 25 Pa Code §127.81. The Philadelphia Refinery is a major stationary source, and a modification to the source that would result in a "significant emission increase" and a "significant net emissions increase" would trigger PSD applicability.

The PSD regulations define a major modification in 40 CFR 52.21(b)(3)(i) as any physical change in or change in the method of operation of a major stationary source that would result in a significant emission increase and a significant net emission increase of any pollutant subject to regulation under the Act. The regulation defines threshold levels of annual emission rates that constitute "significant increases" for a variety of pollutants. The PSD emissions analysis is performed as per applicable regulation in 25 Pa

Code §127.81 and 40 CFR §52.21. EPA takes the position that the PSD emissions analysis should be performed in two steps<sup>6</sup>.

## 4.1.1 Plan Approval Emissions Analysis (Step 1)

In Step 1 of the analysis, the emissions increases from all plan approval sources including the target heaters whose rates are increased and the ancillary units are calculated. The emissions calculation methodology was described in the earlier sections. As indicated in the Table 4-1 below, NO<sub>2</sub>, CO, and CO<sub>2</sub>e emissions for the proposed plan approval exceed the PSD threshold; therefore, PES performed a netting analysis over the contemporaneous period for these three pollutants.

Table 4-1 PSD Emissions Analysis (Step 1)

	Pollutant (TPY)									
Emissions	NO <sub>2</sub>	SO <sub>2</sub>	СО	PM	PM <sub>10</sub>	Sulfuric acid mist	Lead	CO₂e		
Heater Firing Rate Increase Plan Approval	140.1	7.1	191.6	13.2	13.2	0.0	1.1E-03	255,372		
PSD Significant Level	40	40	100	25	15	7	0.6	75,000		
PSD Triggered (Before Netting Analysis)	Yes	No	Yes	No	No	No	No	Yes		

The PSD netting analyses for NO<sub>2</sub>, CO, and CO<sub>2</sub>e are discussed in Section 4.1.2. The PSD netting analysis includes other contemporaneous emission increases and decreases at the facility in the past five years.

## 4.1.2 PSD Emissions Netting Analysis (Step 2)

If the emissions from a plan approval exceed the applicable significant emission rate for a PSD regulated pollutant, the facility can choose to net out the emissions increase from the plan approval with other reductions in emissions that have occurred during the contemporaneous emissions period. PSD regulations allow the use of a netting analysis to determine if a "significant net emission increase" will occur as a result of a plan approval. PES has performed the netting analysis consistent with PSD

<sup>&</sup>lt;sup>6</sup> EPA, 2010. Re: Hovensa Gas Turbine Nitrogen Oxides Prevention of Significant Deterioration (PSD) Permit Application – Emission Calculation Clarification; Letter from Stephen Riva, Permitting Chief to Kathleen Antoine, Environmental Director, Hovensa, LLC. March 30, 2010. While PES does not agree that this two-step analysis is compelled by the PSD regulations or the Clean Air Act, PES follows it here.

regulations in 40 CFR §52.21. A six-step procedure is used for determining the net emissions change and is summarized below.

- 1. <u>Emission Increases from the Proposed Plan Approval</u> Determine the emission increases from the proposed plan approval. If increases are significant, proceed; if not, the plan approval is not subject to PSD review.
- 2. <u>Contemporaneous Period</u> Determine the beginning and ending dates of the contemporaneous period as it relates to the proposed plan approval.
- 3. Emissions Increases and Decreases during the Contemporaneous

  Period Determine which emissions units at the facility experienced

  (or will experience, including any proposed decreases resulting from
  the proposed plan approval) a creditable increase or decrease in
  emissions during the contemporaneous period.
- 4. <u>Creditable Emissions Changes</u> Determine which contemporaneous emissions changes are creditable.
- 5. <u>Amount of the Emissions Increase and Decrease</u> Determine, on a pollutant-by-pollutant basis, the amount of each contemporaneous and creditable emissions increase and decrease.
- 6. <u>PSD Review</u> Sum all contemporaneous and creditable increases and decreases with the emissions changes from the proposed plan approval to determine if a significant net emissions increase will occur.

In order to perform a netting analysis, the contemporaneous periods must be determined. The term "contemporaneous period" is defined in the PSD regulations as the period that includes the five (5) years prior to initiating construction on a proposed modification, and the period between the initiation of construction and the initiation of operation of the new or altered equipment. Because this plan approval involves no physical change to any units at the Refinery, the initiation of operation of the Heater Firing Rate Increase Plan Approval will occur immediately upon approval. Therefore, the contemporaneous period for this plan approval runs from 2nd Quarter 2008 through the 3rd Quarter 2013.

Table 4-2 below summarizes the contemporaneous and creditable emissions increases/decreases included in the plan approval PSD netting analysis. Detailed emissions estimates and netting analyses are provided in Attachment D.

Table 4-2 PSD Contemporaneous Netting Analysis (Step 2)

Emissions	NO <sub>2</sub> Emissions (TPY)	CO Emissions (TPY)	CO₂e Emissions (TPY)
Heater Firing Rate Increase Plan Approval	140.1	191.6	255,372
Contemporaneous Increases/Decreases	-320.7	-17.5	-310,956
Total	-180.7	174.1	-55,583
PSD Significance Level	40	100	75,000
PSD Review Required	No	Yes	No

As shown in Table 4-2, the Heater Firing Rate Increase Plan Approval triggers PSD review for CO. Therefore, a full PSD review is required for CO as a result of this plan approval. The PSD review requirement for CO is summarized below:

- Apply Best Available Control Technology (BACT) for regulated pollutants emitted above PSD thresholds for all applicable emissions units (see discussion in Section 5 of this report); and
- Assess the ambient impact of emissions through the use of dispersion modeling (Attachment F).

Also shown in Table 4-2, the Heater Firing Rate Increase Plan Approval does not exceed the PSD significance level for NO<sub>2</sub>; therefore, further PSD review is not required. In addition, the emissions of GHG are less than the applicable threshold; therefore, GHG is not considered a regulated pollutant in this plan approval.

#### 4.2 NON-ATTAINMENT NEW SOURCE REVIEW ANALYSIS

Major sources located in nonattainment areas must evaluate whether a change constitutes a major modification under nonattainment NSR regulations (NA-NSR). The requirements are defined in 25 Pa Code §127.201 through §127.217. For this plan approval, PES evaluated NA-NSR under the revised NSR requirements published in the *Pennsylvania Bulletin* on May 19, 2007. Currently, Philadelphia is designated as a moderate nonattainment area for ozone and nonattainment for PM<sub>2.5</sub>.

Under the revised Pennsylvania NSR regulation, facilities located in the five-county area (including Philadelphia County) are subject to NSR requirements for serious or severe ozone classification. The applicability

threshold under the special permit requirements codified at \$127.203(b) for serious or severe classification is 25 TPY for both VOC and NO<sub>x</sub> emissions. When considering a modification, major sources must determine if either of the following conditions exceed the 25 TPY threshold for VOC or NO<sub>x</sub>, which would subject the facility to special permit requirements:

- Increases or decreases in emissions from the plan approval are aggregated with other net emissions increases over the consecutive 5-calendar year period including the year in which the plan approval is constructed (calendar years 2009 – 2013 for this Plan Approval); and
- Increases or decreases in emissions from the plan approval are aggregated with other net emission increases or decreases over the previous 10-year period. If the result is over threshold levels, the facility is subject only to the emissions offset requirements codified at 25 Pa Code §127.205.

If the resulting net change exceeds the applicable thresholds, those emissions must be offset by a ratio of 1.3 to 1. If the offsets come from internal emission reductions, then Lowest Achievable Emission Rate (LAER) requirement does not apply (25 Pa Code §127.203(b)(3)).

Table 4-3 below presents a summary of plan approval emissions for VOC and  $NO_x$  aggregated with other net emissions increases over the consecutive 5-calendar year period including the year in which the plan approval implementation is planned (calendar years 2009 through 2013).

Table 4-3 NA-NSR Netting Analysis for VOC and NO<sub>x</sub> Emissions (5-year)

Plan Approval	5-year NO <sub>x</sub> (TPY)	5-year VOC (TPY)
Heater Firing Rate Increase Plan Approval	140.1	23.2
Contemporaneous Increases	10.7	2.8
Net Emissions Increase	150.7	26.0
Internal Offsets required (1.3:1 Ratio)	195.9	33.8
Netting Credits Applied <sup>1</sup>	-195.9	-33.8
Net Emissions (After Offsetting, if applicable)	0.0	0.0
NA-NSR Significance Level	25	25
NA-NSR Review Required	No	No

<sup>&</sup>lt;sup>1</sup> The 5-calendar year net emission increase for NO<sub>x</sub> and VOC is offset using internal netting credits at a ratio of 1.3:1 as required by 25 Pa Code §127.203(b)(3).

Table 4-4 below presents a summary of plan approval emissions for  $NO_x$  and VOC aggregated with other net emission increases or decreases over the previous 10-year period.

Table 4-4 NA-NSR Netting Analysis for VOC and  $NO_x$  Emissions (10-year)

Plan Approval	10-year NO <sub>x</sub> (TPY)	10-year VOC (TPY)
Heater Firing Rate Increase Plan Approval	140.1	23.2
Contemporaneous Increases/Decreases	-296.7	-11.4
Net Emissions Increase	-156.7	11.7
NA-NSR Significance Level	25	25
NA-NSR Review Required	No	No

As shown in Tables 4-3 and 4-4 above, the net emissions increases of VOC and  $NO_x$  from the proposed plan approval are below the NA-NSR applicability thresholds of 25 tons per year. Therefore, the proposed plan approval is not subject to NA-NSR requirements for ozone.

For PM<sub>2.5</sub>, NA-NSR will be triggered if changes in direct PM<sub>2.5</sub> emissions exceed 10 TPY or emission changes associated with precursors such as NO<sub>x</sub> or SO<sub>2</sub> exceed 40 TPY. As indicated in Table 4-5 below, NO<sub>x</sub> emissions for the proposed plan approval exceed the NA-NSR regulatory threshold as a precursor to PM<sub>2.5</sub>; therefore, as per 25 Pa Code \$127.203a(a)(1)(i)(A), a netting analysis over the contemporaneous period must be performed.

Table 4-5 NA-NSR Analysis for SO<sub>2</sub>, NO<sub>x</sub>, and PM<sub>2.5</sub> Emissions (Step 1)

Plan Approval	SO <sub>2</sub> (TPY)	NO <sub>x</sub> (TPY)	PM <sub>2.5</sub> (TPY)
Heater Firing Rate Increase Plan Approval	7.1	140.1	13.2
NA-NSR Significance Level	40	40	10
NA-NSR Triggered (Before Netting Analysis)	No	Yes	Yes

As shown in Table 4-6 below, the  $PM_{2.5}$  and  $NO_x$  (as a  $PM_{2.5}$  precursor) netting analysis over the contemporaneous period shows that the emissions from the plan approval are not greater than the NA-NSR thresholds for  $PM_{2.5}$ . Therefore, the proposed plan approval is not subject to 25 Pa Code §127.203a for  $PM_{2.5}$ .

Table 4-6 NA-NSR Netting Analysis for  $PM_{2.5}$  and  $NO_x$  as  $PM_{2.5}$  Precursor (Step 2)

Plan Approval	NO <sub>x</sub> (TPY)	PM <sub>2.5</sub> (TPY)
Heater Firing Rate Increase Plan Approval	140.1	13.2
Contemporaneous Increases/Decreases	-320.7	-22.3
Net Emissions Increase	-180.7	-9.0
NA-NSR Significance Level	40	10
NA-NSR Review Required	No	No

## 5.0 BACT ANALYSIS FOR CO CONTROL

As shown in Section 4.1.2, the net increase in CO emissions associated with this plan approval is above the PSD threshold. Therefore, the target heaters are subject to the application of BACT.

#### 5.1 METHODOLOGY

BACT is defined in 40 CFR 52.21(b)(12) of the PSD regulations as "...an emission limitation based on the maximum degree of reduction for each pollutant subject to regulation under the Act which would be emitted from any...source...which on a case-by-case basis is determined to be achievable taking into account energy, environmental and economic impacts and other costs". Both 25 Pa Code §127.83 and AMS Regulation I, Section XI, Part C incorporate the PSD regulations codified in 40 CFR 52.21 by reference.

Each BACT analysis is done on a case-by-case basis, where the reviewing authority evaluates the energy, environmental, economic and other costs associated with each alternative technology, and the benefit of the expected reduced emissions which the technology would bring. In no event however, can an emission limitation be recommended that would not be at least as stringent as any applicable standard of performance under 40 CFR Parts 60 (New Source Performance Standards) and 61 ((National Emission Standards for Hazardous Air Pollutants). Additionally, if the reviewing authority finds during the course of a BACT analysis that there is no economically reasonable or technologically feasible way to accurately measure the emissions, and hence to impose an enforceable emissions standard, it may require the source to use design, alternative equipment, work practices or operational standards to reduce emissions of the pollutant.

In summary, the top-down process provides that all available control technologies be ranked in descending order of control effectiveness. The PSD applicant first examines the most stringent or "top" alternative. This alternative is to be selected as BACT unless the applicant demonstrates, and the permitting authority in its informed judgment agrees, that technical considerations, or energy, environmental, or economic impacts justify a conclusion that the most stringent technology is not "achievable" in that case. If the most stringent technology is eliminated in this fashion, then the next most stringent alternative is considered, and so on.

Under the "top-down" approach, as described in EPA's *Draft New Source Review Workshop Manual*, the five basic steps of a "top-down" BACT analysis are listed as follows:

Step 1: Identify potential control technologies

Step 2: Eliminate technically infeasible options

Step 3: Rank remaining control technologies by control effectiveness

Step 4: Evaluate the most effective controls and document results

Step 5: Select BACT

The first step is to identify potentially "available" control options for each emission unit triggering PSD, for each pollutant under review. Available options should consist of a comprehensive list of those technologies with a potentially practical application to the emission unit in question. The list includes technologies used to satisfy BACT requirements, innovative technologies, and controls applied to similar source categories.

During any BACT review, typically, the following sources are investigated to identify potentially available control technologies:

- EPA's RACT/BACT/LAER Clearinghouse (RBLC) Database;
- EPA's New Source Review Website;
- In-house experts;
- State air regulatory agency contacts;
- Technical articles and publications;
- State permits issued for similar sources that have not yet been entered into the RBLC; and
- Guidance documents and personal communications with federal and state agencies.

After identifying potential technologies, the second step is to eliminate technically infeasible options from further consideration. To be considered feasible, a technology must be both available and applicable. It is important, in this step, that the technical basis for eliminating a technology from further consideration be clearly documented based on

physical, chemical, engineering, and source-specific factors related to safe and successful use of the controls.

The third step is to rank the technologies not eliminated in Step 2 in order of descending control effectiveness for each pollutant of concern. If the highest ranked technology is proposed as BACT, it is not necessary to perform any further technical or economic evaluation. Potential adverse impacts of implementing such technology, however, must still be identified and evaluated.

The fourth step entails an evaluation of energy, environmental, and economic impacts for determining a final level of control. The evaluation begins with the most stringent control option and continues until a technology under consideration cannot be eliminated based on adverse energy, environmental, or economic impacts. The economic or "cost-effectiveness" analysis is conducted in a manner consistent with EPA's OAQPS Control Cost Manual Fifth Edition (EPA 1996) and subsequent revisions. An important aspect of the top-down BACT methodology is the establishment of baseline emission levels that are used in calculating the cost-effectiveness of alternative control options. EPA's Draft New Source Review Workshop Manual states that baseline emissions should be a realistic upper bound estimate of emissions taking into account physical or operational constraints and historical operating data.

The fifth and final step is to select as BACT the emission limit resulting from application of the most effective of the remaining technologies under consideration for each pollutant of concern.

## 5.2 IDENTIFY ALL CONTROL TECHNOLOGIES

This plan approval will require the target heaters to be evaluated for CO controls. The potentially available emission controls for reducing CO emissions from heaters are:

- Good combustion practices; and
- Oxidation catalysts.

Based on a review of EPA's RBLC database, Bay Area Air Quality Management District (BAAQMD) BACT database (see Attachment G), and other permits issued for refineries, no documented cases of oxidation catalysts being implemented on similarly sized heaters were identified. Therefore, installation of oxidation catalyst for heaters of this size has not been demonstrated and is not available. The lack of application in

refineries is largely due to operational limitations of the oxidation catalysts. The installation of oxidation catalyst in flue gas containing more than trace levels of SO<sub>2</sub> will result in poisoning and deactivation of the catalyst by sulfur-containing compounds, as well as increasing the conversion of SO<sub>2</sub> to SO<sub>3</sub>. This would increase condensable particulate matter emissions, which would foul the catalyst, in turn, prohibiting oxidation as well as increasing flue gas system corrosion rates. Another operating limitation is that oxidation catalysts typically operate at 650 degrees Fahrenheit (°F) to 1,000°F to be effective at minimizing CO emissions. None of the heaters in this BACT analysis achieve stack temperatures within the typical operating range of an oxidation catalyst.

## 5.3 ELIMINATE TECHNICALLY INFEASIBLE OPTIONS

This step of the top-down BACT analysis eliminates from consideration technically infeasible options. A control technology is not considered technically feasible unless it is both available and applicable according to the New Source Review Workshop manual. To be considered available, a technology must have reached the licensing and commercial demonstration phase of its development. Applicability is based on source-specific factors and physical, chemical, and engineering principles that include safe and successful operation of a control option at a specific location.

While documented application of oxidation catalysts for refinery heaters similar to those in this plan approval application has not been identified and operational limitations related to stack temperatures and catalyst poisoning prevent the use of oxidation catalysts on the existing target heaters – making the technology infeasible, PES will nonetheless carry that technology forward to the next steps. Thus, all options presented will be explored in more detail.

# 5.4 RANK REMAINING CONTROL TECHNOLOGIES BY CONTROL EFFECTIVENESS

The next step in the top-down BACT analysis is to rank the remaining control technologies by control effectiveness. Technologies for minimizing CO emissions from the target heaters (estimated level of reduction):

1. Good combustion practices (reduction level varies based on heater configurations)

# 2. Oxidation catalysts (50-92%7)

# 5.5 EVALUATE MOST EFFECTIVE CONTROLS BASED ON ECONOMIC, ENERGY, AND ENVIRONMENTAL IMPACTS

The fourth step in the top-down BACT analysis involved the evaluation of energy, environmental, and economic impacts for determining a final level of control. The evaluation begins with the most stringent control option and continues until a technology under consideration cannot be eliminated based on adverse energy, environmental, or economic impacts.

While the use of an oxidation catalyst has not been identified as a demonstrated technology for refinery heaters, the Refinery has estimated the cost effectiveness at approximately \$10,800 to \$17,800 per ton of CO emissions reductions (see analysis presented in Attachment H). An EPA guidance document was used as the basis for this analysis and limitations regarding stack temperatures relative to required catalyst operating temperatures as well as any impacts of catalyst fouling were ignored. The EPA Air Pollution Control Technology Fact Sheet for Regenerative Incinerator (EPA-452/F-03-021) shows that capital costs range from \$51.50 to \$206 per cubic foot per minute (cfm) and operation and maintenance costs range from \$8.80 to \$29.40 per cfm (costs escalated from 2002 to 2012 dollars). Conservatively, PES estimated cost effectiveness using \$51.50 per cfm for capital costs and \$8.80 per cfm for operation and maintenance costs. Further note - as PES is a recently established company in a private equity structure, the cost of borrowing capital (the minimum return that investors expect for providing capital to the company) is considered at a higher risk than many established companies. The cost effectiveness analysis reflects the current cost of capital for PES, which is 21.83%.

The estimates of potential emission reductions that could be achieved through the application of an oxidation catalyst, and corresponding control effectiveness costs (\$/ton), are calculated based on the total CO emissions from the sources. As shown in Attachment H, even when using the most conservative (lowest expected) capital and annual operating and maintenance costs and ignoring potential issues regarding flue gas temperatures, the installation of oxidation catalyst for CO control would not be considered cost effective.

For the BACT cost effectiveness analysis, PES conservatively assumed 92% control effectiveness for application of oxidation catalyst (See Attachment H).

#### 5.6 SELECTION OF BACT

Aside from the technical issues discussed above, the installation of oxidation catalyst for CO control is not considered cost effective and is eliminated from further analysis. Good combustion practice is the predominantly used control option for reducing CO emissions from process heaters. PES currently implements good combustion practice through a comprehensive program of quarterly combustion tuning, as required by the facility's RACT permit. The use of combustion tuning and implementation of periodic maintenance on the heaters ensure that the CO emissions are limited.

Accordingly, good combustion practices are BACT for limiting CO emissions from the heaters.

The heaters will also have annual emission limits (TPY) as discussed in Section 7.

#### 6.0 APPLICABLE STANDARDS

Local, state, and federal regulations, in addition to NA-NSR and PSD have been reviewed for applicability to this plan approval. The following sections provide a summary of these reviews.

#### 6.1 PADEP REGULATIONS - BEST AVAILABLE TECHNOLOGY ANALYSIS

As part of this Plan Approval analysis, AMS has requested a Best Available Technology (BAT) analysis for the applicable target heaters, and PES provides this analysis below.

25 Pa Code §127.12(a)(5) provides that an application for a plan approval must show that emissions from a "new source" will be the minimum attainable through the use of Best Available Technology (BAT). 25 Pa Code §121.1 (Definitions) defines a new source as a source that was constructed and commenced operation on or after July 1, 1972, or a source that was modified so that the fixed capital cost of new components exceeds 50% of the fixed capital cost that would be required to construct a comparable entirely new source<sup>8</sup>.

The Unit 231-B101 Heater and the Unit 210-H101 Heater are excluded from this analysis as they were installed prior to July 1, 1972 and have not been modified since that date in any way that would result in the emission of an air contaminant not previously emitted. While Unit 231-B101 Heater was upgraded in 2004 for the installation of low  $NO_x$  burners, the cost of those changes was not in excess of the 50% fixed capital cost described above for the project to be considered a "new source" per 25 Pa Code §121.1.

PES has completed a review of available and applicable emission controls beyond those already implemented on these heaters for all criteria pollutants. The target heaters covered by this plan approval and their corresponding construction dates at the Philadelphia Refinery are shown in Table 6-1 below.

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<sup>&</sup>lt;sup>8</sup> The heaters involved in this plan approval are existing sources, not new sources as defined above. Further, the heaters are not being modified as defined above. Therefore, PES believes that BAT analysis is not required as a part of this Plan Approval application. Nonetheless, PES provides this BAT analysis in response to AMS' request for same.

Table 6-1 Target Heaters Construction Dates

Process Unit	Heater	Construction Date
GP Unit 231 HDS	B101 Feed Heater	1957
PB Unit 865 HDS	11H1 Feed Heater	1973
PB Unit 865 HDS	11H2 Reboiler Heater	1973
PB Unit 210 Crude	H101 Crude Heater	1964
PB Unit 210 Crude	H-201A/B Crude Heater	1973
PB Unit 866 HDS	12H1 Feed Heater	1973
PB Unit 868 FCCU	8H101 Recycle Heater	1980

BAT is a pollutant-specific determination. Based on a review of established emission control technologies and emission limits in permits, the following text documents the results of the source and pollutant specific BAT determinations.

The Refinery reviewed publicly available databases to identify potential controls that have been installed on sources similar to the proposed heaters, including:

- EPA's New Source Review website;
- U.S. EPA's RACT/BACT/LAER Clearinghouse (RBLC) Database;
- Recent EPA consent decrees within the refining industry; and
- State and federal guidance documents.

Detailed discussion on the BAT analysis for all pollutants affected by this plan approval is presented below.

# 6.1.1 $NO_x$ Controls

PES reviewed available and applicable  $NO_x$  controls that have been installed on process heaters at refineries or similar operations. Currently, combustion tuning is performed on the target heaters to reduce  $NO_x$  emissions. In addition, the Unit 210-H201 heater has and Unit 865-11H1 will have ultra-low  $NO_x$  burners (ULNB) installed to reduce  $NO_x$  emissions as part of this plan approval.

The Refinery evaluated the potential emission reductions that could be achieved beyond the current baseline emissions using more stringent emission controls including:

- Low NO<sub>x</sub> Burners (LNB);
- Selective catalytic reduction (SCR);
- Selective non-catalytic reduction (SNCR);
- A combination of ULNB plus SCR; and
- A combination of LNB plus SNCR.

The Refinery estimated the cost effectiveness for additional  $NO_x$  controls beyond those currently installed on these heaters in the BAT  $NO_x$  cost effectiveness analysis presented in Attachment I. Cost effectiveness of the various technology options range from approximately \$7,400 to \$41,000 per ton of  $NO_x$  emissions reductions. As PES is a recently established company in a private equity structure, the cost of borrowing capital (the minimum return that investors expect for providing capital to the company) is considered at a higher risk than many established companies. The cost effectiveness analysis reflects the current cost of capital for PES, which is 21.83%.

In the cost analyses contained here, costs for  $NO_x$  CEMS have not been included in the control effectiveness costs. However, it is expected that installation of a CEMS would likely be requested by AMS as part the installation of any of the control options considered. Adding a CEMS would result in an estimated additional \$40,000 in annualized costs, which corresponds to an actual additional cost of \$1,400 to \$3,900 per ton depending on the  $NO_x$  emission rate. Therefore, the control effectiveness costs presented in Attachment I are considered conservative since the actual costs to the Refinery are expected to be greater.

For the Unit 210-H201 and Unit 865-11H1 heaters, PES determined that SCR cannot physically fit the plot plan and there is inadequate pressure from the burners to overcome the SCR pressure drop. Flue gas recirculation would require the installation of mechanical draft burners, a major re-design for both units. Accordingly, ULNBs are considered BAT for the Unit 210-H201 and Unit 865-11H1 heaters.

For the remaining heaters (Unit 865-11H2, Unit 866-12H1, and Unit 868-8H101), the BAT cost effectiveness analysis determined that no additional controls were found to be cost effective, as set forth in

Attachment I. Therefore, operation of the units as proposed under this plan approval and as shown in Table 6-2 below satisfies BAT.

Table 6-2  $NO_x$  BAT Determinations

Process Unit	Heater	Proposed Annual Firing Limit (MMBtu/year)	NO <sub>x</sub> BAT
PB Unit 865 HDS	11H1 Feed Heater	699,000	ULNB
PB Unit 865 HDS	11H2 Reboiler Heater	500,000	Tuning <sup>1</sup>
PB Unit 210 Crude	H201 Crude Heater	2,172,000	ULNB
PB Unit 866 HDS	12H1 Feed Heater	456,000	Tuning <sup>1</sup>
PB Unit 868 FCCU	8H101 Recycle Heater	480,000	Tuning <sup>1</sup>

<sup>&</sup>lt;sup>1</sup> Combustion tuning required by the RACT Plan Approval satisfies BAT.

#### 6.1.2 CO Controls

See the detailed BACT discussion in Section 5 for CO controls.

Good combustion practices are BAT for limiting CO emissions from the heaters.

## 6.1.3 PM/PM<sub>10</sub>/PM<sub>2.5</sub> Controls

The available emission control options for reducing PM emissions from the heaters include:

- Good combustion practices;
- Electrostatic precipitators;
- Baghouse or fabric filters; and
- Use of gaseous fuels.

Refinery fuel gas will be used as the only fuel for these heaters. Based on our review of the RBLC database, BAAQMD, and permits issued at refineries, ESPs or baghouses are not installed on similarly sized heaters fired on refinery fuel gas. Though these control options are potentially technically feasible for combustion sources such as process heaters, they are not commercially demonstrated on similarly sized process heaters.

Therefore, these control options are not further considered in this evaluation. The refinery fuel gas fired in the heaters is comprised of a significant amount of natural gas and therefore, is similar in heating value and characteristics to natural gas.

BAT for limiting PM emissions is good combustion practices and firing of refinery fuel gas.

## 6.1.4 SO<sub>2</sub> Controls

The available emission control options for minimizing SO<sub>2</sub> emissions from the heaters include:

- Wet flue gas desulfurization (FGD) scrubber;
- Dry FGD scrubber; and
- Use of gaseous fuels.

Based on a review of EPA's RBLC and BAAQMD databases, and permits issued for refineries, wet FGD and dry FGD systems have not been installed on natural gas or refinery fuel gas fired heaters at any refinery in the country. Though these control options are potentially technically feasible for combustion sources such as process heaters, they are not commercially demonstrated on similarly sized process heaters. Therefore, these control options are not considered further in this evaluation.

As described earlier, refinery fuel gas consists of a combination of refinery process by-product gas and natural gas. The refinery by-product gas is desulfurized prior to supplementing with natural gas through a mix drum in order to ensure New Source Performance Standards Subpart J limits are met prior to combustion. Refinery fuel gas is used at every refinery in the country as part of balancing available energy from process operations and by-products.

The use of refinery fuel gas is BAT for the target heaters for SO<sub>2</sub>.

#### 6.1.5 *VOC Controls*

The available emission control options for minimizing VOC emissions from the heaters include:

- Oxidation catalysts; and
- Good combustion practices; and

# Use of gaseous fuels.

Based on our review of the RBLC and BAAQMD databases, oxidation catalysts have not been demonstrated on process heaters at refineries. The predominant control option to reduce VOC emissions from process heaters is the use of good combustion practice. The use of oxidation catalyst is not commercially demonstrated on refinery process heaters. Therefore, oxidation catalysts are not considered further in this analysis.

PES currently implements a comprehensive program of quarterly combustion tuning, as required by the facility's RACT permit. The use of combustion tuning and implementation of periodic maintenance on the heaters ensures that the VOC emissions are limited.

The heaters only fire refinery fuel gas which is lower in VOC content than liquid fuels and some other gaseous fuels. The Refinery removes many VOCs from the by-product gases before they are sent to the refinery fuel gas system and thus refinery fuel gas consists of mostly non-VOC compounds such as methane, ethane, and hydrogen.

The use of good combustion practices and firing of refinery fuel gas is BAT for VOC.

#### 6.2 AIR MANAGEMENT SERVICES REGULATIONS

AMS Regulations incorporate Pennsylvania air contaminant emissions limits and control efficiencies (Regulation I, Section X) and include by reference, the federal regulations (AMS Regulation 1, Section XI). AMS also regulates SO<sub>2</sub> emissions (Regulation III, Section III), fuel sulfur content (Regulation III, Section III), pump and compressor emissions (Regulation V, Section IV), and process equipment leaks (Regulation V, Section XIII).

With regard to Regulation VI, there will be no new air toxic contaminants associated with this plan approval.

There are no AMS regulations that are significantly different from, or more stringent than, the regulations cited herein. The proposed plan approval will not result in any additional AMS applicable requirements.

#### 6.3 FEDERAL REGULATIONS

## 6.3.1 New Source Performance Standards (NSPS)

The Refinery evaluated whether increasing the firing rates for the target heaters triggers the applicability of NSPS for any Refinery sources. No physical changes or capital expenditures are required to accommodate the increase in firing rates. As such, no sources are considered to be modified sources under EPA's New Source Performance Standards codified under 40 CFR Part 60. Specifically, 40 CFR 60.14(e)(2) excludes from the definition of modification...

"an increase in production rate of an existing facility, if that increase can be accomplished without a capital expenditure on that facility."

The increase in heater firing rates sought in this plan approval represents a production rate increase for the target heaters. All of the heaters serve the same overall purpose - to produce heated hydrocarbon streams for processing. Additionally, as discussed in published EPA guidance, both changes in production rate and operating changes are included in the assessment of capital expenditure associated with the plan approval<sup>9</sup>.

The change in firing rates for the target heaters in this plan approval can be achieved without any capital expenditure. Therefore, the target heaters are not considered modified sources and therefore are not subject to NSPS.

While PES is agreeing to voluntarily install ULNB on the Unit 231-B101 and Unit 865-11H1 Heaters, PES does not feel that this constitutes an NSPS modification. However, it should be noted that the future projected  $NO_x$  emission rate (0.03 lb/MMBtu) for each of these heaters is expected to meet the  $NO_x$  emissions limitations (0.04 lb/MMBtu) set forth in 40 CFR 60.102a(g)(2)(i).

# 6.3.2 Maximum Achievable Control Technology (MACT)

The target heaters will be subject to the National Emission Standards for Hazardous Air Pollutants for Major Sources: Industrial, Commercial, and Institutional Boilers and Process Heaters (Boiler MACT) codified in 40 CFR §63.7490. The existing target heaters must be in compliance with Boiler MACT within 180 days of January 31, 2016. The Refinery will demonstrate compliance by performing annual tune-ups of each affected heater and completing a one-time energy assessment.

<sup>&</sup>lt;sup>9</sup> EPA, 1989. Re: Applicability of NSPS. Letter from Don R. Clay, Acting Assistant EPA Administrator of EPA to Mr. John W. Boston, WEPCO, February 15, 1989.

#### 7.0 PROPOSED PLAN APPROVAL CONDITIONS

PES proposes the following permit conditions and compliance methods for the proposed plan approval. The target heaters will be subject to revised firing rate limits as shown in Tables 7-1 and 7-2 and annual emission limits (TPY) as shown in Tables 7-3 and 7-4.

Table 7-1 Revised Firing Rate Limits for Unmodified Target Heaters

Process Unit	Heater	Proposed Annual Firing Limit (MMBtu/year)	RACT NO <sub>x</sub> Emission Rate Limit (lb/MMBtu) <sup>1</sup>	
PB Unit 865 HDS	11H2 Reboiler Heater	500,000	0.113	
PB Unit 210 Crude	H101 Crude Heater	1,643,000	0.089	
PB Unit 210 Crude	H201 Crude Heater	2,172,000	0.03	
PB Unit 866 HDS	12H1 Feed Heater	456,000	0.113	
PB Unit 868 FCCU	8H101 Recycle Heater	480,000	0.113	

 $<sup>^{1}</sup>$  See Attachment A for the RACT Analysis that discusses the RACT  $NO_x$  emission rate for each target heater.

Table 7-2 Revised Firing Rate Limits for Modified Target Heaters

Process Unit	Heater	Firing Limit	RACT NO <sub>x</sub> Emission Rate Limit (lb/MMBtu)	
RAC	T Plan Approval Conditions	Pending ULNB Installat	ion	
GP Unit 231 HDS	GP Unit 231 HDS B101 Feed Heater		0.122	
PB Unit 865 HDS	11H1 Feed Heater	72.2 MMBtu/hr	0.113	
Pro	pposed Conditions after ULN	NB Installation and Testin	g	
GP Unit 231 HDS	GP Unit 231 HDS B101 Feed Heater		0.03 1	
PB Unit 865 HDS	11H1 Feed Heater	699,000 MMBtu/year	0.03 1	

 $<sup>^{1}</sup>$  The Firing and RACT NO<sub>x</sub> Firing Rate Limits will only apply to the Unit 231-B101 and Unit 865-11H1 Heaters after the ULNBs have been successfully installed and tested.

Compliance with the annual firing rate limits will be demonstrated on a rolling 365-day average. The Refinery will monitor the inputs to the heaters including fuel throughput (scf/hour) and heat content (Btu/scf) on a daily basis for compliance with the firing rate limits.

Table 7-3 Proposed Emissions Limits for Unmodified Target Heaters (Based on Projected Actual Emissions)

Target Heater	PM (TPY)	PM <sub>10</sub> (TPY)	PM <sub>2.5</sub> (TPY)	CO (TPY)	VOC (TPY)	NO <sub>x</sub> (TPY)	SO <sub>2</sub> (TPY)	Lead (TPY)	CO <sub>2</sub> e (TPY)
Unit 865-11H2	1.8	1.8	1.8	20.4	1.3	28.3	0.5	1.2E-04	29,168
Unit 210-H101	6.1	6.1	6.1	66.9	4.4	73.1	2.7	4.0E-04	95,847
Unit 210-H201	8.0	8.0	8.0	88.5	5.8	32.6	3.2	5.3E-04	126,707
Unit 866-12H1	1.7	1.7	1.7	18.6	1.2	25.8	0.5	1.1E-04	26,601
Unit 868-8H101	1.7	1.7	1.7	18.9	1.2	27.1	0.6	1.1E-04	27,054

Table 7-4 Proposed Emissions Limits for Modified Target Heaters (Based on Projected Actual Emissions)

Target Heater	PM (TPY)	PM <sub>10</sub> (TPY)	PM <sub>2.5</sub> (TPY)	CO (TPY)	VOC (TPY)	NO <sub>x</sub> (TPY)	SO <sub>2</sub> (TPY)	Lead (TPY)	CO <sub>2</sub> e (TPY)
	Prop	osed Con	ditions af	ter ULNB	Installatio	on and Tes	sting 1		
Unit 231-B101	3.1	3.1	3.1	34.4	2.3	12.8	0.8	2.0E-04	49,253
Unit 865-11H1	2.6	2.6	2.6	28.5	1.9	10.5	0.7	1.7E-04	40,777

<sup>&</sup>lt;sup>1</sup> The Emissions Limits will only apply to the Unit 231-B101 and Unit 865-11H1 Heaters after the ULNBs have been successfully installed and tested.

Compliance with the annual emission limits (TPY) will be on a rolling 12-month basis.

Attachment A Reasonably Achievable Control Technology (RACT) analysis

# REASONABLY ACHIEVABLE CONTROL TECHNOLOGY ANALYSIS



Philadelphia Energy Solutions Refining and Marketing, LLC. (PES).

Reasonably Achievable Control Technology Analysis for the Heater Firing Rate Increase

August 31, 2012 (Submittal) September 6, 2012 (Completeness Determination) September 2013 (Supplement)

**Environmental Resources Management** 

75 Valley Stream Parkway Suite 200 Malvern, Pennsylvania 19355

REA	SONA	BLY ACHIEV	ABLE CONTROL TECHNOLOGY ANALYSIS	1			
1.0	REA	SONABLY A	CHIEVABLE CONTROL TECHNOLOGY ANALYSIS	1			
	1.1	RACT ANA	LYSIS REQUIREMENTS	1			
	1.2	1.2.1 P 1.2.2 N	N APPROVAL CHANGES Presumptive RACT Revisions Modifications to Unit 231-B101 and Unit 865-11H1 Sessation of Refinery Fuel Oil Firing	3 3 3 4			
	1.3	RACT COS	T EFFECTIVENESS CALCULATIONS	6			
	1.4	RACT ANA	LYSIS RESULTS	7			
2.0 RACT PI		T PLAN APP	ROVAL PROPOSED CONDITIONS	8			
	2.1	RACT CON	TROL EQUIPMENT REQUIREMENTS	8			
	2.2	RACT IMP	LEMENTATION SCHEDULE	8			
	2.3	RACT TEST	TING REQUIREMENTS AND STACK EMISSION ONS	8			
	2.4	RACT REC	ORDKEEPING AND REPORTING REQUIREMENTS	9			
List	of Tabl	les					
	Table	2 1-1	25 Pa Code §129.92(b) RACT Requirements				
	Table	2 1-2	Proposed RACT Plan Approval Conditions for Unit 231-B10 Unit 865-11H1	01 and			
	Table	2 1-3	$NO_x$ Emissions Reductions from Cessation of Refinery Fuel Oil Firing				
	Table	2 1-4	Summary of RACT Plan Approval Revisions				
	Table	2 2-1	RACT Plan Approval Existing and Proposed Limits				
List	of App	endix					
	Арре	ndix A	RACT Cost Effectiveness Analysis				

#### 1.0 REASONABLY ACHIEVABLE CONTROL TECHNOLOGY ANALYSIS

The Sunoco, Inc. (R&M)¹ Girard Point Processing Area and Point Breeze Processing Area RACT Plan Approval amended on October 7, 2002 was established for nitrogen oxides (NO<sub>x</sub>) and volatile organic compounds (VOCs) and limits the firing rate on the heaters to comply with the RACT regulatory requirements codified in 25 Pa Code §129.91 through §129.95. This application addresses changes to certain NO<sub>x</sub> RACT conditions². No changes to VOC RACT conditions are requested. With this application, the Refinery proposes to remove the firing rate limits in the RACT Plan Approval for seven target heaters:

- Unit 231-B101 Heater;
- Unit 865-11H1 Heater;
- Unit 865-11H2 Heater;
- Unit 210-H101 Heater;
- Unit 210-H201 Heater;
- Unit 866-12H1 Heater; and
- Unit 868-8H101 Heater.

# 1.1 RACT ANALYSIS REQUIREMENTS

As described in 25 Pa Code §129.92(b), each RACT Analysis must include the requirements listed in Table 1-1 below.

<sup>&</sup>lt;sup>1</sup> The Sunoco Philadelphia Refinery is now owned and operated by Philadelphia Energy Solutions Refining and Marketing, LLC (PES).

<sup>&</sup>lt;sup>2</sup> The RACT Plan Approval revisions to the target heater firing rate or emission limits are not being requested by PES to comply with any requirements of Consent Decree No. 05-02866 (Fourth Amendment, dated August 17, 2012).

Table 1-1 25 Pa Code §129.92(b) RACT Requirements

25 Pa Code §129.92(b) Requirement	Discussion
A ranking of the available control options for the affected source in descending order of control effectiveness. <sup>1</sup>	<ul> <li>Ultra-low NO<sub>x</sub> burners (ULNB) and Selective Catalytic Reduction (SCR) - 96%</li> <li>Selective Catalytic Reduction - 85%</li> <li>Ultra-low-NO<sub>x</sub> burners - 66 to 76%</li> <li>Low-NO<sub>x</sub> burners and Selective Non-Catalytic Reduction (SNCR) - 70%</li> <li>Low-NO<sub>x</sub> burners (LNB) and Flue Gas Recirculation (FGR) - 55%</li> <li>Selective Non-Catalytic Reduction - 40%</li> </ul>
An evaluation of the technical feasibility of the available control options identified based on physical, chemical and engineering principles. A determination of technical infeasibility should identify technical difficulties restricting the successful use of the control option on the affected source.	<ul> <li>Unit 865-11H1 - The installation of SCR is not possible as there is not adequate plot space available; further, there is not adequate pressure to overcome the SCR pressure drop; therefore, SCR is infeasible. FGR installation would require the installation of mechanical draft burners, which is a major re-design of the unit; therefore FGR is infeasible.</li> <li>Unit 210-H101 - FGR would not physically fit the plot space; therefore, it is infeasible.</li> <li>Unit 210-H201 - The installation of SCR is not possible as there is not adequate plot space available; further, there is not adequate pressure to overcome the SCR pressure drop; therefore, SCR is infeasible. FGR installation would require the installation of mechanical draft burners, which is a major re-design of the unit; therefore FGR is infeasible.</li> </ul>
A ranking of the technically feasible control options in order of overall control effectiveness for NO <sub>x</sub> emissions.	The RACT summary in Appendix A for each target heater ranks the technically feasible controls options by listing them from highest to lowest control effectiveness.
The baseline emissions of $NO_x$ before implementation of each control option ("pre-control emissions").	The "pre-control emissions" are listed in the "Potential Emissions (TPY)" column for each target heater in the RACT summary for each heater in Appendix A.
The estimated emission reduction potential or the estimated control efficiency of each control option.	The estimated emission reduction potential for each control option for each target heater is listed in the "Potential NO <sub>x</sub> Reduced (TPY)" column in the RACT summary for each heater in Appendix A. These values based on design firing for each heater.
The estimated emissions after the application of each control option ("post-control emissions").	The "post-control emissions" are listed in the "Maximum Post Control Emissions @ Design Firing (TPY)" column for each target heater in the RACT summary for each heater in Appendix A.
An evaluation of cost effectiveness of each control option consistent with EPA's cost guidance manuals. The cost effectiveness shall be evaluated in terms of dollars per ton of NO <sub>x</sub> emissions reduction.	See Appendix A for the RACT Cost Effectiveness Analysis.

 $<sup>^1\</sup> NO_x$  control effectiveness derived from Alternative Control Techniques Document –  $NO_x$  Emissions from Process Heaters (Revised) - EPA Emissions Standards Division - EPA-453/R-93-034 and Refinery process knowledge.

#### 1.2 RACT PLAN APPROVAL CHANGES

PES is requesting changes to the RACT Plan Approval including updates to presumptive RACT sources and updates to previous RACT determinations on select heaters. For this RACT analysis and future RACT analyses, PES is requesting that the RACT determinations focus on identifying specific NO<sub>x</sub> control technology requirements and pollutant emission rates (lb/MMBtu) as RACT. Previously the RACT determinations were identified as hourly firing rate limits (MMBtu/hr) and pollutant emission rates. The basis for the RACT analysis, provided here, now relies on design firing for all heaters.

A summary of requested RACT Plan Approval revisions are found in Table 1-4 at the end of this section.

## 1.2.1 Presumptive RACT Revisions

Three of the target heaters, Unit 865-11H2, Unit 866-12H1, and Unit 868-8H101, previously had firing rate limits less than 50 million British thermal units per hour (MMBtu/hr) and were therefore subject to presumptive RACT  $NO_x$  controls established under 25 Pa Code §129.93. Presumptive RACT required the use of combustion tuning rather than physical controls. Because these three heaters are seeking annual equivalent firing rate limits over 50 MMBtu/hr, PES has provided a Case-by-Case RACT analysis in Appendix A for these heaters as a part of this plan approval application along with the other target heaters.

# 1.2.2 Modifications to Unit 231-B101 and Unit 865-11H1

Ultra-low  $NO_x$  burners (ULNBs) are planned to be installed on Unit 231-B101 and Unit 865-11H1³. PES proposes that the RACT Plan Approval be revised to keep the current RACT limits for hourly firing limit (MMBtu/hr) and  $NO_x$  emission rate (lb/MMBtu) in place until the installation of the ULNBs are complete. A new permit condition should be included in Section 2 of the RACT Plan Approval to only allow the removal of the hourly firing limits for the Unit 231-B101 and Unit 865-11H1 heaters after the ULNBs have been successfully installed and stack test results show that the heaters meet the specified  $NO_x$  emission rate (0.03 lb/MMBtu). See the proposed RACT limits in Table 1-2 below.

-

As part of a settlement agreement with the Clean Air Council, PES agreed voluntarily to install ultra-low  $NO_x$  burners on Unit 231-B101 Heater and Unit 865-11H1 Heater at the Refinery to further reduce emissions beyond the cuts achieved by the shut-down of the Marcus Hook Refinery.

Table 1-2 Proposed RACT Plan Approval Conditions for Unit 231-B101 and Unit 865-11H1

Heater	Hourly Firing Limit NO <sub>x</sub> Emission Rate (MMBtu/hr) (lb/MMBtu)		RACT NO <sub>x</sub> Control			
RACT Plan Approval Conditions Pending ULNB Installation						
Unit 231-B101	91	0.122 (refinery fuel gas)	Combustion Tuning			
Unit 865-11H1	72.2	0.113 (refinery fuel gas)/0.400 (refinery fuel oil)	Combustion Tuning			
	Proposed Conditions af	ter ULNB Installation and Testi	ng			
Unit 231-B101		0.03 (refinery fuel gas)	Combustion Tuning			
Unit 865-11H1		0.03 (refinery fuel gas)	Combustion Tuning			

# 1.2.3 Cessation of Refinery Fuel Oil Firing

As discussed under Section 110(l) of the Clean Air Act, while the changes to the RACT Plan Approval include removal of firing rates of seven heaters, the RACT Plan Approval will still provide reasonable further progress toward ozone attainment because PES is also requesting removal of the ability for fuel oil firing for five of the seven heaters. Typically refinery fuel oil firing  $NO_x$  emission rates are higher than gaseous fuel-firing  $NO_x$  emission rates.

Table 1-3 below shows the change in  $NO_x$  maximum emissions, based on the RACT limits for the target heaters based on the removal of the ability for fuel oil firing. The current oil firing  $NO_x$  emissions rate limits and hourly firing limits (MMBtu/hr) as well as the proposed gaseous fuel-firing  $NO_x$  emission rate limits and design firing (MMBtu/hr) for five of the target heaters were used to determine the total reduction in maximum  $NO_x$  emissions associated with the proposed RACT limit changes. This reduction in emissions provides reasonable further progress toward ozone attainment.

Table 1-3 NO<sub>x</sub> Emissions Reductions from Cessation of Refinery Fuel Oil Firing

Target Heater	Existing Hourly Firing Limit (MMBtu/ hr)	Oil Firing Emission Limit (lb NO <sub>x</sub> / MMBtu)	Current RACT NO <sub>x</sub> (TPY)	Design Firing (MMBtu/ hr)	Gas Firing Proposed Emission Limit (lb NO√ MMBtu)	Proposed RACT NO <sub>x</sub> (TPY)	Change in NO <sub>x</sub> (TPY)		
Unit 865-11H1	72.2	0.400	126.5	87.3	0.030	11.5	<i>-</i> 115.0		
Unit 865-11H2 <sup>1</sup>	49.9	0.113	24.7	64.2	0.113	31.8	7.1		
Unit 210-H101	183.0	0.400	320.6	192.0	0.089	74.8	-245.8		
Unit 210-H201	242.0	0.400	424.0	254.0	0.030	33.4	-390.6		
Unit 866-12H1 <sup>1</sup>	43.0	0.113	21.3	61.2	0.113	30.3	9.0		
Total Target Heater NO <sub>x</sub> RACT Reduction (TPY)									

 $<sup>^{1}</sup>$  Note that Unit 865-11H2 and Unit 866-12H1 are currently complying with the presumptive RACT limits and do not have oil firing NO<sub>x</sub> emission limits. Conservatively, the proposed gas firing NO<sub>x</sub> emission limit of 0.113 lb/MMBtu was assumed as the oil firing emission limit for this analysis.

Table 1-4 Summary of RACT Plan Approval Revisions

Section	Revisions Requested
Section 1.A(2)	Revise firing duty of Unit 231-B101 to 104.5 MMBtu/hr.
Section 1.A(11)	Revise firing duty of Unit 210-H101 to 192 MMBtu/hr. Revise firing duty of Unit 210-H201 to 254 MMBtu/hr. Revise the section to remove the firing of refinery fuel oil.
Section 1.A(15)	Revise firing duty of Unit 865-11H1 to 87.3 MMBtu/hr. Revise firing duty of Unit 865-11H2 to 64.2 MMBtu/hr. Revise the section to remove the firing of refinery fuel oil.
Section 1.A(16)	Revise firing duty of Unit 866-12H1 to 61.2 MMBtu/hr. Revise the section to remove the firing of refinery fuel oil.
Section 1.A(19)	Revise firing duty of Unit 868-8H101 to 60.0 MMBtu/hr.
Section 1.B(1)	Add control technology for Unit 210-H201 (ultra-low NO <sub>x</sub> burners).
Section 2.A	Add description that ultra-low $NO_x$ burners are planned to be installed on Unit 231-B101 and Unit 865-11H1. Installation will be completed after issuance of plan approval.
Section 2.B	Include combustion tuning as RACT for Unit 865-11H2 and Unit 868-8H101.
Section 2.C	Removal of the heat input caps (MMBtu/hr) for Unit 231-B101 and Unit 210-H201.
New paragraph in Section 2	Add control technologies for Unit 210-H101 (low NO <sub>x</sub> burners) and Unit 210-H201 (ultra-low NO <sub>x</sub> burners).
New paragraph in Section 3	Add description that original RACT limits apply until the installation of ultra-low NO <sub>x</sub> burners on Unit 231-B101 and Unit 865-11H1.
Section 4.B	Add description that $NO_x$ RACT emissions limit for Unit 210-H201 has been established using CEMS.
Section 4.C	Removal of Unit 231-B101 and Unit 865-11H1 Heaters from the table as compliance will be demonstrated through performance testing.
Section 4.C	Updates to add $NO_x$ emission rate for Unit 865-11H2, Unit 866-12H1, and Unit 868-8H101.
Section 4.C	Updates to $NO_x$ emission rate for Unit 210-H201 Heater and removing refinery fuel oil firing $NO_x$ emission limitations for Unit 210-H101 and Unit 210-H201.

#### 1.3 RACT COST EFFECTIVENESS CALCULATIONS

In this application, the cost effectiveness calculations for the RACT analyses were based on the EPA guidance document entitled *Alternative Control Techniques Document - NO<sub>x</sub> Emissions from Process Heaters (Revised) -* EPA-453/R-93-034. PES also used cost information from past Refinery ULNB installations on two heaters (Unit 1332 H-400/H-401 Heater and Unit 137 F-3 Heater). These costs – capital and operation and maintenance (O&M) – were scaled up to 2012 dollar amounts using *Chemical* 

*Engineering* cost indices. PES has also conducted the analysis at the current cost of borrowing capital.

As PES is a recently established company under new ownership in a private equity structure, the cost of borrowing capital (the minimum return that investors expect for providing capital to the company) is considered at a higher risk than many established companies. The cost effectiveness analysis reflects the current cost of capital for PES, which is 21.83%.

#### 1.4 RACT ANALYSIS RESULTS

The RACT cost effectiveness for the subject heaters are calculated at approximately \$6,700 to \$163,000 per ton of NO<sub>x</sub> emissions reductions for additional controls beyond those considered part of current heater design and operation. The RACT analysis leads to the following conclusions:

- The Unit 210-H101 Heater already has LNB installed<sup>4</sup>; however, the installation of current generation UNLB is not cost effective.
- Unit 210-H201 has NO<sub>x</sub> control today at a permit limit of 0.03 lb/MMBtu, and no further control is deemed to be cost effective as indicated by the RACT analysis.
- With the planned installations of ULNBs on Unit 231-B101 and Unit 865-11H1, as indicated by the RACT analysis, no other control technologies are found to be cost effective.
- As illustrated in Appendix A, for the remaining heaters, additional retrofit NO<sub>x</sub> control options beyond combustion tuning are not cost effective. Therefore, combustion tuning is RACT for these heaters.

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<sup>&</sup>lt;sup>4</sup> Burners were considered UNLB when installed, but referred to here as LNB to avoid confusion.

#### 2.0 RACT PLAN APPROVAL PROPOSED CONDITIONS

Based on this RACT analysis, including the RACT cost effectiveness analysis completed in Appendix A, PES is proposing RACT for the seven target heaters as described below. Table 2-1 at the end of this section shows the existing and proposed RACT Plan Approval limits.

# 2.1 RACT CONTROL EQUIPMENT REQUIREMENTS

Combustion tuning will be RACT for the following heaters: Unit 231-B101 Heater, Unit 865-11H1 Heater, Unit 865-11H2 Heater; Unit 210-H101 Heater; Unit 210 H-201 Heater; Unit 866-12H1 Heater; and Unit 868-8H101 Heater as well as compliance with the RACT  $NO_x$  emission rate limit for each heater listed in Table 2-1.

#### 2.2 RACT IMPLEMENTATION SCHEDULE

Sources in Table 2-1 below proposing combustion tuning to comply with RACT requirements of 25 PA Code 129.91(f) shall perform quarterly combustion tuning.

# 2.3 RACT TESTING REQUIREMENTS AND STACK EMISSION LIMITATIONS

After installation of the ULNB on the Unit 231-B101 and Unit 865-11H1 Heaters, PES shall conduct a one-time performance tests for  $NO_x$ . The results of these tests will be submitted to AMS.

The final NO<sub>x</sub> RACT emission limits for the Unit 210-H201 Heater shall be established through the use of the Department-approved Continuous Emission Monitoring System (CEMS) currently installed. Compliance with the limitation listed in Table 2-1 below for Unit 210-H201 will be on a 365-day rolling average based on hourly averages of CEM data.

Compliance with emission limits for the Unit 210-H101, Unit 865-11H2, Unit 866-12H1, and Unit 868-8H101 Heaters shall be determined by quarterly stack sampling with a portable  $NO_x$  analyzer. After one year sampling, PES may petition AMS for semi-annual monitoring.

All annual combustion tuning shall at a minimum meet the requirements set forth in 25 PA Code 129.93 (b)(2) through (5).

At least thirty (30) days prior to a performance  $NO_x$  test, PES shall inform AMS of the date and time of the scheduled test.

# 2.4 RACT RECORDKEEPING AND REPORTING REQUIREMENTS

PES shall maintain a file containing all the records and other data that are required to be collected to demonstrate compliance with  $NO_x$  RACT requirements of 25 PA Code 129.91- 129.94.

The records shall provide sufficient data and calculations to clearly demonstrate that the requirements of §129.91-129.94 are met.

Data or information required to determine compliance shall be recorded and maintained in a time frame consistent with the averaging period of the requirement.

Records shall be retained for at least two years and shall be made available to the Department on request.

Table 2-1 RACT Plan Approval Existing and Proposed Limits

Unit	Existing		Emissio	n Rate Lin	RACT Control			
	Hourly Firing Limit	Design Firing (MMBtu/hr)	Existing <sup>3</sup>		Proposed 4			
	(MMBtu/hr) <sup>2</sup>	(MIMBLWIII)	Gas	Oil	Gas	Oil	Existing	Proposed
Unit 231-B101	91	104.5	0.122	-	0.03	-	Tuning	Tuning 5
Unit 865-11H1	72.2	87.3	0.113	0.400	0.03	-	Tuning	Tuning 5
Unit 865-11H2 <sup>1</sup>	49.9	64.2	-	-	0.113	-	-	Tuning
Unit 210-H101	183	192.0	0.089	0.400	0.089	-	Tuning	Tuning 6
Unit 210-H201	242	254.0	0.173	0.400	0.03	-	Tuning	Tuning 6
Unit 866-12H1 <sup>1</sup>	43	61.2	-	-	0.113	-	-	Tuning
Unit 868-8H101 <sup>1</sup>	49.5	60.0	-	-	0.113	-	-	Tuning

<sup>&</sup>lt;sup>1</sup> Units are currently subject to PADEP's presumptive RACT and not subject to specific requirements in the RACT Plan Approval.

<sup>&</sup>lt;sup>2</sup> Compliance with limitation is based on the daily average heat input.

<sup>&</sup>lt;sup>3</sup> Compliance with limitation is based on quarterly stack sampling using a portable NO<sub>x</sub> analyzer.

<sup>&</sup>lt;sup>4</sup> The Refinery is only proposing limits for firing natural gas at the target heaters. The Refinery no longer uses refinery fuel oil as a fuel for the Unit 865-11H1, Unit 210-H101, and Unit 210-H201 heaters and proposes to remove the capability to use refinery fuel oil as a fuel from the RACT Plan Approval. For Unit 210-H201, compliance with the emission rate limit will be through the use of Department-approved CEMS currently installed. For heaters other than Unit 210-H201, compliance with limitation is based on quarterly stack sampling using a portable NO<sub>x</sub> analyzer.

<sup>&</sup>lt;sup>5</sup> PES is proposing that the current RACT Plan Approval conditions remain in place and the hourly firing rate limits can only be removed after the installation and testing of the ULNBs at Unit 231-B101 and Unit 865-11H1.

<sup>&</sup>lt;sup>6</sup> Control equipment is currently installed; however only combustion tuning is currently required as RACT control for these units in the RACT Plan Approval. The proposed emission rate limits also reflect the presence of control equipment.



# CITY OF PHILADELPHIA DEPARTMENT OF PUBLIC HEALTH AIR MANAGEMENT SERVICES

#### RACT PLAN APPROVAL

Effective Date: August 1, 2000

Amended Date: October 7, 2002

**Expiration Date: None** 

Replaces Permit No. None

These amendments will update RACT requirements for sources affected in the Heater Firing Rate Increase Plan Approval.

In accordance with provisions of the Air Pollution Control Act, the Act of January 8, 1960, P.L. 2119, as amended, and after due consideration of a Reasonably Available Control Technology (RACT) proposal received under the Pennsylvania Code, Title 25, Chapter 129.91 thru 129.95, of the rules and regulations of the Pennsylvania Department of Environmental Protection (PADEP), Air Management Services (AMS) amended the RACT Plan Approval of the Facility below for the source(s) listed in section 1.A. Emission Sources of the attached RACT Plan Approval.

Facility: Sunoco, Inc. (R & M)

Owner: Sunoco, Inc.

Location: Girard Point Processing Area located at 3001 Penrose Ave

Point Breeze Processing Area located at 3144 Passyunk Ave

Mailing Address: 3144 Passyunk Ave., Philadelphia, PA 19145

SIC Code(s): 2911

Plant ID: 1501 and 1517

Facility Contact: Eric Schneider
Phone: (215) 339-2091

Permit Contact: Eric Schneider,
Phone: (215) 339-2091

Responsible Official: Vincent J. Kelley
Title: Refinery Manager

Edward Braun, Chief of Source Registration

Date

The RACT plan approval is subject to the following conditions:

1. The purpose of this Plan Approval is to establish Nitrogen Oxides (NOx)/Volatile Organic Compound (VOC) Reasonably Available Control Technology (RACT) for Sunoco, Inc. (R&M) Girard Point Processing Area and Point Breeze Processing Area. This includes the following emission sources and control equipment:

#### A. Emission Sources

(1) Process Heaters: Unit 137: F1 heater (415 MMBTU/hr)

F2 heater (155 MMBTU/hr) F3 heater (60 MMBTU/hr)

Process heaters F1 and F2 burn refinery fuel gas or refinery fuel oil. Heater F3 burns refinery fuel oil.

(2) Process Heater: Unit 231: B-101 heater (94 MMBTU/hr) Heater fires refinery fuel gas.

(3) Process Heater: Unit 433: H-1 heater (243 MMBTU/hr) Heater fires refinery fuel gas.

(4) Process Heaters: Unit 1332: H-400 heater (186 MMBTU/hr)

H-401 heater (233 MMBTU/hr) H-600 heater (21.3 MMBTU/hr) H-601 heater (48 MMBTU/hr) H-602 heater (49 MMBTU/hr) H-1 heater (45 MMBTU/hr) H-2 heater (60 MMBTU/hr) H-3 heater (43 MMBTU/hr)

These heaters burn refinery fuel gas.

- (5) Process Heater: Unit 1232: B-104 heater (70 MMBTU/hr) Heater fires refinery fuel gas.
- (6) Boiler House #3: Boiler #37 (495 MMBTU/hr)

Boiler #38 (495 MMBTU/hr) Boiler #39 (495 MMBTU/hr) Boiler #40 (660 MMBTU/hr)

These boilers fire refinery fuel gas or refinery fuel oil.

- (7) Sludge Incinerator 8832: Unit was 44 MMBTU/hr and burned refinery fuel gas or refinery fuel oil.
- (8) Sulfur Recovery Unit 532: SO2 incinerator was 16 MMBTU/hr. Unit burned refinery fuel gas.
- (9) 1232 FCCU CO Boiler: CO waste gas combustion unit (580 MMBTU/hr) burns process waste gas, refinery fuel gas and refinery fuel oil.
- (10) Asphalt Heater: H1 (12.8 MMBTU/hr)

H2 (12.8 MMBTU/hr) H3 (12.8 MMBTU/hr) H5 (12.8 MMBTU/hr)

These heaters burned fire refinery fuel gas.

(11) Crude Unit 210: Section A HTR H101 (183 MMBTU/hr)

Section B HTR H201 (242 MMBTU/hr) Section C HTR 13H1 (235.4 MMBTU/hr)

These heaters above fire refinery fuel gas and refinery fuel oil.

(12) Hydrocracker Unit 859: HTR 1H1 (76 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil.

HTR 1H2 (70 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. HTR 1H3 (211 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil.

HTR 1H4 (19 MMBTU/hr) Unit fires refinery fuel gas.

(13) Reformer Unit 864: HTR PH3 (80 MMBTU/hr)

HTR PH5 (90 MMBTU/hr)
HTR PH1 (80 MMBTU/hr)
HTR PH2 (45 MMBTU/hr)
HTR PH4 (57 MMBTU/hr)
HTR PH7 (45.5 MMBTU/hr)
HTR PH11 (74 MMBTU/hr)
HTR PH12 (85.1 MMBTU/hr)

These heaters fire refinery fuel gas and refinery fuel oil.

(14) Hydrogen Plant 861: HTR 3H1S (123 MMBTU/hr)

HTR 3H1N (125 MMBTU/hr)

These heaters burned refinery fuel gas.

(15) Distillate HDS Unit 865: HTR 11H1 (72.2 MMBTU/hr)

HTR 11H2 (49.9 MMBTU/hr)

These heaters fire refinery fuel gas and refinery fuel oil.

(16) Gas Oil HDS Unit 866: HTR 12H1(43 MMBTU/hr) Heater fires refinery fuel gas and refinery fuel oil.

(17) 22 Boiler House: Boiler #1 (169 MMBTU/hr)

Boiler #2 (169 MMBTU/hr) Boiler #3 (203 MMBTU/hr)

These three boilers burn only refinery fuel gas or natural gas and are equipped with Ultra Low NOx Burners.

(18) Reformer Unit 860: HTR 2H3 (174.67 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil.

HTR 2H5 (155 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. HTR 2H1 (49 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. HTR 2H2 (69.78 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. HTR 2H4 (99.44 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. HTR 2H6 (36.7 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. HTR 2H7 (59 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. HTR 2H8 (49.6 MMBTU/hr) Unit fires refinery fuel gas and refinery fuel oil. Boiler 2H9 (165 MMBTU/hr) Unit fires refinery fuel gas or natural gas.

- (19) 868 FCCU HTR 8H101 (47.92 MMBTU/hr) Unit fires refinery fuel gas.
- (20) 868 FCCU Catalyst Regenerator
- (21) 867 Sulfur Recovery Unit Incinerator
- (22) Emergency Flares
- (23) Cooling towers
- (24) Fugitive leaks: valves, flanges, compressors, pumps, pipes.
- B. Control Equipment

(1) Ultra-low NOx burner (ULNB) systems are installed on the following sources to control NOx emissions:

Unit 433 H-1 heater Unit 1232 B-104 heater

#3 Boiler House boilers #37, #38, #39, and #40.

Unit 210-H201

2. This approval requires and authorizes:

A. The installation of the Ultra Low NOx Burners on 433 H-1 heater, 1232 B-104 heater, and #3 Boiler House boilers #37, #38, #39, and #40 to comply with RACT requirements. The installation of the burners has been completed.

B. Sunoco will use combustion tuning to comply with RACT requirements for the following heaters:

Unit 137: F1 heater, F2 heater, F3 heater

Unit 231: B-101 heater

Unit 1332: H-400 heater, H-401 heater, H-2 heater

Crude Unit: 210A HTR H101, 210B HTR H201, 210C HTR 13H1

Hydrocracker Unit 859: HTR 1H1, HTR 1H2, HTR 1H3

Reformer Unit 864: HTR PH3, HTR PH5, HTR PH1, HTR PH2, HTR PH4, HTR PH11, HTR PH12

Hydrogen Plant 861: HTR 3H1S, HTR 3H1N

Distillate HDS Unit 865: HTR 11H1

Reformer Unit 860: HTR 2H3, HTR 2H5, HTR 2H4, HTR 2H2, HTR 2H7

Gas Oil HDS Unit 866: HTR 12H1(43 MMBTU/hr)

Distillate HDS Unit 865: HTR 11H2 and HDS Unit 868: HTR 8H101

lapproval.

Add description that ultra-low NOx burners

B101 and Unit 865-11H1. Installation will

are planned to be installed on Unit 231-

be completed after issuance of plan

C. All fuel burning sources will be capped at the heat input specified in the table below. If Sunoeo desires to raise the cap, a RACT evaluation will have to be performed at that new heat input. The economic evaluation will be made using cost of living increases. Changes will require a resubmission as revision to the PA State Implementation Plan. The applicant shall bear the cost of public hearing and notification required for EPA approval as stipulated in 25 PA Code §129.9(h). Modifications or changes may require additional controls or more strict emission limits depending on the applicable regulation triggered as a result of the modification or change.

		Heat Input
Process Unit	Source	Cap (MMBTU/hr)
Unit 137:	F1 heater	415
	F2 heater	155
<del>Unit 231:</del>	B-101 heater	91
Unit 433:	H-1 heater	243
Unit 1332:	H-400 heater	186
Unit 1232:	B-104 heater	70
Boiler House #3:	Boilers #37, #38, #39	495
	Boiler #40	660
Crude Unit 210B:	HTR H201	242
Hydrocracker Unit 859:	HTR 1H1	76
	HTR 1H2	70
Reformer Unit 864:	HTR PH3	80
	HTR PH5	90
	HTR PH2	45
	HTR PH4	57
Hydrogen Plant 861:	HTR 3H1S	123
	HTR 3HIN	125

D. Sunoco shall monitor all fuel input to all heaters and boilers with BTU limitations on a daily basis to insure capacity limits are not exceeded or sun shall install fuel limiting devices on the heaters or boilers to keep capacities below allowable. The compliance method must be in place by June 30<sup>th</sup> 2000.

E. All fuel combustion sources with heat input equal to or greater than 20 MMBTU/hr and less than 50 MMBTU/hr shall comply with applicable presumptive RACT requirements of 25 PA Code 129.93(b)(2)-(5). All fuel combustion sources with heat input less than 20 MMBTU/hr shall comply with presumptive RACT requirements of 25 PA Code 129.93(c).

- F. RACT for 22 Boiler House: Boiler #1, Boiler #2, and Boiler #3 is combustion tuning.
- G. RACT for Reformer Unit 860 HTR 2H9 is combustion tuning.
- H. The 868 FCCU NOx emissions shall be limited to 569 tons per year calculated on a 365 day rolling average basis. Sun shall follow good combustion practices controlling the level of excess oxygen and CO promoter in the regenerator to minimize NOx emissions from the regenerator.
- J. Sunoco shall utilize an inspection and maintenance/monitoring program for VOC fugitive emissions from cooling towers.
- K. Sunoco shall utilize a fugitive emissions leak detection and repair program (LDAR) for all valves, pumps, flanges, and compressors in VOC service. All applicable equipment shall be tagged by May 31, 1995. Monitoring of components shall begin by July 31, 1995 and shall be conducted on a quarterly basis (gaseous service) and an annual basis (liquid service) for all sources not covered under an existing LDAR program.
- L. The 1232 FCCU CO Boiler: CO waste gas combustion unit (580 MMBTU/hr) shall comply with the presumptive RACT requirements of 25 PA Code 129.93(c)(4), which is installation, maintenance and operation of the source in accordance with manufacturers specifications.

#### 3. RACT Implementation Schedule

Add control technologies for Unit 210-H101 (low NOx burners) and Unit 210-H201 (ultra-low NOx burners).

- A. Upon issuance of this approval, Sunoco, Inc. (R&M), Inc. shall begin immediate implementation of the measures necessary to comply with the approved RACT proposal.
- B. Sources proposing combustion tuning to comply with RACT requirements of 25 PA Code 129.91(f) shall perform the annual combustion tuning by December 31st of each year not to exceed 12 months between tunings.
- C. Sources applicable to presumptive RACT requirements of 25 PA Code 129.93(b)(2) shall complete the annual adjustment or tune-up by December 31<sup>st</sup> of each year not to exceed 12 months between tunings.
- D. Sources proposing installing Ultra Low NOx Burners to comply with RACT requirements of 25 PA Code 129.91(f) shall perform combustion tuning annually by Decem Add description that original RACT limits apply until the
- 4. Testing Requirements and Stack Emission Limitations

installation of ultra-low NOx burners on Unit 231-B101 and Unit 865-11H1.

- A. For units installing ULNB, Sunoco shall conduct performance tests for NOx. The results of these tests have been submitted to AMS.
- B. The final NOx RACT emission limits for the #3 Boiler House boilers, 137 Unit F1 heater, #22 Boiler House boilers: #1, 2, & 3 and the 860 unit Boiler 2H9 have been established through the use of Department approved Continuous Emission Monitoring System (CEMS). Compliance with the limitation listed below will be on a 30 day rolling average based on hourly averages of CEM data.

Source	Limitation
Boiler House #3 – boilers #37, #38, #39, and #40	0.330 lbs. NOx/MMBTU
137 Unit F1 heater	0.230 lbs. NOx/MMBTU
Reformer Unit 860 Boiler 2H9	0.20 lbs. NOx/MMBTU
#22 Boiler House – boilers #1, #2, and #3	0.20 lbs. NOx/MMBTU

C. Compliance with emission limits for combustion sources listed below shall be determined by quarterly stack sampling with a portable NOx analyzer. After one year sampling, Sunoco may petition AMS for semi-annual monitoring. AMS may, at any time, require three one-hour stack tests per fuel type for each unit where fuels can be fired separately. AMS may, at any time, require three one-hour stack tests for dual-fuel type combustion sources where

Add description that NOx RACT emission limit for Unit 210-H201 has been established based on a rolling 365-day average using CEMS.

both fuels must be fired at the same time and compliance with emission limits will be through the use of one set of three one-hour stack tests.

	Limitation (lbs	. NOx/MMBTU)
Source	Gas	Oil
Process Heater Unit 433 H-1 heater	0.060	N/A
Process Heater Unit 1332 H-400 heater	0.156	N/A
Process Heater Unit 1332 H-401 heater	0.156	N/A
Crude Unit 210A HTR H101	0.089	0.4
Crude Unit 210B HTR H201	0.173	0.4
Crude Unit 210C HTR 13H1	0.104	0.4
Hydrocracker Unit 859 HTR 1H3	0.134	0.4
Hydrogen Plant 861 HTR3H1S	0.133	N/A
Hydrogen Plant 861 HTR3H1N	0.133	N/A
F-2 @ 137 Unit	0.257	0.4
F-3 @ 137 Unit	N/A	0.4
B-101@ 231 Unit	0.122	N/A
H-2 @ 1332 Unit	0.300	N/A
B-104 @ 1232 Unit	0.177	N/A
1H-1 @ 859 Unit	0.123	0.4
1H-2 @ 859 Unit	0.123	0.4
PH-3 @ 864 Unit	0.284	0.4
PH-5 @ 864 Unit	0.283	0.4
PH-1 @ 864 Unit	0.167	0.4
PH-4 @ 864 Unit	0.102	0.4
PH-11 @ 864 Unit	0.145	0.4
PH-12 @ 864 Unit	0.119	0.4
11H-1 @ 865 Unit	0.113	0.4
2H-3 @ 860 Unit	0.163	0.4
2H-5 @ 860 Unit	0.163	0.4
2H-2 @ 860 Unit	0.350	0.4
2H-4 @ 860 Unit	0.270	0.4
2H-7 @ 860 Unit	0.157	0.4

Add NOx emission rate for Unit 865-11H2, Unit 866-12H1, and Unit 868-8H101

- D. All annual combustion tuning shall at a minimum meet the requirements set forth in 129.93 (b)(2) through (5).
- E. At least thirty (30) days prior to a performance NOx test, Sunoco shall inform AMS of the date and time of the scheduled test.

#### 5. Recordkeeping and Reporting Requirements

- A. The permittee shall maintain a file containing all the records and other data that are required to be collected to demonstrate compliance with NOx/VOC RACT requirements of 25 PA Code 129.91 129.94.
- B. The records shall provide sufficient data and calculations to clearly demonstrate that the requirements of §129.91-129.94 are met.
- C. Data or information required to determine compliance shall be recorded and maintained in a time frame consistent with the averaging period of the requirement.
- D. Records shall be retained for at least two years and shall be made available to the Department on request.
- 6. The operation of the aforementioned sources shall not at any time result in the emission of visible air contaminants in excess of the limitations specified in Section 123.41, particulate matter in excess of the limitations specified in Section 123.11 or sulfur oxides in excess of the limitations specified in Section 123.22, all Sections of Chapter 123 of Article III of the Rules and Regulations of the Department of Environmental Resources, or in the emission of any of these or any

other type of air contaminant in excess of the limitations specified in, or established pursuant to, any other applicable rule or regulation contained in Article III.

- 7. The company shall not impose conditions upon or otherwise restrict the Department's access to the aforementioned source(s) and/or any associated air cleaning device(s) and shall allow the Department to have access at any time to said source(s) and associated air cleaning device(s) with such measuring and recording equipment, including equipment recording visual observations, as the Department deems necessary and proper for performing its duties and for the effective enforcement of the Air Pollution Control Act.
- 8. Revisions to any emission limitations incorporated in this RACT Approval will require resubmission as revision to the PA State Implementation Plan. The applicant shall bear the cost of public hearing and notification required for EPA approval as stipulated in 25 PA Code §129.9(h).

Appendix A RACT Cost Effectiveness Analysis

#### NOx RACT Control Cost Effectiveness Cost Effectiveness Summary

Control Option		Cost Effectiveness (\$/Ton)								
	Unit 231-B101	Unit 865-11H1	Unit 865-11H2	Unit 210-H101	Unit 210-H201	Unit 866-12H1	Unit 868-8H101			
ULNB & SCR	NA	NA	34,287	30,796	NA	34,831	35,060			
SCR	102,243	NA	32,909	27,397	NA	33,524	33,782			
ULNB	NA	NA	6,737	9,477	NA	6,737	6,737			
LNB & SNCR	NA	NA	11,045	57,667	162,271	11,331	14,513			
LNB & FGR	NA	NA	8,704	NA	NA	8,960	12,965			
SNCR	39,924	42,874	13,132	10,825	28,098	13,379	13,482			

Assumptions for all heaters:

Number of Years (n)	10
Interest Rate, % (i)	21.83
Annualized Cost Factor (ACF)	0.253

Based on 90% equity cost of the average Carlyle energy funds and 10% after tax debt cost.

$$ACF = \frac{i(1+i)^n}{(1+i)^n - 1}$$

EPA Air Pollution Control Cost Manual, Sixth Edition, EPA/452/B-02-001 - Equation 2.8a

Year	Chemical Engineering Cost Index
1986	318.4
1991	361
2012	582.2
Cost Escalation Factor for SCR <sup>1</sup>	1.83
Cost Escalation Factor for LNB, SNCR, and FGR <sup>2</sup>	1.61

 $^1$  Cost data from Alternative Control Techniques Document -  $NO_x$  Emissions from Process Heaters (Revised) - EPA-453/R-93-034 scaled from 1986 to 2012 costs using the Cost Escalation Factor.

 $^2$  Cost data from Alternative Control Techniques Document - NO  $_x$  Emissions from Process Heaters (Revised) - EPA-453/R-93-034 scaled from 1991 to 2012 costs using the Cost Escalation Factor.

Source		Control Efficiency	Comment
Ultra low-NO <sub>x</sub> burners and Selective Catalytic Reduction	ULNB & SCR	96%	Combining both removal efficiencies of ULNB and SCR.
Selective Catalytic Reduction	SCR	85%	Based on Unit 1332 performance.
Ultra low-NO <sub>x</sub> burners	ULNB	66 to 87%	Based on vendor experience at 0.03 lb/MMBtu.
Low-NO <sub>x</sub> burners and Selective Non- Catalytic Reduction	LNB & SNCR	70%	Combining both removal efficiencies. Assumes 50% control efficiency for LNB and 40% control efficiency for SNCR. Alternative Control Techniques Document - $NO_x$ Emissions from Process Heaters (Revised) - EPA-453/R-93-034.
Low-NO <sub>x</sub> burners and Flue Gas Recirculation	LNB & FGR	55%	$Alternative\ Control\ Techniques\ Document\ -\ NO_x\ Emissions\ from\ Process\ Heaters\ (Revised)\ -\ EPA-453/R-93-034.$
Selective Non-Catalytic Reduction	SNCR	40%	Heater stack temperature below 700°F results in low $NO_x$ removal efficiency. EPA Air Pollution Control Technology Fact Sheet - EPA-452/F-03-031.

Source Name	Design Capacity (MMBtu/hr)	NO <sub>x</sub> Emission Rate (lb/MMBtu)	Number of Burners	Summary of Technical Infeasibilities for NO <sub>x</sub> Control
Unit 231-B101	104.5	0.030	26	None.
Unit 865-11H1	87.3	0.030	8	SCR would not physically fit the plot space and there is not adequate pressure to overcome the SCR pressure drop; therefore, SCR is infeasible. FGR installation would require the installation of mechanical draft burners, which is a major re-design of the unit; therefore FGR is infeasible.
Unit 865-11H2	64.2	0.113	8	None.
Unit 210-H101	192.0	0.089	6	FGR would not physically fit the plot space; therefore, it is infeasible.
Unit 210-H201	254.0	0.030	8	SCR would not physically fit the plot space and there is not adequate pressure to overcome the SCR pressure drop; therefore, SCR is infeasible. FGR installation would require the installation of mechanical draft burners, which is a major re-design of the unit; therefore FGR is infeasible.
Unit 866-12H1	61.2	0.113	6	None.
Unit 868-8H101	60.0	0.113	4	None.

#### PES Refinery

#### Heater Firing Rate Increase Plan Approval

#### NOx RACT Control Cost Effectiveness

Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034 All costs are scaled from 2012 U.S. dollars using the appropriate Cost Escalation Factor.

#### Capital Cost of Low NO<sub>x</sub> Burners (page 6-4 and 6-5):

$$TCI = 30,000 + HQ[5,230 - (622 \times BQ) + (26.1 \times BQ^2)]$$

Where:

TCI = Total Capital Investment

HQ = heater capacity (GJ/hr)

BQ = burner heat release rate (GJ/hr)

 $BO = HO/NB \times (1.158 + 8/HO)$ 

NB = number of burners

#### Capital Cost of Ultra-low NOx Burners:

See the "Refinery ULNB Control Costs" tab for capital cost details for Ultra-low NO<sub>x</sub> Burners

#### Capital Cost of Selective Non-Catalytic Reduction (page 6-7):

$$TCI = 31,850(HQ)^{0.6}$$

HQ = heater capacity (GJ/hr)

#### Operating Cost of Selective Non-Catalytic Reduction (page 6-8):

Where:

Q = heater capacity, MMBtu/hr

$$Electricty\ cost = \left(\frac{0.3\ kWh}{ton\ NH_3}\right) \times \left(\frac{ton\ NH_3}{year}\right) \times \left(\frac{\$0.06}{kWh}\right)$$

Where

$$\frac{ton\ NH_3}{year} = Q\ \times\ (lb\ NO_x/MMBtu) \times \left(\frac{1\ mole\ NO_x}{46\ lb\ NO_x}\right) \times \left(\frac{17\ lb\ NH_3}{1\ mole\ NH_3}\right) \times \left(\frac{1\ mole\ NH_3}{1\ mole\ NO_x}\right) \times \left(\frac{ton}{2000\ lb}\right) \times \left(8,760\ \frac{hours}{year}\right) \times \left(\frac{10\ nole\ NH_3}{10\ nole\ NH_3}\right) \times \left(\frac{10\ nole\ NH_3}{10\ nole\ NO_x}\right) \times \left(\frac{10\ nole\ NH_3}{10\ nole\ NH_3}\right) \times \left(\frac{10\ nole\ NH_3}{10\ nole\ NH_3}$$

#### Capital Cost of Selective Catalytic Reduction (page 6-8):

$$TCI = 1,373,000 \times \left(\frac{Q}{48.5}\right)^{0.6} + 49,000 \times \left(\frac{Q}{485}\right)$$

Where:

Q = heater capacity, MMBtu/hr

#### Operating Cost of Selective Catalytic Reduction (page 6-9):

$$NH_{3} \ cost = Q \times (lb/MMBtu) \times \left(\frac{1 \ mole \ NO_{x}}{46 \ lb \ NO_{x}}\right) \times \left(\frac{17 \ lb \ NH_{3}}{1 \ mole \ NH_{3}}\right) \times \left(\frac{1 \ mole \ NH_{3}}{1 \ mole \ NO_{x}}\right) \times \left(\frac{\$0.125}{lb \ NH_{3}}\right) \times \left(\frac{8,760 \ hours}{year}\right)$$

Where:

Q = heater capacity, MMBtu/hr

Note the capacity factor has been assumed to be equal to 1; therefore, the capacity factor term has been omitted

Catalyst Replacement Cost = 
$$49,000 \times \frac{Q}{48.5} / 5$$
 years

$$Electricty \ cost = \ \left(\frac{0.3 \ kWh}{ton \ NH_3}\right) \times \left(\frac{ton \ NH_3}{year}\right) \times \left(\frac{\$0.06}{kWh}\right)$$

Where

$$\frac{ton \ NH_3}{year} = Q \ \times \ (lb \ NO_x/MMBtu) \times \left(\frac{1 \ mole \ NO_x}{46 \ lb \ NO_x}\right) \times \left(\frac{17 \ lb \ NH_3}{1 \ mole \ NH_3}\right) \times \left(\frac{1 \ mole \ NH_3}{1 \ mole \ NO_x}\right) \times \left(\frac{ton}{2000 \ lb}\right) \times \left(8,760 \frac{hours}{year}\right) \times \left(\frac{10 \ NH_3}{1 \ mole \ NH_3}\right) \times \left(\frac{10 \ NH_3}{1 \ mole \ NH_3}\right)$$

#### Capital Cost of Flue Gas Recirculation (page 6-9):

$$TCI = 12,800(HQ)^{0.6}$$

Where:

HQ = heater capacity (GJ/hr)

#### Operating Cost of Flue Gas Recirculation (page 6-10):

$$Electricty\ cost =\ (motor\ hp) \times \left(\frac{0.75\ kW}{hp}\right) \times \left(\frac{8,760\ hours}{year}\right) \times \left(\frac{\$0.06}{kWh}\right)$$

Where:

motor hp = FGR fan motor horsepower,  $(1/5) \times (Q)$ 

Q = heater capacity, MMBtu/hr

# PES Refinery Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Ultra Low NO<sub>x</sub> Burner Costs - from PES Refinery Project Experience

Economic Data	Heater Fired Duty (MMBtu/hr)	Number of Burners	Burner Heat Release (MMBtu/hr/burner)	Base Year ULNB Cost (\$/burner)	Normalized Cost (\$/MMBtu/hr)
1332 H-400/H-401 Heater	419	54	7.8	\$50,000	\$6,444
137 F-3 Heater	60	4	15	\$80,500	\$5,367
				Average	\$5,905

Source Name	Design Capacity (MMBtu/hr)	ULNB Capital Cost Using (\$/MMBtu/hr)	ULNB Total Capital Investment
Unit 231-B101	104.5	\$617,103	NA
Unit 865-11H1	87.3	\$515,532	NA
Unit 865-11H2	64.2	\$379,120	\$559,581
Unit 210-H101	192.0	\$1,133,816	\$1,673,512
Unit 210-H201	254.0	\$1,499,944	NA
Unit 866-12H1	61.2	\$361,404	\$533,432
Unit 868-8H101	60.0	\$354,317	\$522,973

#### PES Refinery Heater Firing Rate Increase Plan Approval Unit 231-B101 RACT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	Design Firing (MMBtu/hr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ Design Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized  Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	104.5	0.03	13.7	96%	0.5	13.2	NA	NA	NA	NA
SCR	104.5	0.03	13.7	85%	2.1	11.7	4,118,447	149,357	1,193,342	102,243
LNB & SNCR	104.5	0.03	13.7	70%	4.1	9.6	NA	NA	NA	NA
LNB & FGR	104.5	0.03	13.7	55%	6.2	7.6	NA	NA	NA	NA
SNCR	104.5	0.03	13.7	40%	8.2	5.5	773,123	23,307	219,286	39,924
ULNB	104.5	0.03	13.7	0%	13.7	0.0	NA	NA	NA	NA
	Calculation		= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Notes:

<sup>&</sup>lt;sup>1</sup> ULNB are planned to be installed on the Unit 231-B101 heater and the current emission rate is assumed to be 0.03 lb/MMBtu.

<sup>&</sup>lt;sup>2</sup> See "RACT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

### **Heater Firing Rate Increase Plan Approval**

### **NOx RACT Control Cost Effectiveness**

Source	Unit 231-B101	
Control	SCR	
Rated Heat Input	104.5	MMBtu/hr
<b>Number of Burners</b>	26.0	Burners
<b>Baseline Actual Emissions</b>	13.73	tpy
<b>Current Emission Rate</b>	0.030	lb/MMBtu
Control Efficiency	85%	
Heater Capacity	110.3	GJ/hr
<b>Burner Heat Release Rate</b>	5.2	GJ/hr

### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

COST COMPONENT:	COST (\$)
DIRECT COSTS	
Purchased Equipment Costs	
Equipment Cost (EC)	3,998,493
Instrumentation (Included in above costs)	
Sales taxes (Included in above costs)	
Freight (Included in above costs)	
Subtotal - Purchased Equipment Costs (PEC)	3,998,493
Direct Installation Costs	
Foundations & supports; handling & erection; electrical; piping;	
etc.	0
Site Preparation / Buildings- Included above	<del></del>
Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TDC)	3,998,493
INDIRECT INSTALLATION COSTS	
Engineering Costs (Included in above costs)	
Construct. & Field Expenses (Included in above costs)	
Contractor Fees (Included in above costs)	
Start-up (Included in above costs)	
Performance Test (Included in above costs)	
Contingency (3% of PEC)	119,955
TOTAL INDIRECT COSTS, IC	119,955
TOTAL CAPITAL INVESTMENT (TCI)	4,118,447

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	113,257 113,257
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	2,046
Catalyst Replacement Cost	34,054
Electricity Cost	0.1
Subtotal - Utilities	36,100
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	149,357

	COST (\$)				
TOTAL ANNUAL O&M C	POSTS		149,357		
Annualized Cost Factor	$Equipment\ Life\ (years) = \\ Interest\ Rate\ (\%) = \\ Annualized\ Cost\ Factor$	10 21.83			
CAPITAL RECOVERY COS	STS TOTAL CAPITAL REQUIREMENT		4,118,447		
	TOTAL ANNUAL CAPITAL REQUIREMENT		1,043,985		
	TOTAL ANNUALIZED COST Total annual O&M cost and annualized capital cost)				

### **Heater Firing Rate Increase Plan Approval**

#### **NOx RACT Control Cost Effectiveness**

Source	Unit 231-B101	
Control	SNCR	
Rated Heat Input	104.5	MMBtu/hr
Number of Burners	26.0	Burners
<b>Baseline Actual Emissions</b>	13.73	tpy
<b>Current Emission Rate</b>	0.030	lb/MMBtu
<b>Control Efficiency</b>	40%	
Heater Capacity	110.3	GJ/hr
<b>Burner Heat Release Rate</b>	5.2	GJ/hr

## Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	750,605
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	750,605
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COS	TS (TDC)	750,605
INDIRECT INSTALLA	TION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	22,518
TOTAL INDIRECT CO	OSTS, IC	22,518
TOTAL CAPITA	L INVESTMENT (TCI)	773,123

## **Heater Firing Rate Increase Plan Approval**

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	21,261 21,261
Annualized Cost Factor  Replacement Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities Ammonia Cost Electricity Cost	2,046 0.1
Subtotal - Utilities	2,046
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	23,307

	COST (\$)			
TOTAL ANNUAL O&M	COSTS			23,307
Annualized Cost Factor	Ec	quipment Life (years) = Interest Rate (%) =	10 21.83	0.25
CAPITAL RECOVERY CO	OSTS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIRE	MENT		773,123 <b>195,979</b>
TOTAL ANNUALIZED (	219,286			

### PES Refinery Heater Firing Rate Increase Plan Approval Unit 865-11H1 RACT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	Design Firing (MMBtu/hr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ Design Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized  Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	87.3	0.03	11.5	96%	0.5	11.0	NA	NA	NA	NA
SCR	87.3	0.03	11.5	85%	1.7	9.8	NA	NA	NA	NA
LNB & SNCR	87.3	0.03	11.5	70%	3.4	8.0	NA	NA	NA	NA
LNB & FGR	87.3	0.03	11.5	55%	5.2	6.3	NA	NA	NA	NA
SNCR	87.3	0.03	11.5	40%	6.9	4.6	694,045	20,796	196,729	42,874
ULNB	87.3	0.03	11.5	0%	11.5	0.0	NA	NA	NA	NA
	Calculation	•	= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Technical Infeasibilities:

SCR would not physically fit the plot space and there is not adequate pressure to overcome the SCR pressure drop; therefore, SCR is infeasible FGR installation would require the installation of mechanical draft burners, which is a major re-design of the unit; therefore FGR is infeasible Notes:

<sup>&</sup>lt;sup>1</sup> ULNB are planned to be installed on the Unit 865-11H1 heater and the current emission rate is assumed to be 0.03 lb/MMBtu.

<sup>&</sup>lt;sup>2</sup> See "RACT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

### Heater Firing Rate Increase Plan Approval

#### **NOx RACT Control Cost Effectiveness**

Source Unit 865-11H1 Control **SNCR Rated Heat Input** 87.3 MMBtu/hr **Number of Burners Burners Baseline Actual Emissions 11.47** tpy **Current Emission Rate** 0.030 lb/MMBtu **Control Efficiency** 40% **Heater Capacity** 92.1 GJ/hr Burner Heat Release Rate 14.3 GJ/hr

### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	673,830
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	673,830
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S(TDC)	673,830
INDIRECT INSTALLAT	TION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	20,215
TOTAL INDIRECT CO	STS, IC	20,215
TOTAL CAPITAI	L INVESTMENT (TCI)	694,045

## **Heater Firing Rate Increase Plan Approval**

COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS Operation and Maintenance Labor Maintenance Labor and Materia	al (2.75% of TCI)		19,086 19,086
Annualized Cost Factor  Annualized Cost Factor	Replacement Life (years) = Interest Rate (%) =	10 21.83	0.25
Replacement cost			
Subtotal - Operation and Maintenance Labor			
Utilities Ammonia Cost Electricity Cost			1,709 0.1
Subtotal - Utilities			1,709
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>			20,796

	COST (\$)			
TOTAL ANNUAL O&M	COSTS			20,796
Annualized Cost Factor	Eq	quipment Life (years) = Interest Rate (%) =	10 21.83	0.25
CAPITAL RECOVERY CO	STS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIREM	MENT		694,045 175,933
TOTAL ANNUALIZED (	COST und annualized capital cost)			196,729

### PES Refinery Heater Firing Rate Increase Plan Approval Unit 865-11H2 RACT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	Design Firing (MMBtu/hr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ Design Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized  Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	64.2	0.113	31.8	96%	1.3	30.5	3,631,525	125,523	1,046,078	34,287
SCR	64.2	0.113	31.8	85%	4.8	27.0	3,071,944	110,135	888,841	32,909
ULNB	64.2	0.113	31.8	73%	8.4	23.3	559,581	15,388	157,237	6,737
LNB & SNCR	64.2	0.113	31.8	70%	9.5	22.2	857,483	28,316	245,679	11,045
LNB & FGR	64.2	0.113	31.8	55%	14.3	17.5	512,272	22,250	152,106	8,704
SNCR	64.2	0.113	31.8	40%	19.1	12.7	577,165	20,607	166,913	13,132
	Calculation		= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Notes:

 $<sup>^{1}</sup>$  Unit 865-11H2 is projected to be above PADEP presumptive RACT firing limits and assumed NO  $_{\rm x}$  emission rate limit of 0.113 lb/MMBtu is used.

<sup>&</sup>lt;sup>2</sup> See "RACT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

#### PES Refinery Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Source Unit 865-11H2 Control ULNB & SCR

Rated Heat Input 64.2 MMBtu/hr
Number of Burners 8.0 Burners
Baseline Actual Emissions 31.78 tpy
Current Emission Rate 0.113 lb/MBtu

Control Efficiency 96%

Heater Capacity 67.7 GJ/hr Burner Heat Release Rate 10.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - ULNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	379,120
	Instrumentation (10% of EC)	37,912
	Sales taxes (5% of EC)	18,956
	Freight (8% of EC)	30,330
	Subtotal - Purchased Equipment Costs (PEC)	466,317
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical;	
	piping; etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TD	OC) - ULNB	466,317
NDIRECT INSTALLATION		
	Engineering Costs (5% of PEC)	23,316
	Construct. & Field Expenses (Included in above costs)	16.622
	Contractor Fees (10% of PEC)	46,632
	Start-up (1% of PEC) Performance Test (1% of PEC)	4,663 4,663
	Contingency (3% of PEC)	13,990
TOTAL INDIRECT COSTS, I	TC - ULNB	93,263
DIRECT COSTS - SCR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,982,470
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	2,982,470
	Direct Installation Costs	
	Foundations & supports; handling & erection; electrical;	
	piping; etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TD	OC) - SCR	2,982,470
NDIRECT INSTALLATION	COSTS - SCR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	89,474
TOTAL INDIRECT COSTS, I	C - SCR	89,474
	VESTMENT (TCI) - ULNB	559,581
	VESTMENT (TCI) - SCR	3,071,944
TOTAL CAPITAL IN	VESTMENT (TCI)	3,631,525

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	99,867 <b>99,867</b>
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = 21.83 Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,735
Catalyst Replacement Cost	20,921
Electricity Cost	0.3
Subtotal - Utilities	25,656
TOTAL ANNUAL DIRECT COSTS*	125,523

COST COMPONENT:	COST (\$)
TOTAL ANNUAL O&M COSTS	125,523
Annualized Cost Factor  Equipment Life (years) =	10
Interest Rate (%) = 21 Annualized Cost Factor	0.25
CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT	3,631,525
TOTAL ANNUAL CAPITAL REQUIREMENT	920,555
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)	1,046,078

## **Heater Firing Rate Increase Plan Approval**

### **NOx RACT Control Cost Effectiveness**

Source	Unit 865-11H2	
Control	SCR	
Rated Heat Input	64.2	MMBtu/hr
Number of Burners	8.0	Burners
<b>Baseline Actual Emissions</b>	31.78	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
<b>Control Efficiency</b>	85%	
Heater Capacity	67.7	GJ/hr
<b>Burner Heat Release Rate</b>	10.8	GJ/hr

### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,982,470
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	2,982,470
	Direct Installation Costs Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (T	DC)	2,982,470
INDIRECT INSTALLATION	COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	89,474
TOTAL INDIRECT COSTS,	IC	89,474
TOTAL CAPITAL IN	VESTMENT (TCI)	3,071,944

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	04.470
Maintenance Labor and Material (2.75% of TCI)	84,478 84,478
	04,470
Annualized Cost Factor	
Replacement Life (years) =	10
Interest Rate (%) =	21.83
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,735
Catalyst Replacement Cost	20,921
Electricity Cost	0.3
Subtotal - Utilities	25,656
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	110,135

COST COMPONENT	:		COST (\$)
TOTAL ANNUAL O&M COSTS			110,135
Annualized Cost Factor			
	Equipment Life (years) =	10	ļ
	Interest Rate (%) =	21.83	
Annualized Cost Factor			0.25
CAPITAL RECOVERY COSTS			
TOTAL CAPITAL REQU	JIREMENT		3,071,944
TOTAL ANNUAL CAP	ITAL REQUIREMENT		778,707
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost	)		888,841

**Heater Firing Rate Increase Plan Approval** 

### **NOx RACT Control Cost Effectiveness**

Source	Unit 865-11H2	
Control	ULNB	
Rated Heat Input	64.2	MMBtu/hr
Number of Burners	8.0	Burners
<b>Baseline Actual Emissions</b>	31.78	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	73%	
<b>Heater Capacity</b>	67.7	GJ/hr
<b>Burner Heat Release Rate</b>	10.8	GJ/hr

### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	379,120
	Instrumentation (10% of EC)	37,912
	Sales taxes (5% of EC)	18,956
	Freight (8% of EC)	30,330
	Subtotal - Purchased Equipment Costs (PEC)	466,317
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC)	466,317
INDIRECT INSTALLATI	ON COSTS	
	Engineering Costs (5% of PEC)	23,316
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	46,632
	Start-up (1% of PEC)	4,663
	Performance Test (1% of PEC)	4,663
	Contingency (3% of PEC)	13,990
TOTAL INDIRECT COS	TS, IC	93,263
TOTAL CAPITAL	INVESTMENT (TCI)	559,581

## PES Refinery Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	15,388 15,388
Annualized Cost Factor Replacement Life Interest R Annualized Cost Factor	
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities None	
Subtotal - Utilities	0.0
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	15,388

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M	COSTS			15,388
Annualized Cost Factor				
	Eq	uipment Life (years) =	10	
		Interest Rate (%) =	21.83	
	Annualized Cost Factor			0.25
CAPITAL RECOVERY CO	OSTS			
	TOTAL CAPITAL REQUIREMENT			559,581
	TOTAL ANNUAL CAPITAL REQUIREM	MENT		141,848
TOTAL ANNUALIZED ( (Total annual O&M cost	COST and annualized capital cost)			157,237

Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Source Unit 865-11H2 Control LNB & SNCR

Rated Heat Input 64.2 MMBtu/hr
Number of Burners 8.0 Burners
Baseline Actual Emissions 31.78 tpy
Current Emission Rate 0.113
Control Efficiency 70%

Heater Capacity 67.7 GJ/hr Burner Heat Release Rate 10.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

(	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	189,917
	Instrumentation (10% of EC)	18,992
	Sales taxes (5% of EC)	9,496
	Freight (8% of EC)	15,193
	Subtotal - Purchased Equipment Costs (PEC)	233,598
1	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	tc.	0
9	Site Preparation / Buildings- Included above	= = =
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TDC	') - LNB	233,598
NDIRECT INSTALLATION C	OSTS - LNB	
	Engineering Costs (5% of PEC)	11,680
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	23,360
	Start-up (1% of PEC)	2,336
	-	
	Performance Test (1% of PEC)	2,336
(	Contingency (3% of PEC)	7,008
TOTAL INDIRECT COSTS, IC - LNB		46,720
DIRECT COSTS - SNCR		
I	Purchased Equipment Costs	
	Equipment Cost (EC)	560,355
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	560,355
1	Direct Installation Costs (Based on Vendor Discussion)	
I	Foundations & supports; handling & erection; electrical; piping;	
	tc.	0
	Site Preparation / Buildings- Included above Subtotal - Direct Installation Costs	0
OTAL DIRECT COSTS (TDC	C) - SNCR	560,355
NDIRECT INSTALLATION C	OSTS - SNCR	
	Engineering Costs (Included in above costs)	
(	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs) Contingency (3% of PEC)	16,811
OTAL INDIRECT COSTS, IC		16,811
TOTAL CAPITAL INV	ESTMENT (TCI) - LNB	280,318
	ESTMENT (TCI) - LNB ESTMENT (TCI) - SNCR	280,318 577,165

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	23,581 23,581
Annualized Cost Factor	
Replacement Life (years) = 10	D
Interest Rate (%) = 21.8:	3
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,735
Electricity Cost	0.3
Subtotal - Utilities	4,735
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	28,316

	COST COMPONENT:				
TOTAL ANNUAL O&M	COSTS			28,316	
Annualized Cost Factor					
	I	Equipment Life (years) =	10		
		Interest Rate (%) =	21.83		
	Annualized Cost Factor			0.25	
CAPITAL RECOVERY CO	OSTS				
	TOTAL CAPITAL REQUIREMENT			857,483	
	TOTAL ANNUAL CAPITAL REQUIRE	EMENT		217,363	
TOTAL ANNUALIZED ( (Total annual O&M cost	245,679				

Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Source Unit 865-11H2 Control LNB & FGR

Rated Heat Input64.2MMBtu/hrNumber of Burners8.0BurnersBaseline Actual Emissions31.78tpyCurrent Emission Rate0.113Ib/MMBtuControl Efficiency55%

Heater Capacity 67.7 GJ/hr Burner Heat Release Rate 10.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	189,917
	Instrumentation (10% of EC)	18,992
	Sales taxes (5% of EC)	9,496
	Freight (8% of EC)	15,193
	Subtotal - Purchased Equipment Costs (PEC)	233,598
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TD	C) - LNB	233,598
INDIRECT INSTALLATION	COSTS - LNB	
	Engineering Costs (5% of PEC)	11,680
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	23,360
	Start-up (1% of PEC)	2,336
	Performance Test (1% of PEC)	2,336
	Contingency (3% of PEC)	7,008
TOTAL INDIRECT COSTS, I	C - LNB	46,720
DIRECT COSTS - FGR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	225,197
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	= = =
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	225,197
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TD	C) - FGR	225,197
INDIRECT INSTALLATION	COSTS - FGR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs) Contingency (3% of PEC)	6,756
TOTAL INDIRECT COSTS, I		6,756
TOTAL CAPITAL IN	VESTMENT (TCI) - LNB	280,318
TOTAL CAPITAL IN	VESTMENT (TCI) - FGR	231,953
TOTAL CAPITAL IN	VESTMENT (TCI)	512,272

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	14,087 14,087
Annualized Cost Factor	
Replacement Life (years) = Interest Rate (%) =	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Electricity Cost	8,163
Subtotal - Utilities	8,163
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	22,250

	COST COMPONENT:				
TOTAL ANNUAL O&M	COSTS			22,250	
Annualized Cost Factor					
	E	Equipment Life (years) =	10		
		Interest Rate (%) =	21.83		
	Annualized Cost Factor			0.25	
CAPITAL RECOVERY CO	OSTS				
	TOTAL CAPITAL REQUIREMENT			512,272	
	TOTAL ANNUAL CAPITAL REQUIRE	EMENT		129,856	
TOTAL ANNUALIZED ( (Total annual O&M cost	152,106				

### **Heater Firing Rate Increase Plan Approval**

#### **NOx RACT Control Cost Effectiveness**

Source	Unit 865-11H2	
Control	SNCR	
Rated Heat Input	64.2	MMBtu/hr
Number of Burners	8.0	Burners
<b>Baseline Actual Emissions</b>	31.78	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
<b>Control Efficiency</b>	40%	
Heater Capacity	67.7	GJ/hr
<b>Burner Heat Release Rate</b>	10.8	GJ/hr

## Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	560,355
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	560,355
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC)	560,355
INDIRECT INSTALLATI	ON COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	16,811
TOTAL INDIRECT COS	TS, IC	16,811
TOTAL CAPITAL	INVESTMENT (TCI)	577,165

## **Heater Firing Rate Increase Plan Approval**

COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (	(2.75% of TCI)		15,872 15,872
Annualized Cost Factor  Annualized Cost Factor	Replacement Life (years) = Interest Rate (%) =	10 21.83	0.25
Replacement cost  Subtotal - Operation and Maintenance Labor			
Utilities Ammonia Cost Electricity Cost			4,735 0.3
Subtotal - Utilities			4,735
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>			20,607

	COST COMPONENT:					
TOTAL ANNUAL O&M	COSTS			20,607		
Annualized Cost Factor	Eq. Annualized Cost Factor	quipment Life (years) = Interest Rate (%) =	10 21.83	0.25		
CAPITAL RECOVERY CO	CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT					
	TOTAL ANNUAL CAPITAL REQUIREM	MENT		146,306		
OTAL ANNUALIZED COST Total annual O&M cost and annualized capital cost)				166,913		

### PES Refinery Heater Firing Rate Increase Plan Approval Unit 210-H101 RACT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	Design Firing (MMBtu/hr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ Design Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	192	0.089	74.8	96%	3.0	71.9	7,613,995	283,106	2,213,176	30,796
SCR	192	0.089	74.8	85%	11.2	63.6	5,940,483	237,084	1,742,936	27,397
LNB & SNCR	192	0.089	74.8	70%	22.5	52.4	10,712,635	305,750	3,021,296	57,667
ULNB	192	0.089	74.8	66%	25.2	49.6	1,673,512	46,022	470,240	9,477
LNB & FGR	192	0.089	74.8	55%	33.7	41.2	NA	NA	NA	NA
SNCR	192	0.089	74.8	40%	44.9	29.9	1,113,678	41,779	324,085	10,825
	Calculation	•	= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Technical Infeasibilities:

FGR would not physically fit the plot space; therefore, it is infeasible.

Notes:

 $<sup>^1</sup>$  Current generation UNLB is considered to be 0.03 lb/MMBtu, which represents a 66% reduction from 0.089 lb/MMBtu.

<sup>&</sup>lt;sup>2</sup> See "RACT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

#### PES Refinery Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Source Unit 210-H101
Control ULNB & SCR

Rated Heat Input 192.0 MMBtu/hr Number of Burners Burners **Baseline Actual Emissions** 74.85 tpy **Current Emission Rate** 0.089 lb/MMBtu **Control Efficiency** 96% **Heater Capacity** 202.6 GJ/hr Burner Heat Release Rate 40.4 GJ/hr

### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS - ULI	VR	
	Purchased Equipment Costs	
	Equipment Cost (EC)	1,133,816
	Instrumentation (10% of EC)	113,382
	Sales taxes (5% of EC)	56,691
	Freight (8% of EC)	90,705
	Subtotal - Purchased Equipment Costs (PEC)	1,394,593
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	TS (TDC) - ULNB	1,394,593
INDIRECT INSTALLA	TION COSTS - ULNB	
	Engineering Costs (5% of PEC)	69,730
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	139,459
	Start-up (1% of PEC)	13,946
	Performance Test (1% of PEC)	13,946
	Contingency (3% of PEC)	41,838
TOTAL INDIRECT CO	OSTS, IC - ULNB	278,919
DIRECT COSTS - SCK	2	
DINEET COSTS SCI	Purchased Equipment Costs	
	Equipment Cost (EC)	5,767,459
	Instrumentation (Included in above costs)	5,767,437
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Teight (included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	5,767,459
	Direct Installation Costs	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	TS (TDC) - SCR	5,767,459
INDIRECT INSTALLA	TION COSTS - SCR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	173,024
TOTAL INDIRECT CO	OSTS, IC - SCR	173,024
TOTAL CAPITA	L INVESTMENT (TCI) - ULNB	1,673,512
	L INVESTMENT (TCI) - SCR	5,940,483
	L INVESTMENT (TCI)	7,613,995
TOTAL CALLIA	LINESIMENI (ICI)	/,013,333

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	209,385 2 <b>09,385</b>
Annualized Cost Factor	207,363
Replacement Life (years) = $10$ Interest Rate (%) = $21.83$ Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	11,152
Catalyst Replacement Cost Electricity Cost	62,568 0.8
Subtotal - Utilities	73,721
TOTAL ANNUAL DIRECT COSTS*	283,106

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M	COSTS			283,106
Annualized Cost Factor				
	Eq	uipment Life (years) =	10	
	Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
CAPITAL RECOVERY CO	OSTS			
	TOTAL CAPITAL REQUIREMENT			7,613,995
	TOTAL ANNUAL CAPITAL REQUIREM	ENT		1,930,071
TOTAL ANNUALIZED ( (Total annual O&M cost	OOST and annualized capital cost)			2,213,176

## **Heater Firing Rate Increase Plan Approval**

### **NOx RACT Control Cost Effectiveness**

Source	Unit 210-H101	
Control	SCR	
Rated Heat Input	192.0	MMBtu/hr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	74.85	tpy
<b>Current Emission Rate</b>	0.089	lb/MMBtu
<b>Control Efficiency</b>	85%	
<b>Heater Capacity</b>	202.6	GJ/hr
<b>Burner Heat Release Rate</b>	40.4	GJ/hr

### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	5,767,459
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	5,767,459
	Direct Installation Costs	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TD	C)	5,767,459
INDIRECT INSTALLATION (	COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	173,024
TOTAL INDIRECT COSTS, I	C	173,024
TOTAL CAPITAL IN	JECTMENT (TOI)	5,940,483

## **Heater Firing Rate Increase Plan Approval**

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	163,363 163,363
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	11,152
Catalyst Replacement Cost	62,568
Electricity Cost	0.8
Subtotal - Utilities	73,721
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	237,084

COST COMPONENT:		COST (\$)
TOTAL ANNUAL O&M COSTS		237,084
Annualized Cost Factor  Equipment Life (years) =  Interest Rate (%) =  Annualized Cost Factor	10 21.83	
CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIREMENT		5,940,483 <b>1,505,852</b>
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)		1,742,936

#### PES Refinery Heater Firing Rate Increase Plan Approval

NOx RACT Control Cost Effectiveness

Source Unit 210-H101
Control LNB & SNCR

Rated Heat Input192.0MMBtu/hrNumber of Burners6.0BurnersBaseline Actual Emissions74.85tpyCurrent Emission Rate0.089lb/MBtuControl Efficiency70%

Heater Capacity 202.6 GJ/hr Burner Heat Release Rate 40.4 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	6,503,358
	Instrumentation (10% of EC)	650,336
	Sales taxes (5% of EC)	325,168
	Freight (8% of EC)	520,269
	Subtotal - Purchased Equipment Costs (PEC)	7,999,131
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping; etc.	0
		0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST.	S (TDC) - LNB	7,999,131
INDIRECT INSTALLAT	TION COSTS - LNB	
	Engineering Costs (5% of PEC)	399,957
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	799,913
	Start-up (1% of PEC)	79,991
	Performance Test (1% of PEC)	79,991
	· · · · · · · · · · · · · · · · · · ·	· ·
	Contingency (3% of PEC)	239,974
TOTAL INDIRECT CO	STS, IC - LNB	1,599,826
DIRECT COSTS - SNC	R	
	Purchased Equipment Costs	
	Equipment Cost (EC)	1,081,241
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	1,081,241
		, ,
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S (TDC) - SNCR	1,081,241
INDIRECT INSTALLAT	TON COSTS - SNCR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs) Contingency (3% of PEC)	32,437
TOTAL INDIRECT COS		32,437
TOTAL CAPITAL	L INVESTMENT (TCI) - LNB	9,598,957
	L INVESTMENT (TCI) - END	1,113,678
	\ /	, ,
TOTAL CAPITAL	L INVESTMENT (TCI)	10,712,635

COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material	(2.75% of TCI)		294,597 294,597
Annualized Cost Factor  Annualized Cost Factor	Replacement Life (years) = Interest Rate (%) =	10 21.83	0.25
Replacement cost  Subtotal - Operation and Maintenance Labor			
Utilities Ammonia Cost Electricity Cost  Subtotal - Utilities			11,152 0.8 11,153
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>			305,750

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M	COSTS			305,750
Annualized Cost Factor	Equ Annualized Cost Factor	ipment Life (years) = Interest Rate (%) =	10 21.83	0.25
CAPITAL RECOVERY CO	TOTAL CAPITAL REQUIREMENT	77. V		10,712,635
TOTAL ANNUALIZED C	TOTAL ANNUAL CAPITAL REQUIREM  OST  and annualized capital cost)	ENI		2,715,545 3,021,296

### Heater Firing Rate Increase Plan Approval

### **NOx RACT Control Cost Effectiveness**

Source Unit 210-H101 **ULNB** Control **Rated Heat Input** 192.0 MMBtu/hr **Number of Burners** 6.0 **Burners Baseline Actual Emissions** 74.85 tpy **Current Emission Rate** 0.089 lb/MMBtu **Control Efficiency** 66% GJ/hr **Heater Capacity** 202.6 Burner Heat Release Rate 40.4 GJ/hr

### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	1,133,816
	Instrumentation (10% of EC)	113,382
	Sales taxes (5% of EC)	56,691
	Freight (8% of EC)	90,705
	Subtotal - Purchased Equipment Costs (PEC)	1,394,593
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC)	1,394,593
INDIRECT INSTALLATION	ON COSTS	
	Engineering Costs (5% of PEC)	69,730
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	139,459
	Start-up (1% of PEC)	13,946
	Performance Test (1% of PEC)	13,946
	Contingency (3% of PEC)	41,838
TOTAL INDIRECT COST	TS, IC	278,919
TOTAL CAPITAL	INVESTMENT (TCI)	1,673,512

## **Heater Firing Rate Increase Plan Approval**

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	46,022 46,022
Annualized Cost Factor  Replacement Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities None	
Subtotal - Utilities	0.0
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	46,022

	COST COMPONENT:		COST (\$)
TOTAL ANNUAL O&M C	COSTS		46,022
Annualized Cost Factor	Equipment Life (years) = Interest Rate (%) = Annualized Cost Factor	10 21.83	0.25
CAPITAL RECOVERY CO.	STS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIREMENT		1,673,512 <b>424,218</b>
TOTAL ANNUALIZED C (Total annual O&M cost a			470,240

### **Heater Firing Rate Increase Plan Approval**

#### **NOx RACT Control Cost Effectiveness**

Source	Unit 210-H101	
Control	SNCR	
Rated Heat Input	192.0	MMBtu/hr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	74.85	tpy
<b>Current Emission Rate</b>	0.089	lb/MMBtu
Control Efficiency	40%	
<b>Heater Capacity</b>	202.6	GJ/hr
<b>Burner Heat Release Rate</b>	40.4	GJ/hr

## Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	1,081,241
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	1,081,241
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	TS (TDC)	1,081,241
INDIRECT INSTALLA	TION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	32,437
TOTAL INDIRECT CO	OSTS, IC	32,437
TOTAL CAPITA	L INVESTMENT (TCI)	1,113,678

## **Heater Firing Rate Increase Plan Approval**

COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (	(2.75% of TCI)		30,626 30,626
Annualized Cost Factor  Annualized Cost Factor	Replacement Life (years) = Interest Rate (%) =	10 21.83	0.25
Replacement cost			
Subtotal - Operation and Maintenance Labor			
Utilities Ammonia Cost Electricity Cost			11,152 0.8
Subtotal - Utilities			11,153
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>			41,779

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M	COSTS			41,779
Annualized Cost Factor	E	Equipment Life (years) =	10	
	Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
CAPITAL RECOVERY CO	STS			
	TOTAL CAPITAL REQUIREMENT			1,113,678
	TOTAL ANNUAL CAPITAL REQUIRE	EMENT		282,306
TOTAL ANNUALIZED C	OST nd annualized capital cost)			324,085

### PES Refinery Heater Firing Rate Increase Plan Approval Unit 210-H201 RACT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	Design Firing (MMBtu/hr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ Design Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	254	0.03	33.4	96%	1.3	32.0	NA	NA	NA	NA
SCR	254	0.03	33.4	85%	5.0	28.4	NA	NA	NA	NA
LNB & SNCR	254	0.03	33.4	70%	10.0	23.4	13,474,367	375,519	3,791,135	162,271
LNB & FGR	254	0.03	33.4	55%	15.0	18.4	NA	NA	NA	NA
SNCR	254	0.03	33.4	40%	20.0	13.4	1,317,284	41,199	375,117	28,098
ULNB	254	0.03	33.4	0%	33.4	0.0	NA	NA	NA	NA
	Calculation		= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Technical Infeasibilities:

SCR would not physically fit the plot space and there is not adequate pressure to overcome the SCR pressure drop; therefore, SCR is infeasible. FGR installation would require the installation of mechanical draft burners, which is a major re-design of the unit; therefore FGR is infeasible.

<sup>&</sup>lt;sup>1</sup> ULNB is already installed on the Unit 210-H201 heater.

<sup>&</sup>lt;sup>2</sup> See "RACT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

#### PES Refinery Heater Firing Rate Increase Plan Approval

NOx RACT Control Cost Effectiveness

Source Unit 210-H201 Control LNB & SNCR

 Rated Heat Input
 254.0
 MMBtu/hr

 Number of Burners
 8.0
 Burners

 Baseline Actual Emissions
 33.38
 tpy

 Current Emission Rate
 0.030
 lb/MBtu

 Control Efficiency
 70%

 Heater Capacity
 268.0
 GJ/hr

Heater Capacity 268.0 GJ/hr Burner Heat Release Rate 39.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	8,236,506
	Instrumentation (10% of EC)	823,651
	Sales taxes (5% of EC)	411,825
	Freight (8% of EC)	658,920
	Subtotal - Purchased Equipment Costs (PEC)	10,130,902
	1.7	.,, .
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
OTAL DIRECT COSTS	(TDC) - LNB	10,130,902
VIDIDEOT DIOTALLAN	ON COURS IND	
NDIRECT INSTALLATION		506.545
	Engineering Costs (5% of PEC)	506,545
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	1,013,090
	Start-up (1% of PEC)	101,309
	Performance Test (1% of PEC)	101,309
	Contingency (3% of PEC)	303,927
TOTAL INDIRECT COST	TS, IC - LNB	2,026,180
DIRECT COSTS - SNCR		
DIKECT COSTS - SIVCK	Durchased Equipment Costs	
	Purchased Equipment Costs	1 279 016
	Equipment Cost (EC)	1,278,916
	Instrumentation (Included in above costs)	= = =
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	= = =
	Subtotal - Purchased Equipment Costs (PEC)	1,278,916
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC) - SNCR	1,278,916
INDIRECT INSTALLATION	ON COSTS - SNCR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	= = =
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs) Contingency (3% of PEC)	38,367
TOTAL INDIRECT COST		38,367
	INVESTMENT (TCI) - LNB	12,157,083
	INVESTMENT (TCI) - SNCR	1,317,284
I OTAL CAPITAL	INVESTMENT (TCI)	13,474,367

COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (	2.75% of TCI)		370,545 370,545
Annualized Cost Factor  Annualized Cost Factor	Replacement Life (years) = Interest Rate (%) =	10 21.83	0.25
Replacement cost  Subtotal - Operation and Maintenance Labor			
Utilities Ammonia Cost Electricity Cost  Subtotal - Utilities			4,973 0.4 <b>4,973</b>
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>			375,519

COST COMPONENT:		COST (\$)
M COSTS		375,519
Equipment Life (years) =	10	
Interest Rate (%) =	21.83	
Annualized Cost Factor		0.25
COSTS		
TOTAL CAPITAL REQUIREMENT		13,474,367
TOTAL ANNUAL CAPITAL REQUIREMENT		3,415,616
D COST		3,791,135
	Interest Rate (%) = Annualized Cost Factor  COSTS TOTAL CAPITAL REQUIREMENT	Equipment Life (years) = 10 Interest Rate (%) = 21.83  Annualized Cost Factor  COSTS TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIREMENT

### **Heater Firing Rate Increase Plan Approval**

#### **NOx RACT Control Cost Effectiveness**

Source	Unit 210-H201	
Control	SNCR	
Rated Heat Input	254.0	MMBtu/hr
Number of Burners	8.0	Burners
<b>Baseline Actual Emissions</b>	33.38	tpy
<b>Current Emission Rate</b>	0.030	lb/MMBtu
Control Efficiency	40%	
Heater Capacity	268.0	GJ/hr
<b>Burner Heat Release Rate</b>	39.8	GJ/hr

## Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	1,278,916
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	1,278,916
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	TS (TDC)	1,278,916
INDIRECT INSTALLA	TION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	38,367
TOTAL INDIRECT CO	STS, IC	38,367
TOTAL CAPITA	L INVESTMENT (TCI)	1,317,284

## **Heater Firing Rate Increase Plan Approval**

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	36,225 36,225
Annualized Cost Factor  Replacement I  Interes  Annualized Cost Factor	Life (years) = 10 at Rate (%) = 21.83 0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities Ammonia Cost Electricity Cost	4,973 0.4
Subtotal - Utilities	4,973
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	41,199

	COST (\$)		
TOTAL ANNUAL O&M C	OSTS		41,199
Annualized Cost Factor			
	Equipment Life (y	years) = 10	
	Interest Rate Annualized Cost Factor	21.83	0.25
CAPITAL RECOVERY COS	TS		
	TOTAL CAPITAL REQUIREMENT		1,317,284
	TOTAL ANNUAL CAPITAL REQUIREMENT		333,918
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)			375,117

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 866-12H1 RACT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	Design Firing (MMBtu/hr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ Design Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	61.2	0.113	30.3	96%	1.2	29.1	3,518,199	121,208	1,013,036	34,831
SCR	61.2	0.113	30.3	85%	4.5	25.7	2,984,767	106,538	863,147	33,524
ULNB	61.2	0.113	30.3	73%	8.0	22.2	533,432	14,669	149,889	6,737
LNB & SNCR	61.2	0.113	30.3	70%	9.1	21.2	838,966	27,585	240,255	11,331
LNB & FGR	61.2	0.113	30.3	55%	13.6	16.7	503,525	21,628	149,267	8,960
SNCR	61.2	0.113	30.3	40%	18.2	12.1	560,828	19,936	162,101	13,379
	Calculation	•	= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Notes:

 $<sup>^1</sup>$  Unit 866-12H1 is projected to be above PADEP presumptive RACT firing limits and assumed NO  $_{\rm x}$  emission rate limit of 0.113 lb/MMBtu is used.

 $<sup>^2\,\</sup>mbox{See}$  "RACT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

#### PES Refinery Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Source Unit 866-12H1
Control ULNB & SCR

Rated Heat Input 61.2 MMBtu/hr Number of Burners 6.0 Burners Baseline Actual Emissions 30.29 tpy **Current Emission Rate** lb/MMBtu 0.113 **Control Efficiency** 96% **Heater Capacity** 64.6 GJ/hr Burner Heat Release Rate 13.8 GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS - UL	NB	
	Purchased Equipment Costs	
	Equipment Cost (EC)	361,404
	Instrumentation (10% of EC)	36,140
	Sales taxes (5% of EC)	18,070
	Freight (8% of EC)	28,912
	Subtotal - Purchased Equipment Costs (PEC)	444,527
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COS	TS (TDC) - ULNB	444,527
NDIRECT INSTALL	ATION COSTS - ULNB	
	Engineering Costs (5% of PEC)	22,226
	Construct. & Field Expenses (Included in above costs)	22,220
	Contractor Fees (10% of PEC)	44,453
	Start-up (1% of PEC)	4,445
	Performance Test (1% of PEC)	4,445
	Contingency (3% of PEC)	13,336
TOTAL INDIRECT C	OSTS, IC - ULNB	88,905
DIRECT COSTS - SC	R	
DIKECI COSIS-SC	Purchased Equipment Costs	
	Equipment Cost (EC)	2,897,832
	Instrumentation (Included in above costs)	2,097,032
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	2,897,832
	Direct Installation Costs	
	Direct Installation Costs  Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COS	TS (TDC) - SCR	2,897,832
INDIRECT INSTALL	ATION COSTS - SCR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	86,935
TOTAL INDIRECT C	OSTS, IC - SCR	86,935
TOTAL CAPITA	AL INVESTMENT (TCI) - ULNB	533,432
	AL INVESTMENT (TCI) - SCR	2,984,767
	AL INVESTMENT (TCI)	3,518,199
I O I AL CAFIL	TE HAVE STRICKE (ICI)	3,518,199

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	96,750
	96,750
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = $21.83$	1
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,513
Catalyst Replacement Cost	19,943
Electricity Cost	0.3
Subtotal - Utilities	24,457
TOTAL ANNUAL DIRECT COSTS*	121,208

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M	COSTS			121,208
Annualized Cost Factor				
	Ec	quipment Life (years) =	10	
	Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
CAPITAL RECOVERY CO	STS			
	TOTAL CAPITAL REQUIREMENT			3,518,199
	TOTAL ANNUAL CAPITAL REQUIREM	ENT		891,828
TOTAL ANNUALIZED C (Total annual O&M cost o	OST nd annualized capital cost)			1,013,036

# **Heater Firing Rate Increase Plan Approval**

## **NOx RACT Control Cost Effectiveness**

Source	Unit 866-12H1	
Control	SCR	
Rated Heat Input	61.2	MMBtu/hr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	30.29	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	85%	
<b>Heater Capacity</b>	64.6	GJ/hr
<b>Burner Heat Release Rate</b>	13.8	GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,897,832
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	2,897,832
	Direct Installation Costs	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S (TDC)	2,897,832
INDIRECT INSTALLAT	TION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	86,935
TOTAL INDIRECT CO	STS, IC	86,935
TOTAL CAPITAI	L INVESTMENT (TCI)	2,984,767

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	82,081 82,081
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,513
Catalyst Replacement Cost	19,943
Electricity Cost	0.3
Subtotal - Utilities	24,457
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	106,538

	COST COMPONENT:		COST (\$)
TOTAL ANNUAL O&M C	OSTS		106,538
Annualized Cost Factor			
	Equipment Life (	years) = 10	)
	Interest Rat		
	Annualized Cost Factor		0.25
CAPITAL RECOVERY COS	TS		
	TOTAL CAPITAL REQUIREMENT		2,984,767
	TOTAL ANNUAL CAPITAL REQUIREMENT		756,608
TOTAL ANNUALIZED CO			863,147

## **Heater Firing Rate Increase Plan Approval**

#### **NOx RACT Control Cost Effectiveness**

Source	Unit 866-12H1	
Control	ULNB	
Rated Heat Input	61.2	MMBtu/hr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	30.29	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	73%	
Heater Capacity	64.6	GJ/hr
<b>Burner Heat Release Rate</b>	13.8	GJ/hr

## **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	361,404
	Instrumentation (10% of EC)	36,140
	Sales taxes (5% of EC)	18,070
	Freight (8% of EC)	28,912
	Subtotal - Purchased Equipment Costs (PEC)	444,527
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC)	444,527
INDIRECT INSTALLATIO	ON COSTS	
	Engineering Costs (5% of PEC)	22,226
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	44,453
	Start-up (1% of PEC)	4,445
	Performance Test (1% of PEC)	4,445
	Contingency (3% of PEC)	13,336
TOTAL INDIRECT COST	TS, IC	88,905
TOTAL CAPITAL	INVESTMENT (TCI)	533,432

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	14,669 14,669
Annualized Cost Factor  Replacement Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities None	
Subtotal - Utilities	0.0
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	14,669

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M CO	OSTS			14,669
Annualized Cost Factor				
	Equipn	nent Life (years) =	10	
	II	nterest Rate (%) =	21.83	
	Annualized Cost Factor			0.25
CAPITAL RECOVERY COS	TS			
	TOTAL CAPITAL REQUIREMENT			533,432
	TOTAL ANNUAL CAPITAL REQUIREMENT	r		135,220
TOTAL ANNUALIZED CO (Total annual O&M cost an				149,889

#### PES Refinery Heater Firing Rate l

Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Source Unit 866-12H1
Control LNB & SNCR

Rated Heat Input 61.2 MMBtu/hr
Number of Burners 6.0 Burners
Baseline Actual Emissions 30.29 tpy
Current Emission Rate 0.113
Control Efficiency 70%

Heater Capacity 64.6 GJ/hr Burner Heat Release Rate 13.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	188,440
	Instrumentation (10% of EC)	18,844
	Sales taxes (5% of EC)	9,422
	Freight (8% of EC)	15,075
	Subtotal - Purchased Equipment Costs (PEC)	231,781
	Direct Installation Costs (Based on Vendor Discussion)	
I	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
:	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TDC	C) - LNB	231,781
INDIRECT INSTALLATION C	COSTS - LNB	
1	Engineering Costs (5% of PEC)	11,589
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	23,178
	Start-up (1% of PEC)	2,318
	Performance Test (1% of PEC)	2,318
	Contingency (3% of PEC)	6,953
TOTAL INDIRECT COSTS, IC	C - LNB	46,356
DIRECT COSTS - SNCR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	544,494
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	544,494
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TDO	C) - SNCR	544,494
INDIRECT INSTALLATION C		
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs) Performance Test (Included in above costs)	
	Contingency (3% of PEC)	16,335
TOTAL INDIRECT COSTS, IC	C - SNCR	16,335
TOTAL CAPITAL INV	VESTMENT (TCI) - LNB	278,137
TOTAL CAPITAL INV	/ESTMENT (TCI) - SNCR	560,828
TOTAL CAPITAL INV	/FSTMENT (TCI)	838,966

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	<u>23,072</u> 23,072
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,513
Electricity Cost	0.3
Subtotal - Utilities	4,514
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	27,585

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M	COSTS			27,585
Annualized Cost Factor				
	E	Equipment Life (years) =	10	
		Interest Rate (%) =	21.83	
	Annualized Cost Factor			0.25
CAPITAL RECOVERY CO	OSTS			
	TOTAL CAPITAL REQUIREMENT			838,966
	TOTAL ANNUAL CAPITAL REQUIRE	EMENT		212,669
TOTAL ANNUALIZED ( (Total annual O&M cost	COST and annualized capital cost)			240,255

Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

Source Unit 866-12H1 Control LNB & FGR

 Rated Heat Input
 61.2
 MMBtu/hr

 Number of Burners
 6.0
 Burners

 Baseline Actual Emissions
 30.29
 tpy

 Current Emission Rate
 0.113
 lb/MBtu

Control Efficiency 55%

Heater Capacity 64.6 GJ/hr Burner Heat Release Rate 13.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LN	В	
	Purchased Equipment Costs	
	Equipment Cost (EC)	188,440
	Instrumentation (10% of EC)	18,844
	Sales taxes (5% of EC)	9,422
	Freight (8% of EC)	15,075
	Subtotal - Purchased Equipment Costs (PEC)	231,781
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COS	TS (TDC) - LNB	231,781
NDIRECT INSTALLA	ATION COSTS - LNB	
	Engineering Costs (5% of PEC)	11,589
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	23,178
	Start-up (1% of PEC)	2,318
	Performance Test (1% of PEC)	2,318
	Contingency (3% of PEC)	6,953
TOTAL INDIRECT C	OSTS, IC - LNB	46,356
DIRECT COSTS - FG	R	
	Purchased Equipment Costs	
	Equipment Cost (EC)	218,823
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	218,823
	Direct Installation Costs (Based on Vendor Discussion)	210,020
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COS	TS(TDC) - $FGR$	218,823
NDIRECT INSTALLA	ATION COSTS - FGR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs) Contingency (3% of PEC)	6,565
TOTAL INDIRECT C		6,565
TOTAL CAPITA	AL INVESTMENT (TCI) - LNB	278,137
	AL INVESTMENT (TCI) - FGR	225,388
	` '	
IOTAL CAPITA	AL INVESTMENT (TCI)	503,525

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	13,847 13,847
Annualized Cost Factor  Replacement Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities Electricity Cost	7,781
Subtotal - Utilities	7,781
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	21,628

COST COMPONENT:	COST (\$)
TOTAL ANNUAL O&M COSTS	21,628
Annualized Cost Factor	
Equipment Life (years) = 10	
Interest Rate (%) = $21.83$	
Annualized Cost Factor	0.25
CAPITAL RECOVERY COSTS	
TOTAL CAPITAL REQUIREMENT	503,525
TOTAL ANNUAL CAPITAL REQUIREMENT	127,639
TOTAL ANNUALIZED COST	149,267
Total annual O&M cost and annualized capital cost)	

## **Heater Firing Rate Increase Plan Approval**

#### **NOx RACT Control Cost Effectiveness**

Source	Unit 866-12H1	
Control	SNCR	
Rated Heat Input	61.2	MMBtu/hr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	30.29	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	40%	
Heater Capacity	64.6	GJ/hr
<b>Burner Heat Release Rate</b>	13.8	GJ/hr

# **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	544,494
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	544,494
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S(TDC)	544,494
INDIRECT INSTALLAT	ION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	16,335
TOTAL INDIRECT COS	STS, IC	16,335
TOTAL CAPITAI	INVESTMENT (TCI)	560,828

# PES Refinery Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	15,423
	15,423
Annualized Cost Factor  Replacement Life (years) = 10 Interest Rate (%) = 21.83 Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost Electricity Cost	4,513 0.3
Subtotal - Utilities	4,514
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	19,936

COST COMPONENT	Γ:		COST (\$)
TOTAL ANNUAL O&M COSTS			19,936
Annualized Cost Factor	Equipment Life (years) =	10	
Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
CAPITAL RECOVERY COSTS			
TOTAL CAPITAL REQ	QUIREMENT		560,828
TOTAL ANNUAL CA	PITAL REQUIREMENT		142,164
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost	t)		162,101

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 868-8H101 RACT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	Design Firing (MMBtu/hr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ Design Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	60	0.113	29.7	96%	1.2	28.5	3,472,395	119,468	999,686	35,060
SCR	60	0.113	29.7	85%	4.5	25.2	2,949,422	105,087	852,736	33,782
ULNB	60	0.113	29.7	73%	7.9	21.8	522,973	14,382	146,950	6,737
LNB & SNCR	60	0.113	29.7	70%	8.9	20.8	1,057,946	33,519	301,697	14,513
LNB & FGR	60	0.113	29.7	55%	13.4	16.3	726,468	27,607	211,759	12,965
SNCR	60	0.113	29.7	40%	17.8	11.9	554,204	19,666	160,151	13,482
	Calculation		= A * B * 8760 / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Notes:

 $<sup>^1</sup>$  Unit 868-8H101 is projected to be above PADEP presumptive RACT firing limits and assumed NO  $_{\rm x}$  emission rate limit of 0.113 lb/MMBtu is used.

<sup>&</sup>lt;sup>2</sup> See "RACT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

#### PES Refinery Heater Firing Rate Increase Plan Approval

#### NOx RACT Control Cost Effectiveness

Source Unit 868-8H101 Control ULNB & SCR

Rated Heat Input 60.0 MMBtu/hr Number of Burners 4.0 Burners Baseline Actual Emissions 29.70 tpy **Current Emission Rate** lb/MMBtu 0.113 Control Efficiency 96% **Heater Capacity** 63.3 GJ/hr Burner Heat Release Rate 20.3 GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS - UL	NB	
	Purchased Equipment Costs	
	Equipment Cost (EC)	354,317
	Instrumentation (10% of EC)	35,432
	Sales taxes (5% of EC)	17,716
	Freight (8% of EC)	28,345
	Subtotal - Purchased Equipment Costs (PEC)	435,810
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COS	TS (TDC) - ULNB	435,810
INDIRECT INSTALLA	ATION COSTS - ULNB	
	Engineering Costs (5% of PEC)	21,791
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	43,581
	Start-up (1% of PEC)	4,358
	Performance Test (1% of PEC)	4,358
	Contingency (3% of PEC)	13,074
TOTAL INDIRECT CO	OSTS, IC - ULNB	87,162
DIRECT COSTS - SC	R	
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,863,517
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	2,863,517
	Direct Installation Costs	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above  Subtotal - Direct Installation Costs	0
TOTAL DIRECT COS	TS (TDC) - SCR	2,863,517
INDIRECT INSTALLA	TION COSTS - SCR	
INSTALL	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	85,906
TOTAL INDIRECT C	OSTS, IC - SCR	85,906
TOTAL CAPITA	AL INVESTMENT (TCI) - ULNB	522,973
	AL INVESTMENT (TCI) - SCR	2,949,422
	AL INVESTMENT (TCI)	3,472,395
- CHILL		3,712,373

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	95,491
	95,491
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = $21.83$	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,425
Catalyst Replacement Cost	19,552
Electricity Cost	0.3
Subtotal - Utilities	23,978
TOTAL ANNUAL DIRECT COSTS"	119,468

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&	M COSTS			119,468
Annualized Cost Facto	or.			
	Equ	nipment Life (years) =	10	
	Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
CAPITAL RECOVERY	COSTS			
	TOTAL CAPITAL REQUIREMENT			3,472,395
	TOTAL ANNUAL CAPITAL REQUIREME	ENT		880,217
TOTAL ANNUALIZE	D COST			999,686

## **Heater Firing Rate Increase Plan Approval**

## **NOx RACT Control Cost Effectiveness**

Source	Unit 868-8H101	
Control	SCR	
Rated Heat Input	60.0	MMBtu/hr
Number of Burners	4.0	Burners
<b>Baseline Actual Emissions</b>	29.70	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	85%	
<b>Heater Capacity</b>	63.3	GJ/hr
<b>Burner Heat Release Rate</b>	20.3	GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,863,517
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	2,863,517
	Direct Installation Costs	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S(TDC)	2,863,517
INDIRECT INSTALLAT	TION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	85,906
TOTAL INDIRECT CO	STS, IC	85,906
ΓΟΤΑL CAPITAI	L INVESTMENT (TCI)	2,949,422

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	81,109 81,109
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,425
Catalyst Replacement Cost	19,552
Electricity Cost	0.3
Subtotal - Utilities	23,978
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	105,087

	COST COMPONENT:	COST (\$)
TOTAL ANNUAL O&M COS	STS	105,087
Annualized Cost Factor	Equipment Life (years) = 10 Interest Rate (%) = 21.83 Annualized Cost Factor	
	TOTAL CAPITAL REQUIREMENT	2,949,422
TOTAL ANNUALIZED COS (Total annual O&M cost and		747,649 852,736

## **Heater Firing Rate Increase Plan Approval**

## **NOx RACT Control Cost Effectiveness**

Source	Unit 868-8H101	
Control	ULNB	
Rated Heat Input	60.0	MMBtu/hr
Number of Burners	4.0	Burners
<b>Baseline Actual Emissions</b>	29.70	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	73%	
Heater Capacity	63.3	GJ/hr
<b>Burner Heat Release Rate</b>	20.3	GJ/hr

## **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	354,317
	Instrumentation (10% of EC)	35,432
	Sales taxes (5% of EC)	17,716
	Freight (8% of EC)	28,345
	Subtotal - Purchased Equipment Costs (PEC)	435,810
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC)	435,810
INDIRECT INSTALLATIO	ON COSTS	
	Engineering Costs (5% of PEC)	21,791
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	43,581
	Start-up (1% of PEC)	4,358
	Performance Test (1% of PEC)	4,358
	Contingency (3% of PEC)	13,074
TOTAL INDIRECT COST	S, IC	87,162
TOTAL CAPITAL I	NVESTMENT (TCI)	522,973

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	14,382 14,382
Annualized Cost Factor $ \begin{array}{ccc} & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & \\ & & & \\ & \\ & & \\ &$	0.25
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities  None  Subtotal - Utilities	0.0
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	14,382

CO	OST COMPONENT:	COST (\$)
TOTAL ANNUAL O&M COSTS	S	14,382
Annualized Cost Factor		
	Equipment Life (years) = 10	
	Interest Rate (%) = $21.83$	3
Ar	nnualized Cost Factor	0.25
CAPITAL RECOVERY COSTS		
TO	OTAL CAPITAL REQUIREMENT	522,973
TO	OTAL ANNUAL CAPITAL REQUIREMENT	132,568
TOTAL ANNUALIZED COST (Total annual O&M cost and an	nualized capital cost)	146,950

# PES Refinery Heater Firing Rate

Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

TOTAL TO TOUR OF COST EMOCUTORIES

Source Unit 868-8H101 Control LNB & SNCR

 Rated Heat Input
 60.0
 MMBtu/hr

 Number of Burners
 4.0
 Burners

 Baseline Actual Emissions
 29.70
 tpy

 Current Emission Rate
 0.113
 lb/MBtu

Control Efficiency 70%

Heater Capacity 63.3 GJ/hr Burner Heat Release Rate 20.3 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

C	OST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	ırchased Equipment Costs	
	Equipment Cost (EC)	341,289
	Instrumentation (10% of EC)	34,129
	Sales taxes (5% of EC)	17,064
	Freight (8% of EC)	27,303
Su	ubtotal - Purchased Equipment Costs (PEC)	419,785
Di	irect Installation Costs (Based on Vendor Discussion)	
	oundations & supports; handling & erection; electrical; piping;	
ete	c.	0
Si	te Preparation / Buildings- Included above	
Su	ubtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TDC)	- LNB	419,785
INDIRECT INSTALLATION CO	OSTS - LNB	
	ngineering Costs (5% of PEC)	20,989
	onstruct. & Field Expenses (Included in above costs)	
	ontractor Fees (10% of PEC)	41,979
	art-up (1% of PEC)	4,198
	erformance Test (1% of PEC)	4,198
	ontingency (3% of PEC)	12,594
TOTAL INDIRECT COSTS, IC -	- LNB	83,957
DIRECT COSTS - SNCR		
	and and Francisco and Control	
	urchased Equipment Costs	529.062
	Equipment Cost (EC)	538,062
	Instrumentation (Included in above costs) Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
		538,062
	ubtotal - Purchased Equipment Costs (PEC)	538,062
	irect Installation Costs (Based on Vendor Discussion)	
	oundations & supports; handling & erection; electrical; piping;	0
etc c:	te Preparation / Buildings- Included above	Ü
	abtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TDC)	- SNCR	538,062
NDIRECT INSTALLATION CO	OSTS - SNCR	
	ngineering Costs (Included in above costs)	
	onstruct. & Field Expenses (Included in above costs)	
	ontractor Fees (Included in above costs)	
	art-up (Included in above costs) erformance Test (Included in above costs)	
	entermance 1est (included in above costs) ontingency (3% of PEC)	16,142
TOTAL INDIRECT COSTS, IC	SNCR	16,142
TOTAL CAPITAL INVI	ESTMENT (TCI) - LNB	503,742
	ESTMENT (TCI) - SNCR	554,204
	ESTMENT (TCI)	1,057,946

COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75	5% of TCI)		29,094 29,094
Annualized Cost Factor I Annualized Cost Factor	Replacement Life (years) = Interest Rate (%) =	10 21.83	0.25
Replacement cost  Subtotal - Operation and Maintenance Labor			
Utilities Ammonia Cost Electricity Cost			4,425 0.3
Subtotal - Utilities  TOTAL ANNUAL DIRECT COSTS <sup>a</sup>			4,425 33,519

	COST COMPONENT:					
TOTAL ANNUAL O&M C	OTAL ANNUAL O&M COSTS					
Annualized Cost Factor						
	Eq	uipment Life (years) =	10			
		Interest Rate (%) =	21.83			
	Annualized Cost Factor			0.25		
CAPITAL RECOVERY CO.	CAPITAL RECOVERY COSTS					
	TOTAL CAPITAL REQUIREMENT			1,057,946		
	TOTAL ANNUAL CAPITAL REQUIREM	MENT		268,179		
TOTAL ANNUALIZED C (Total annual O&M cost a	OST nd annualized capital cost)			301,697		

Heater Firing Rate Increase Plan Approval

NOx RACT Control Cost Effectiveness

Source Unit 868-8H101 Control LNB & FGR

 Rated Heat Input
 60.0
 MMBtu/hr

 Number of Burners
 4.0
 Burners

 Baseline Actual Emissions
 29.70
 tpy

 Current Emission Rate
 0.113
 lb/MBtu

Control Efficiency 55%

Heater Capacity 63.3 GJ/hr Burner Heat Release Rate 20.3 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	341,289
	Instrumentation (10% of EC)	34,129
	Sales taxes (5% of EC)	17,064
	Freight (8% of EC)	27,303
	Subtotal - Purchased Equipment Costs (PEC)	419,785
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping; etc.	0
		Ü
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC) - LNB	419,785
NDIRECT INSTALLATION	ON COSTS - LNB	
	Engineering Costs (5% of PEC)	20,989
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	41,979
	Start-up (1% of PEC)	4,198
	-	
	Performance Test (1% of PEC)	4,198
	Contingency (3% of PEC)	12,594
TOTAL INDIRECT COST	TS, IC - LNB	83,957
DIRECT COSTS - FGR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	216,239
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtatal Purchased Equipment Costs (PEC)	216,239
	Subtotal - Purchased Equipment Costs (PEC)	210,239
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	_
	etc.	0
	Site Preparation / Buildings- Included above  Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC) - FGR	216,239
NDIRECT INSTALLATION	ON COSTS - FGR	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs) Contingency (3% of PEC)	6,487
TOTAL INDIRECT COST		6,487
	INVESTMENT (TCI) - LNB	503,742
	INVESTMENT (TCI) - FGR	222,726
POTAL CADITAL	INVESTMENT (TCI)	726,468

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	19,978 19,978
Annualized Cost Factor  Replacement Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities Electricity Cost	7,629
Subtotal - Utilities	7,629
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	27,607

Equipment Life (years) =  Interest Rate (%) =  zed Cost Factor	10 21.83	7,607
Interest Rate (%) =	21.83	
Interest Rate (%) =	21.83	
zed Cost Factor		
		0.25
CAPITAL REQUIREMENT	72	26,468
ANNUAL CAPITAL REQUIREMENT	18	84,152
	21	11,759
	CAPITAL REQUIREMENT  ANNUAL CAPITAL REQUIREMENT  lized capital cost)	ANNUAL CAPITAL REQUIREMENT 18

# **Heater Firing Rate Increase Plan Approval**

#### **NOx RACT Control Cost Effectiveness**

Source	Unit 868-8H101	
Control	SNCR	
Rated Heat Input	60.0	MMBtu/hr
Number of Burners	4.0	Burners
<b>Baseline Actual Emissions</b>	29.70	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	40%	
<b>Heater Capacity</b>	63.3	GJ/hr
<b>Burner Heat Release Rate</b>	20.3	GJ/hr

# **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	538,062
	Instrumentation (Included in above costs)	
	Sales taxes (Included in above costs)	
	Freight (Included in above costs)	
	Subtotal - Purchased Equipment Costs (PEC)	538,062
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S(TDC)	538,062
INDIRECT INSTALLAT	TION COSTS	
	Engineering Costs (Included in above costs)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (Included in above costs)	
	Start-up (Included in above costs)	
	Performance Test (Included in above costs)	
	Contingency (3% of PEC)	16,142
TOTAL INDIRECT CO	STS, IC	16,142
TOTAL CAPITAI	L INVESTMENT (TCI)	554,204

# PES Refinery Heater Firing Rate Increase Plan Approval NOx RACT Control Cost Effectiveness

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	15,241 15,241
Annualized Cost Factor  Replacement Li  Interest I  Annualized Cost Factor	
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities  Ammonia Cost Electricity Cost	4,425 0.3
Subtotal - Utilities	4,425
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	19,666

COST COMPONENT:	COST (\$)	
TOTAL ANNUAL O&M COSTS	19,666	
Annualized Cost Factor  Equipment Life (years) =  Interest Rate (%) =  Annualized Cost Factor	10 21.83	
CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIREMENT		554,204 <b>140,485</b>
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)	160,151	

Attachment B AMS Plan Approval Application Forms



# CITY OF PHILADELPHIA

DEPARTMENT OF PUBLIC HEALTH PUBLIC HEALTH SERVICES AIR MANAGEMENT SERVICES Air Management Services 321 University Avenue Philadelphia PA 19104-4543 Phone: (215) 685-7572 FAX: (215) 685-7593

# APPLICATION FOR PLAN APPROVAL TO CONSTRUCT, MODIFY OR REACTIVATE AN AIR CONTAMINATION SOURCE AND/OR AIR CLEANING DEVICE

(Prepare all information completely in print or type in triplicate)

		эт от турс ил тор.						
SECTION A - APPLICATIO	N INFC	DRMATION						
Location of source ( Street Address) Facility Name								
3144 Passyunk Avenue		PES Philadelphia Refinery						
Owner				Tax ID N	0.			
Philadelphia Energy Solutions Refining & Marketing, LLC				61-16895	74			
Mailing Address		Telephone No.		Fax No.	/4			
3144 Passyunk Avenue, Philadelphia, PA 19145 (215) 339-2657								
Contact Person Title								
Charles D. Barksdale		Manager, Environmen	atal Dep	artment				
Mailing Address		Telephone No.		Fax No				
3144 Passyunk Avenue, Philadelphia, PA 19145  SECTION B - DESCRIPTIO	ON OF AC	(215) 339-2074		(215) 339	-2657			
Application type	JN OF AC	TIAILE	SIC Co	de	Completion I	2040		
Application type			SIC CO	XIE .	Completion 1	Aic		
□ New source □ Modification □ Replacement □ Reactivation □ Air cleaning device	e 🖾 Othe	r	2911		On Approva			
Does Fa	acility subn	nit Compliance Review F	orm bian	mually ?	X Yes	No		
□ NSPS □ NESHAP □ Case by Case MACT □ NSR □ PSD If No at	tach Air Po	ollution Control Act Com	pliance R	leview Fon	m with this app	lication.		
Source Description: The Sunoco Philadelphia Refinery proposes to marginally increase	e the firing	e limitations of seven pro	cos hea	tors and to	a relea refleam	t owndo		
feed and product rates by proportionate amounts. No physical modifications are requ	ired to eit	her process units or mor	ltoring:	systems. I	Emissions incr	enses		
will be netted to insignificant levels by the application of coincident ERC's from shutd	lown units	at the Sunoco Marcus H	iook, Pa	Refinery				
		8						
SECTION C - PERMIT COORDINATION (ONLY R	REQUIRE	D FOR LAND DEVELO	<u>OPMEN</u>	T)				
Question					YE	S NO X		
Will the project involve construction activity that disturbs five or more acres of land?     Will the project involve discharge of industrial wastewater or stormwater to a dry swale, surface water, ground water or an existing sanitary sewer								
2. Will the project involve discharge of industrial wastewater of stormwater to a dry sware, a system?	BUITACE WA	uer, grownu water or an ex	usting sai	mury sewe	ar	x		
3. Will the project involve the construction and operation of industrial waste treatment facili	ity?					X		
4. Is onsite sewage disposal proposed for your project?		<u> </u>				X		
5. Will the project involve construction of sewage treatment facilities, sanitary sewer, or sew	vage pump	ing station?				X		
6. Is a stormwater collection and discharge system proposed for this project?						X		
7. Will any work associated with this project take place in or near a stream, waterway, or we						Х		
8. Does the project involve dredging or construction of any dam, pier, bridge or outfall pipe	?					Х		
9. Will any solid waste or liquid wastes be generated as a result of the project?						Х		
10. Is a State Park located within two miles from your project?		<del></del>				Х		
SECTION D - CERTI								
I certify that I have the authority to submit this Permit Application on behalf of the application is true and correct to the best of my knowledge and information.	applicant	named herein and that	the infor	rmation pr	rovided in this			
Signature Date 1613	Addr	ess 3144 Passyun	k Avenu	e. Philade	lphia, PA 191	<u>45</u>		
Name & Title Nithia Thaver, General Manager Phone (215) 339	2.7414	Fax (215) 339-2657						
- THE STATE OF THE	7414	1 ux (313) 337-3331	······································					
SECTION E - OFFICIAL		VLY.	STATE OF	ME OF FR	的日本人門的	This work		
Application No. Plant ID Health District Census T	ract	Fee	Date	Received	TEACH IN			
			110					
Approved by Date Conformance by	Application of the		Date	THE CHILD	After a A street			
Continuate by			Date					
					F 158 S. S.			

				SECTI	ON F 1 - GENERA	L SOURCE INFORMA	ATION					.,			
1.	SOURCE							2. NORMA	L PROCE	SS OPERA	ATING SC	HEDUL	E		
	A. Type Source (Describe)	Manı	B. ufacturer Source	C. Model No.	D. Rated Capacity (Specify units)	E. Type of Materials Pro	ocessed	A. Amour Processed (Specify u	/yr.	B. Average hr/day	C. Total hr/yr	%		O. uput/Quar	ter
												18	2 <sup>nd</sup>	3 <sup>rd</sup>	4 <sup>th</sup>
1	Target heaters			1											
	See Attached Report for														
	Proposed Heater Firing											<del></del>			
	Changes														
3.	ESTIMATED FUEL USAGE	(Specify Unit	ts)	<u> </u>			4. AN	NUAL FUEL	USAGE						
A. Used in Unit	B. Type Fuel	C. Average Hourly Rate	D. Maximum Hourly Rate	E. Percent Sulfur	F. Percent Ash	G. Heating Value	Annı	A. ual Amounts	B. C. Average hr/day Total hr/yr			D. % Throughput/Quarter			
												l st	2 <sup>nd</sup>	3 <sup>rd</sup>	4 <sup>th</sup>
	See Attached Report for														
	Proposed Fired Htr. Duty														
	Changes														
			1									I	T		

5. IMPORTANT: Attach on a separate sheet a flow diagram of process giving all (gaseous, liquid, and solid) flow rates. Also list raw materials charged to process equipment and the amounts charged (tons/hour, etc.) at rated capacity (give maximum, minimum and average charges describing fully expected variations in production rates). Indicate (on diagram) all points where contaminants are controlled (location of water sprays, hoods or other pickup points, etc.).

Describe fully the methods used to monitor and record all operating conditions that may affect the emission of air contaminants. Provide detailed formation to show that these methods provided are adequate.  o New Monitoring Equipment is Proposed or Required	SECTION F 1 - GENERAL SOURCE INFORMATION, CONTINUED
Describe fully the methods used to monitor and record all operating conditions that may affect the emission of air contaminants. Provide detailed formation to show that these methods provided are adequate.  O New Monitoring Equipment is Proposed or Required  Describe modifications to process equipments in detail.	6. Describe process equipments in detail.
Describe fully the methods used to monitor and record all operating conditions that may affect the emission of air contaminants. Provide detailed formation to show that these methods provided are adequate.  o New Monitoring Equipment is Proposed or Required  Describe modifications to process equipments in detail.	
o New Monitoring Equipment is Proposed or Required  Describe modifications to process equipments in detail.	See Attached Report Sections
o New Monitoring Equipment is Proposed or Required  Describe modifications to process equipments in detail.	
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o New Monitoring Equipment is Proposed or Required  Describe modifications to process equipments in detail.	
o New Monitoring Equipment is Proposed or Required  Describe modifications to process equipments in detail.	7 Describe follows a substantial and a substanti
o New Monitoring Equipment is Proposed or Required  Describe modifications to process equipments in detail.	
Describe modifications to process equipments in detail.	information to show that these methods provided are adequate.
Describe modifications to process equipments in detail.	No New Monitoring Equipment is Proposed or Required
e Attached Report Sections	8. Describe modifications to process equipments in detail.
e Attached Report Sections	
e Attached Report Sections	
	See Attached Report Sections
Attack any and all additional information programs to adequately describe the amount of the day of the second of t	9. Attach any and all additional information necessary to adequately describe the process equipment and to perform a thorough evaluation of the extent and
	9. Attach any and all additional information necessary to adequately describe the process equipment and to perform a thorough evaluation of the extent and nature of its emissions.
ture of its chiassions.	nature of its chiastions.
e Attached Report that includes a BAT/RACT analysis	See Attached Report that includes a BAT/RACT analysis

	SECTION F	2 - COMBUSTION UNIT	'S INFORMATION		
1. COMBUSTION UNITS H101; H20	1; 11H1; 11H2; 12H1; 8	BH101; B101 - See Discussi	on Sections		
A. Manufacturer NA		B. Model No. NA		C. Unit No.	NA
D. Rated heat input (Btu/hr) NA	E. Peak heat input (Bt NA	tu/hr)	F. Use NA		
G. Method firing					
☐ Pulverized ☐ Spreader Stoker	Cyclone Tangen	tial Normal Fluidize	d bed Other		
2. FUEL REQUIREMENTS					
ТҮРЕ	QUANTITY HOURLY	QUANTITY ANNUALLY	SULFUR	ASH	BTU CONTENT
OIL NUMBER	NA	NA	NA	NA	NA
NA					
OTHER NA	NA	NA	NA	NA	NA
3. COMBUSTION AIDS, CONTROLS.	, AND MONITORS (I	No New Equipment)			
A. Overfire jets		Туре	Number	· · · · · · · · · · · · · · · · · · ·	Height above grate
B. Draft controls		Туре	Туре		
C. Oil preheat					
D. Soot cleaning	Temperature (° F)	Frequency	·		
☐ E. Stack sprays	Method				
F. Opacity monitoring device		Method		Cost	
G. Sulfur oxides monitoring device	Туре	Method		Cost	
H. Nitrogen oxides monitoring device	Туре	Method		Cost	
✓ I. Fuel metering and/or recording devi	Туре	Method		Cost	
☐ J. Atomization interlocking device		Туре	Method		Cost
☐ K. Collected flyash reentrainment pre	ventative device	Туре			
L. Modulating controls	Step Automatic				
4.  Flyash reinjection. (Describe opera	tion)				
Describe method of supplying make u	p air to the fumace room.				
N/A					
				······································	

	SECTION F	2 - COMBUSTI	ION UNITS INFORMA	ATION, CONTINUI	ED
6.	OPERATING SCHEDULE			<del></del>	
	NAhours/day	NA	days/week	NA	weeks/year
7.	SEASONAL PERIODS (MONTHS) N/A				
	Operating using primary fuel	·	Operat	ting using secondary ft	uel
	to				
			Non-operating		
	-		to	· · · · · · · · · · · · · · · · · · ·	
8.	If heat input is in excess of 250 x 10 <sup>6</sup> Btu/hr., describules; smoke, sulfur oxides and nitrogen oxides emisgeneration rate.	be fully the methorissions; and if ele	ods used to record the fo	ollowing: rate of fuel the average electrical o	oumed; heating value, sulfur and ash content of output and the minimum and maximum hourly
	will continue to monitor, record, and report with	applicable requi	irements found in the J	Philadelphia Refiner	y's existing Title V permit and the Consent
Decr	ee				
9.	Describe modifications to boiler in detail.			<u> </u>	
	Attached Report Sections				
500	Trucked Report Sections				
<del></del>	<del></del>				
10.	Type and method of disposal of all waste materials ge (Is a Solid Waste Disposal Permit needed?  Yes	enerated by this bo	oiler.		
		e attaine			
11.	Briefly describe the method of handling the waste war (Is a Water quality Management Permit needed?	ater from this boile Yes 🛛 No)		sollution control equip	ment.
12.	Attach any and all additional information necessary to	o perform a thorou	ugh evaluation of this bo	oiler.	
See A	Attached Report Sections				

- USE THIS PAGE FOR COMBUSTION SOURCE, OTHERWISE REMOVE THIS PAGE FROM THIS APPLICATION. IF THERE ARE MORE THAN ONE UNIT, COPY THIS PAGE AND FILL IN THE INFORMATION AS INDICATED

SECTION G - FLUE AND A	AIR CONTAMI	NANT EMISSION II	NFORMATION					
This project does not involve any changes to existing stacks or emis	sion points.							
A. Outlet volume of exhaust gases  B, Exhauster (attach fan curves)								
CFM @°F% Moist	ture	in w.g	НР	@RPM				
C . Stack height above grade (ft)	D Stack d	iameter (ft) or Outlet de	act area (sq. ft.)	E Weather Cap				
Grade elevation (ft)				☐ YES ☐ NO				
Distance from discharge to nearest property line(ft)								
F. Indicate on an attached sheet the location of sampling ports with respect to exhaust fan, breeching, etc. Give all necessary dimensions.								
2 POTENTIAL PROCESS EMISSIONS (OUTLET FROM PROCESS	S, BEFORE ANY	CONTROL EQUIPM	IENT)					
See Attached Report Sections			···· <del>·</del> ·······························	···				
A. Particulate loading (lbs/hr or gr/DSCF)  B. Specific gravi	ity of particulate (	(not bulk density)	C . Attached parti	icle size distribution information				
D. Specify gaseous contaminants and concentration								
Contaminant Concentration VOC Con	taminants C	oncentration						
(1) SO <sub>x</sub> ppm (Vol.) lbs/hr (4)		ppm (Vol.)	lbs/hr					
(2) NO <sub>x</sub> ppm (Vol.)lbs/hr (5)		ppm (Vol.)	lbs/hr					
(3) CO ppm (Vol.) lbs/hr (6)		ppm (Vol.)	lbs/hr					
E. Does process vent through the control device ? YES	NO		······································					
- If YES continue and fill out the appropriate SECTION H - CONTRO - If NO skip to SECTION I - MISCELLANEOUS INFORMATION	OL EQUIPMENT	Γ						
F. Can the control equipment be bypassed: (If Yes, explain)	YES NO							
ATMOSPHERIC EMISSIONS     A. Particulate matter emissions (tons per year)								
See Attached Report Sections								
B. Gaseous contaminant emissions								
Contaminants Concentration VOC C	ontaminants	Concentration						
(1)(tpy) (4)(tpy)								
(2)(tpy) (5)(tpy)								
(3)(tpy) (6)(tp	y)							
See Attached Report Sections								

SECTION H - CONTROL EQUIPMENT, CONTINUED					
12. COSTS - See Attached Report Sections					
A. List costs associated with control equipment. (List individual controls separately)					
Control Equipment Cost: Direct Cost:					
Indirect Cost:					
B. Estimated annual operating costs of control equipment only.					
13. Describe modifications to control equipment in detail.					
N/A					
14. Describe in detail the method of dust removal from the air cleaning and methods of controlling fugitive emissions from dust removal, handling and disposal.					
N/A					
15. Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If so, describe.					
N/A					
16. Attach manufacturer's performance guarantees and/or warranties for each of the major components of the control system (or complete system).					
17. Attach the maintenance schedule for the control equipment and any part of the process equipment that if in disrepair would increase the air contaminant emissions. Periodic maintenance reports are to be submitted to the Department.					
Maintenance will continue to be be provided as per the manufacturer's recommendations and the Title V Permit.					
18. Attach any and all additional information necessary to thoroughly evaluate the control equipment.					
See Attached Report Sections					
SECTION I - MISCELLANEOUS INFORMATION					
1. Specify monitoring and recording devices will be used for monitoring and recording of the emission of air contaminants. Provide detailed information to show that the facilities provided are adequate. Include cost and maintenance information.					
□ Opacity monitoring system       □ SOx monitoring system       □ NOx monitoring system         □ CO monitoring system       □ CO2 monitoring system       □ Oxygen monitoring system         □ HCL monitoring system       □ TRS monitoring system       □ H2S monitoring system         □ Temperature monitoring system       □ Stack flow monitoring system       □ Other					
If checked, provide manufacturer's name, model no. and pertinent technical specifications.					
NO CHANGES PROPOSED FROM EXISTING MONITORING, AS OUTLINED IN EXISTING TITLE V PERMIT.					

- PROVIDE CONTROL EQUIPMENT INFORMATION ON THIS PAGE IF IT PERTAINS TO THIS APPLICATION, OTHERWISE REMOVE THIS PAGE FROM THE APPLICATION.
  IF THERE ARE MORE OF THE SAME TYPE OF CONTROL EQUIPMENT, COPY THAT PAGE AND FILL IN THE INFORMATION AS INDICATED.
  CONTROL EQUIPMENT CAN BE FOUND FROM A MANUFACTURER CATALOGUE OR VENDORS.

NA .
3. If the source is subject to 25 Pa. Code Subchapter E, New Source Review requirements, a. Demonstrate the availability of emission offset (if applicable)
b. Provide an analysis of alternate sites, sizes, production processes and environmental control techniques demonstrating that the benefits of the proposed source outweigh the environmental and social costs.
CO Dispersion modeling is required for PSD purposes. NSR for nonattainment pollutants is not applicable. See the attached Report Sections.
4. Attach calculations and any additional information necessary to thoroughly evaluate compliance with all the applicable requirements of Article III of the rules and regulations of Philadelphia Air Management, Pennsylvania Department of Environmental Protection and those requirements promulgated by the Administrator of the United States Environmental Protection Agency pursuant to the provisions of the Clean Air Act.
See Attached Report Sections

2. Attach Air Pollution Episode Strategy (if applicable)

- PROVIDE CONTROL EQUIPMENT INFORMATION ON THIS PAGE IF IT PERTAINS TO THIS APPLICATION, OTHERWISE REMOVE THIS PAGE FROM THE APPLICATION.

  IF THERE ARE MORE OF THE SAME TYPE OF CONTROL EQUIPMENT, COPY THAT PAGE AND FILL IN THE INFORMATION AS INDICATED.

  CONTROL EQUIPMENT CAN BE FOUND FROM A MANUFACTURER CATALOGUE OR VENDORS.

# Attachment C Compliance Review History

## **Compliance History Review**

The Pa. Code 25 Section 127.12 requires either a completed compliance review form, or reference to the most recently submitted forms for facilities submitting a compliance review form on a periodic basis. PES files compliance review semi-annually per 127.12a(j). The latest form covering the Philadelphia Refinery was sent to the offices of Philadelphia Air Management Services in July of 2013.



Certified Mail: 7002 0460 0003 1936 6809

July 8, 2013

Department of Public Health Air Management Services 321 University Avenue Philadelphia, PA 19104

Philadelphia Energy Solutions Refining and Marketing LLC Re:

Title V Permit V95-038 (Philadelphia Refinery)

Title V Permit V95-039 (Schuylkill River Tank Farm)

Pennsylvania Air Pollution Control Act Compliance History Semi-Annual Submission

Philadelphia Refinery

215-339-2000

Philadelphia Energy Solutions Refining and Marketing LLC 3144 Passyunk Avenue Philadelphia, PA 19145-5299

## Dear Air Quality Program Manager:

Pursuant to 25 Pa. Code 127.412(j), Philadelphia Energy Solutions Refining and Marketing LLC (PES) hereby submits its semi-annual Pennsylvania Air Pollution Control Act Compliance History Form. As provided in 127.412(j), it is PES's ongoing intention to update this submission every six (6) months as opposed to submitting updates with each permit application that may be submitted throughout the year. The short term temporary diesel permits are not included in this submittal, if needed, they can be provided.

Should you have any questions or comments pertaining to this notification, contact me at (215) 339-2074.

Sincerely,

Charles D. Bark&dale Environmental Manager

CDB/pm

Philadelphia Energy Solutions Refining and Marketing LLC
Title V Permit V95-038 (Philadelphia Refinery)
Title V Permit V95-039 (Schuylkill River Tank Farm)
Pennsylvania Air Pollution Control Act Compliance History Semi-Annual Submission
July 8, 2013
Page 2

## Copies:

Certified Mail: 7002 0460 0003 1936 6731 Pennsylvania Department of Environmental Protection Attn: Air Quality Program Manager 2 East Main Street Norristown, PA 19401

Certified Mail: 7002 0460 0003 1936 6724 Pennsylvania Department of Environmental Protection Attn: Air Quality Program Manager 909 Elmerton Avenue Harrisburg, PA 17110-8200



# COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION BUREAU OF AIR QUALITY

## AIR POLLUTION CONTROL ACT COMPLIANCE REVIEW FORM

Fully and acc	curately provide the fo	ollowing	information, a	s spec	ified	. Atta	ch additional sheets as necessary.			
Type of Cor	npliance Review Fo	rm Sub	mittal (check	all tha	ıt ap	ply)				
	☐ Original Filing Date of Last Compliance Review Form Filing:									
Type of Sub										
	an Approval	Ц	New Operatin	-			Renewal of Operating Permit			
☐ Extensi☐ Other:	on of Plan Approval		Change of Ov	wnersh	iip	$\boxtimes$	Periodic Submission (@ 6 mos)			
Other.					······					
	SECT	TION A.	GENERAL A	PPLIC	ATIO	INI NC	FORMATION			
(non-corpor	olicant/Permittee/("a ations-attach docur Energy Solutions Ref	nentati	on of legal na	•						
Address	3144 Passyunk Av		<u> </u>							
	Philadelphia, PA 1									
Telephone	215-339-2000		Taxpay	er ID#	: 6	51-168	39574			
Permit, Plan	Approval or Applic	ation IC								
				plicar	nt co	nduct	s its business (check appropriate box)			
☐ Individu	_	Syndicat		_			t Agency			
☐ Municip	ality 🔲 N	⁄unicipa	al Authority	□ J	oint '	√entur	re			
☐ Propriet	orship 🗌 F	ictitious	s Name	□ A	ssoc	iation				
	•	Partners	•	□ c	ther	Туре	of Business, specify below:			
			Partnership							
	ow the type(s) of bu	ısiness	activities per	forme	d.					
Petroleum Re	fining operations.									

#### SECTION B. GENERAL INFORMATION REGARDING "APPLICANT"

If applicant is a corporation or a division or other unit of a corporation, provide the names, principal places of business, state of incorporation, and taxpayer ID numbers of all domestic and foreign parent corporations (including the ultimate parent corporation), and all domestic and foreign subsidiary corporations of the ultimate parent corporation with operations in Pennsylvania. Please include all corporate divisions or units, (whether incorporated or unincorporated) and privately held corporations. (A diagram of corporate relationships may be provided to illustrate corporate relationships.) Attach additional sheets as necessary.

Principal Places of Business	State of Incorporation	Taxpayer ID	Relationship to Applicant
Philadelphia	PA	61-1688740	Parent
Philadelphia	PA	61-1689574	Applicant
	of Business Philadelphia	of BusinessIncorporationPhiladelphiaPA	of BusinessIncorporationTaxpayer IDPhiladelphiaPA61-1688740

#### SECTION C. SPECIFIC INFORMATION REGARDING APPLICANT AND ITS "RELATED PARTIES"

Pennsylvania Facilities. List the name and location (mailing address, municipality, county), telephone number, and relationship to applicant (parent, subsidiary or general partner) of applicant and all Related Parties' places of business, and facilities in Pennsylvania. Attach additional sheets as necessary.

Unit Name	Street Address	County and Municipality	Telephone No.	Relationship to Applicant
Philadelphia Refinery Complex	3144 Passyunk Ave., Philadelphia, PA 19145	Philadelphia, Philadelphia	215-339- 2000	Applicant
Schuylkill River Tank Farm	3144 Passyunk Ave., Philadelphia, PA 19145	Philadelphia, Philadelphia	215-339- 2000	Applicant

Provide the names and business addresses of all general partners of the applicant and parent and subsidiary corporations, if any.

Name	Business Address
None	

l business address o p. plant manager).	f persons with overall mar	nagement responsibil	ity for the process
me	Bı	usiness Address	<u> </u>
1	3144 Passyunk Ave., Philac	delphia, PA 19145	
pproved local air pol ently in effect or hav This list shall inclu	lution control agency und e been in effect at any time de the plan approval and	er the APCA to the ape 5 years prior to the congression operating permit nu	oplicant or related
Plan Approval/ Operating Permit#	Location	Issuance	Expiration Date
	Operating Permits. pproved local air polently in effect or have this list shall inclusion dates. Attach action dates. Attach action dates.	Operating Permits. List all plan approvals pproved local air pollution control agency und rently in effect or have been in effect at any time. This list shall include the plan approval and ation dates. Attach additional sheets as necessary.	Derating Permits. List all plan approvals or operating permit pproved local air pollution control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agently in effect or have been in effect at any time 5 years prior to the control agency under the APCA to the agency under

Compliance Background. (Note: Copies of specific documents, if applicable, must be made available to the Department upon its request.) List all documented conduct of violations or enforcement actions identified by the Department pursuant to the APCA, regulations, terms and conditions of an operating permit or plan approval or order by applicant or any related party, using the following format grouped by source and location in reverse chronological order. Attach additional sheets as necessary. See the definition of "documented conduct" for further clarification. Unless specifically directed by the Department, deviations which have been previously reported to the Department in writing, relating to monitoring and reporting, need not be reported.

Date	Location	Plan Approval/ Operating Permit#	Nature of Documented Conduct	Type of Department Action	Status: Litigation Existing/Continuing or Corrected/Date	Dollar Amount Penalty
None						\$
						\$
						\$
						\$
						\$
						\$
						\$
						\$
						\$
						\$

List all incidents of deviations of the APCA, regulations, terms and conditions of an operating permit or plan approval or order by applicant or any related party, using the following format grouped by source and location in reverse chronological order. This list must include items both currently known and unknown to the Department. Attach additional sheets as necessary. See the definition of "deviations" for further clarification.

Date	Location	Plan Approval/ Operating Permit#	Nature of Deviation	Incident Status: Litigation Existing/Continuing Or Corrected/Date
	Philadelphia Refinery	V95-038 - issued on January 17, 2002.	Deviations are reported pursuant to the requirements in the Title V permit.	
	SRTF	V05-011 - issued on February 24, 2012.	Deviations are reported pursuant to the requirements in the Title V permit.	

CONTINUING OBLIGATION. Applicant is under a continuing obligation to update this form using the Compliance Review Supplemental Form if any additional deviations occur between the date of submission and Department action on the application.

## **VERIFICATION STATEMENT**

Subject to the penalties of Title 18 Pa.C.S. Section 4904 and 35 P.S. Section 4009(b)(2), I verify under penalty of law that I am authorized to make this verification on behalf of the Applicant/Permittee. I further verify that the information contained in this Compliance Review Form is true and complete to the best of my belief formed after reasonable inquiry. I further verify that reasonable procedures are in place to ensure that "documented conduct" and "deviations" as defined in 25 Pa Code Section 121.1 are identified and included in the information set forth in this Compliance Review Form.

| 7/12/13 | Signature | Date

Mr. Games A. Keeler

Name (Print or Type)

General Manager, PES Refinery

Title

## Attachment

Division	Source	Permit #	Issue Date	Expiration Date
Philadelphia Refinery	210 Temporary Cooling Tower	13039	5/1.2013	3/31/2014
Philadelphia Refinery	433 Flare Tip Replacement	13074	3/18/2013	3/18/2014
Philadelphia Refinery	14- unit Train Crude Unloading	13020	4/8/2013	4/8/2014
Philadelphia Refinery	2013 Tanks Degassing Permit	13009	2/6/2013	12/31.2013
Philadelphia Relinery	General Plan Approval - Tank PB 843	13001	01/22/13	07/23 14
Philadelphia Refinery	Existing air compressor and pumps (4)	12000	10/12/2012	10-12-2013
Philadelphia Refinery	Existing air compressor and pumps (4)	12001	10/12/2012	10/12/2013
Philadelphia Refinery	Existing air compressor and pumps (4)	12002	10/12/2012	10 12.2013
Philadelphia Refinery	Existing air compressor and pumps (4)	12003	10/12/2012	10/12/2013
Philadelphia Refinery	No. 4 Separator during P401B repair	12198	10/12/2012	10/12/2013
Philadelphia Refinery	WWTP Air compressors during blower repairs	12186	10/12/2012	10/12/2013
Philadelphia Refinery	WWTP Air compressors during blower repairs	12187	10/12/2012	10/12/2013
Philadelphia Refinery Philadelphia Refinery	WWTP Air compressors during blower repairs	12188	10/12/2012	10/12/2013
Philadelphia Refinery	WWTP Air compressors during blower repairs	12189	10/12/2012	10/12/2013
Philadelphia Refinery	12 diesel permits from Consent Order 2 Diesel Powered RICE flood control pumps - Owned	11362-11374	9/14/2012	9/14/2013
Philadelphia Relinery	2 Diesel Powered RICE flood control pumps - Owned  2 Diesel Powered RICE flood control pumps - Owned	12098	8/6/2012	8/6/2013
Philadelphia Refinery	1232 Incorporating NOx and SO2 limits	12099	8/6/2012	8/6/2013
Philadelphia Refinery	#2 Separator Pump Repair	11353	7/30/2012	1/28/2014
Philadelphia Relinery	433 Temporary rental HF Mitigation Water Pump (Diesel RICE)	12148	7/9/2012	7/9/2013
Philadelphia Refinery	GP 682 Temp Diesel Pump	12152	7/9/2012	7 9/2013
Philadelphia Refinery	Temp Backup Bluebird Compressor	12133	6/18/2012	6/18/2013
Philadelphia Refinery	3 Sep Remediation System	12133	6/13/2012	6/13/2013
Philadelphia Refinery	4 Temp Compressors GP WWTP	12008 - 12011	6/12/2012	6/12/2013 6/1/2013
Philadelphia Refinery	Temporary Bluebird Compressors	12128 & 12129	6/1/2012	6/2/2013
Philadelphia Refinery	PB Degreasers	12070 & 12071	5/21/2012	5/21/2013
Philadelphia Refinery	Fire and HF Mitigation RICE	11246-11352	2/23/2012	2/23/2013
Philadelphia Refinery	24P1 Diesel RICE Fire Pump	11329	2/23/2012	2/23/2013
Philadelphia Refinery	Pollock St Remediation	12013	2/21/2012	2/21/2013
Philadelphia Refinery	Penrose Remediation	11277	2/6/2012	2/6/2013
Philadelphia Refinery	Cleaver-Brooks Warehouse Boiler	11276	2/6/2012	2/5/2013
Philadelphia Refinery	2012 Tanks Degassing	11415	1/27/2012	12/31/2012
Philadelphia Refinery	Boilers/Flares/Heaters NSPS per CD	11079	9/23/2011	3/23/2013
Philadelphia Refinery	2011 Annual TO Tanks, amended	11026	9/12/2011	12/31/2012
Philadelphia Refinery	Tks 34/1205/24 Degassing	11166	7/13/2011	12/31/2011
Philadelphia Refinery	New No. 4 Fire Pump	10111	6/24/2011	6/23/2012
Philadelphia Refinery	2011 Annual TO Tanks	11026	2/4/2011	12/31/2011
Philadelphia Refinery	GP 1101 Reactivation Plan	11001	1/25/2011	7/25/2012
Philadelphia Refinery	No. 3 Boiler House, Shutdown #38 boiler	8080	11/2/2010	5/2/2012
Philadelphia Refinery	210 Unit H-201 CD NOx Permit	10180	9/9/2010	8/3/2012
Philadelphia Refinery	137 Oil/Water Separator Carbon	10186	8/6/2010	8/6/2011
Philadelphia Refinery	Tank 1051 EFR Odor Control	10185	8/6/2010	8/6/2011
Philadelphia Refinery	1232 Flare vents to RFG	10121	5/19/2010	5/19/2011
Philadelphia Refinery	1214 Tk (Bz) Seal Change to Dbl Wiper	10116	4/21/2010	10/21/2011
Philadelphia Refinery	Ther Ox for All Degassed Tks in 2010	10046	3/5/2010	12/31/2010
Philadelphia Refinery	Unit 1332 H-400/401 to SCR for CD Nox Control	9040	2/1/2010	8/2/2011
Philadelphia Refinery	Ther. Ox for PB 162 & 204	10001	1/8/2010	1/8/2011
Philadelphia Refinery	Unit 433 Flare Tip & Pilot Gas	9190	12/15/2009	12/15/2010
Philadelphia Refinery Philadelphia Refinery	Unit 433 Alt. Disposition to Unit 137 Desalter Temp Ther Ox at PB-33,37,38,39	9116	6/5/2009	6/5/2010
Philadelphia Refinery	TO for PB-33/37/38/39	9050	4/17/2009	4/17/2010
Philadelphia Refinery	Unit 137 Foul Gases Re-route	9050	4/14/2009	4/14/2010
Philadelphia Refinery	Unit 865 Improvements	9022	3/3/2009	12/31/2010
Philadelphia Refinery	Install Pollution Controls at #3 Boilerhouse	8255	2/23/2009 9/9/2008	8/23/2010
Philadelphia Refinery	Instal pumps and corrosion probes at 210	8080 8153		3/9/2010
Philadelphia Refinery	TempTher Ox at PB-34	8180	7/24/2008 7/1/2008	6/27/2009 7/1/2009
Philadelphia Refinery	Operate a thermal Oxidizer	8096		
Philadelphia Refinery	Install an LCO heat exchanger at 868	8048	5/14/2008 2/27/2008	5/14/2009 3/27/2009
Philadelphia Refinery	Reactivate PB 843 Tank	8044	2/21/2008	8/21/2009
Philadelphia Refinery	Instal UNLB at 137 F-3	7163	2/5/2008	8/5/2009
Philadelphia Refinery	Reactivate 859 Unit	6144	1/29/2008	1/29/2010
Philadelphia Refinery	Upgrade PB 128 Tank	7214	12/12/2007	6/12/2008
Philadelphia Refinery	Upgrade single mechanical pump seals	7121	11/11/2007	12/11/2008
Philadelphia Refinery	Upgrade single mechanical pump seals	7210	11/11/2007	12/11/2008
Philadelphia Refinery	Upgrade single mechanical pump seals	7210	11/11/2007	12/11/2008
Philadelphia Refinery	Upgrade single mechanical pump seals	7210	11/11/2007	12/11/2008
Philadelphia Refinery	Operate a thermal Oxidizer	7179	10/10/2007	10/10/2008
			15/11/14/10/1	10/10/2000

July 2013 Page Lof 2

## Attachment

Division	Source	Permit #	Issue Date	<b>Expiration Date</b>
Philadelphia Refinery	Temporary Thermal Oxidizer	7135	8/28/2007	8.16.2008
Philadelphia Refinery	883 Tank General Permit	7105	6/29/2007	12/29/2008
Philadelphia Refinery	231 Jumpover to 250 Tank	7026	6/13/2007	12.13.2008
Philadelphia Refinery	26th Street Bioremediation Unit Amended Permit	6710	4/30/2007	10/30/2008
Philadelphia Refinery	137 ESDV's	7077	4/24/2007	4/23/2008
Philadelphia Refinery	433 Alkylation Expansion	6050	12/4/2006	6/4/2008
Philadelphia Refinery	1733 Arsine Treater	6142	11/29/2006	11/29/2007
Philadelphia Refinery	Permit Upgrade Part 61 BWON Carbon Canister Control Systems	06111-06116	9/7/2006	9/7/2007
Philadelphia Refinery	Permit Upgrade Part 61 BWON Carbon Canister Control Systems	06111-06116	9/7/2006	9/7 2007
Philadelphia Refinery	869 Condensate Cooler (Cooling tower)	6078	6.28/2006	6.28/2007
Philadelphia Refinery	Burner Replacement 231 B101	6069	6,13,2006	6 13 2007
Philadelphia Refinery	Permit (137 Crude Unit): Installation of HE E-21D and Replacement of E-38		5 23.2006	5 23/2007
Philadelphia Refinery	866 Cat Feed Hydrotreater Modification	5219	3 7 2006	9.7.2007
Philadelphia Refinery	1232 FCCU Expansion Permit	4322	2 28/2006	5 31 2008
Philadelphia Refinery	1232 Cooling Tower Rebuild & 1232 Temporary Cooling Tower Operation	06009, 06012	2/13/2006	2 13.2007
Philadelphia Refinery	1231 & 1232 Flare Tip Maintenance Permit	05199, 05200	11/18/2005	11/17/2006
Philadelphia Refinery	1332 CRUH-2 Hydrobon Heater replacement	5124	10/4/2005	4,4/2007
Philadelphia Refinery	Replacement of 867 SRU DEA and SWS Flare tips	05122, 05123	9/6/2005	9/6/2006
Philadelphia Refinery	865 Ultra Low Sulfur Diesel Permit	4237	8/12/2005	2/12/2007
Philadelphia Refinery	North Flare Tip replacement	4209	9/27/2004	9/27/2005
			<del></del>	
Philadelphia Refinery	CCR Emergency Generator	4208	8/13/2004	8/13/2005
Philadelphia Refinery	869 Restart Plan Approval	3163	2/4/2004	8/5/2005
Philadelphia Refinery	433 SHU Plan Approval	3124	1/14/2004	7.14/2005
Philadelphia Refinery	870 Plan Approval	2184	12/29/2003	6/29/2005
Philadelphia Refinery	Installation permit; 49 MMBTU/hr gas fired heater (868 8H-101)	3039	7/29/2003	7/29/2004
Philadelphia Refinery	Tank 826	2120	7/2/2002	1/2/2007
Philadelphia Refinery	Plan Approval: FCCU 868 upgrades, including 210 H-201 LNB	184	3/22/2002	9/22/2003
Philadelphia Refinery	Title V	V95-038	1/17/2002	2/15/2007
Schuylkill River Tank Farm	Butane Unloading	12270	3/5/2013	3/5/2014
Schuylkill River Tank Farm	· · · · · · · · · · · · · · · · · · ·	12212	10/12/2012	10/12/2013
	SR-5 Oil Water Separator Studge Cleaning	12212	10/12/2012	10/12/2013
Schuylkill River Tank Farm		12131	6/1/2012	6/1/2013
Schuylkill River Tank Farm	SRTF Flare Temporary Diesel Air Compressor (RICE)	12132	6/1/2012	6/1/2013
Schuylkill River Tank Farm	Title V	V05-011	2/24/2012	2/23/2017
Schuylkill River Tank Farm	SR90 Degassing	11231	9/20/2011	12/31/2011
Schuylkill River Tank Farm	SR-59 Seal Change	10290	12/6/2010	6/6/2012
Schuylkill River Tank Farm	TO for SR-20 & GP 1218	9181	9/9/2009	9/18/2010
Schuylkill River Tank Farm	TO for SR-7	9127	4/10/2009	3/10/2010
Schuylkill River Tank Farm	Tem Ther Ox at SR-6,7,8	9048	3/31/2009	3/31/2010
Schuylkill River Tank Farm	Tem Ther Ox at SR-35,36	9043	3/23/2009	3/23/2010
Schuylkill River Tank Farm	Upgrade SR-41	8154	7/21/2008	7/21/2009
Schuylkill River Tank Farm	Upgrade SR-41	8155	7/21/2008	7/21/2009
Schuylkill River Tank Farm	Operate a thermal Oxidizer	8152	7/1/2008	7/1/2009
Schuylkill River Tank Farm	Upgrade SR-62	8097	5/16/2008	11/16/2009
Schuylkill River Tank Farm	Upgrade SR-7	8068	4/2/2008	10/2/2009
Some justin 10.001 Tank Latin	i oppines on ,	9900	7/2/2000	101212007

Page 2 of 2 July 2013

## Attachment D Emissions Calculations

#### Heater Firing Rate Increase Plan Approval Emissions

C	Pollutant (TPY)									
Source	NO <sub>x</sub>	SO <sub>2</sub>	CO	VOC	PM	PM <sub>10</sub> /PM <sub>2.5</sub>	H <sub>2</sub> SO <sub>4</sub>	Lead	HAP	CO <sub>2</sub> e
Target Heater Emissions	53.8	2.5	78.5	5.1	7.1	7.1	0	4.7E-04	0	112,420
Ancillary Upstream/Downstream Units	4.2	1.3	18.9	11.7	0.03	0.03	0	0	0	4,312
Ancillary Upstream/Downstream Unmodified Heaters/Boiler	82.1	3.2	94.2	6.3	6.1	6.1	0	6.1E-04	0	138,640
Total Plan Approval Emissions	140.1	7.1	191.6	23.2	13.2	13.2	0.0	1.1E-03	0.0	255,372

#### Step 1. PSD Emissions Analysis

Emissions	Pollutant (TPY)								
Entissions	NO <sub>2</sub>	SO <sub>2</sub>	CO	PM	PM <sub>10</sub>	$H_2SO_4$	Lead	CO₂e	
Heater Firing Rate Increase Plan Approval	140.1	7.1	191.6	13.2	13.2	0.0	1.1E-03	255,372	
PSD Significant Level	40	40	100	25	15	7	0.6	75,000	
PSD Triggered (Before Netting Analysis)	Yes	No	Yes	No	No	No	No	Yes	

#### Step 2. PSD Netting Analysis

Emissions	NO <sub>2</sub> Emissions (TPY)	CO Emissions (TPY)	CO <sub>2</sub> e Emissions (TPY)
Heater Firing Rate Increase Plan Approval	140.1	191.6	255,372
Contemporaneous Increases/Decreases	-320.7	-17.5	-310,956
Total	-180.7	174.1	-55,583
PSD Significance Level	40	100	75,000
PSD Review Required	No	Yes	No

#### NA-NSR Ozone Netting Analysis

Plan Approval	5-year NO <sub>x</sub> (TPY)	5-year VOC (TPY)
Heater Firing Rate Increase Plan Approval	140.1	23.2
Contemporaneous Increases	10.7	2.8
Net Emissions Increase	150.7	26.0
Internal Offsets required (1.3:1 Ratio)	195.9	33.8
Netting Credits Applied	-195.9	-33.8
Net Emissions (After Offsetting, if applicable)	0.0	0.0
NA-NSR Significance Level	25	25
NA-NSR Review Required	No	No

#### NA-NSR Ozone Netting Analysis

Plan Approval	10-year NO <sub>x</sub> (TPY)	10-year VOC (TPY)
Heater Firing Rate Increase Plan Approval	140.1	23.2
Contemporaneous Increases/Decreases	-296.7	-11.4
Net Emissions Increase	-156.7	11.7
NA-NSR Significance Level	25	25
NA-NSR Review Required	No	No

#### ${\rm NA\text{-}NSR~PM}_{2.5}$ Emissions Analysis

Plan Approval	SO <sub>2</sub> (TPY)	NO <sub>x</sub> (TPY)	PM <sub>2.5</sub> (TPY)
Heater Firing Rate Increase Plan Approval	7.1	140.1	13.2
NA-NSR Significance Level	40	40	10
NA-NSR Triggered (Before Netting Analysis)	No	Yes	Yes

#### NA-NSR PM<sub>2.5</sub> Netting Analysis

Plan Approval	NO <sub>x</sub> (TPY)	PM <sub>2.5</sub> (TPY)
Heater Firing Rate Increase Plan Approval	140.1	13.2
Contemporaneous Increases/Decreases	-320.7	-22.3
Net Emissions Increase	-180.7	-9.0
NA-NSR Significance Level	40	10
NA-NSR Review Required	No	No

#### PES Refinery Heater Firing Rate Increase Plan Approval Summary of Contemporaneous Period Emissions

Facility Powert No. Astroity Ef			Effective Date of	NA-NSR Net Emission Change, Ton/Yr						
Facility	Permit No.	Activity	Change	VOC	NO <sub>x</sub>	PM <sub>2.5</sub>	PM <sub>2.5</sub> /NO <sub>x</sub>	PM <sub>2.5</sub> /SO <sub>2</sub>		
Point Breeze	02184	Tier II Gasoline	12/29/2003	0.00	0.00	0.00	0.00	68.59		
Point Breeze	02184	12/29/2003	0.00	0.00	0.00	0.00	-29.70			
Marcus Hook	Delaware permit	Sulfur Recovery Unit (done in Delaware)	3/26/2003	0.40	0.00	0.56	0.00	0.00		
Point Breeze	03124	433 Alkylation Reappl.	1/4/2004	0.00	0.00	0.00	0.00	0.00		
Point Breeze	03163	869 Alky. Reactivation	2/5/2004	0.00	0.00	0.00	0.00	0.40		
Marcus Hook	Pa23-0001 U & W	LSG Revised took out Hydrogen plant etc	2/24/2004	6.40	23.00	6.20	23.00	29.77		
Point Breeze	04208	Emergency Generator	8/13/2004	0.00	0.00	0.00	0.00	0.07		
Gir. Pt./Pt. Br.	04237	865 ULSD	8/12/2005	0.00	0.00	0.00	0.00	7.36		
Gir. Pt./Pt. Br.	04322	1232 Flue Gas Treating & Expansion	2/28/2006	0.00	0.00	1.23	0.00	12.55		
Marcus Hook	De minimis	Alky cooling project- chill the feed with rental	3/3/2006	0.07	0.99	0.16	0.99	0.13		
Point Breeze	05219	866 Unit Modification for ULSD mode	3/7/2006	0.00	0.00	0.00	0.00	1.07		
Girard Point	06050	433 HFAU Process Improvement Project	12/4/2006	0.00	0.00	1.88	0.00	36.35		
Girard Point	07026	231 Imported Jet Project	6/13/2007	0.00	0.00	0.51	0.00	2.51		
Gir. Pt./Pt. Br.	06144	859 ULSD Project	1/29/2008	0.00	0.00	7.50	0.00	23.49		
Girard Point	08080	No. 3 Boiler House NO <sub>x</sub> Reduction	9/9/2008	12.52	0.00	ND*	0.00	0.00		
Girard Point RFD Unit 433 KOH Treater Lines		10/23/2008	0.01	0.19	0.01	0.19	0.05			
Point Breeze	RFD	Unit 866 Stripper Valve	12/22/2008	0.30	0.06	0.00	0.06	0.04		
Point Breeze	08255	Unit 865 Improvement Project	2/23/2009	0.97	9.42	0.27	9.42	5.94		
Girard Point	09022	Unit 137 RFG Changes	3/3/2009	0.02	0.00	0.00	0.00	0.00		
Girard Point	09116	Unit 433 ASO to Unit 137 Desalter	6/5/2009	0.02	0.00	0.00	0.00	0.00		
Marcus Hook	Pa23-0001AA	12 - 3 New Cooling Tower	10/28/2009	0.00	0.00	-0.40	0.00	0.00		
Girard Point	09040	Unit 1332 Heater SEP	2/1/2010	0.03	0.87	0.04	0.87	0.23		
Point Breeze	non permit letter	Tk 33/35 Jump-over line	11/23/2010	0.03	0.00	0.00	0.00	0.00		
Point Breeze	non permit letter	22 Boilerhouse #2/#3	1/19/2010	-0.99	-36.40	-1.41	-36.40	-1.25		
Marcus Hook	non permit letter	15-1 CRUDE HTR shutdown	8/16/2012	-5.05	-136.46	-7.02	-136.46	-0.15		
Marcus Hook	non permit letter	17-2A H-01, H-02, H-03 HTR shutdown	8/16/2012	-2.72	-57.04	-3.75	-57.04	-0.05		
Marcus Hook	non permit letter	17-2A H-04 HTR shutdown	8/16/2012	-0.35	-6.21	-0.50	-6.21	-0.01		
Marcus Hook	non permit letter	12-3 CRUDE HTR H-3006 shutdown	8/16/2012	-4.61	-89.48	-6.36	-89.48	-0.13		
Marcus Hook	non permit letter	12-3 DESULF HTR	8/16/2012	-0.33	-6.06	-0.48	-6.06	-0.01		
Marcus Hook	non permit letter	111 Cooling Towers	8/16/2012	-19.94	0.00	-10.24	0.00	0.00		
Gir. Pt./Pt. Br.	RFD	3-Unit Train - Crude Transfer Pipeline	1/18/2013	0.004	0.00	0.00	0.00	0.00		
Point Breeze	13001	Tank P-590 (PB 843) Reactivation	1/22/2013	1.24	0.27	0.05	0.27	0.18		
Gir. Pt./Pt. Br.	12270	Butane Truck Unloading at SRTF	3/5/2013	0.26	0.09	0.00	0.09	0.00		
Gir. Pt./Pt. Br.	13020	14-Unit Train - Crude Transfer Pipeline	4/8/2013	0.25	0.00	0.00	0.00	0.00		
	5-calendar year in	creases from 3rd Quarter 2013 (PES/Marcus Hook	)	2.82	10.66					
	10-year increases/d	lecreases from 3rd Quarter 2013 (PES/Marcus Hoo	k)	-11.45	-296.74					
	5-year increases/d	ecreases from 3rd Quarter 2013 (PES/Marcus Hool	()			-22.26	-320.73	28.32		

Notes:

Plan Approval 04237 triggered NSR for VOC.

Plan Approval 06144 triggered NSR for VOC & NO<sub>x</sub>. Plan Approval Application submitted January 29, 2008.

NSR contemporaneous period for VOC and  $NO_x$  is 5 calendar years (the year of modification plus back 4 more years).

Under 51 CFR Appendix S, netting analysis for PM<sub>2.5</sub> only required if project itself leads to a significant increase.

 $^{*}$  No. 3 BH PM $_{25}$  reduction may be bankable to an ERC after SIP rule change. Will need PM $_{25}$  factor from a surrogate unit test to determine the value.

Consent Decree does not allow  $\mathrm{NO}_{\mathrm{x}}$  reduction within the No. 3 Boiler House Project.

 $Tank\ P-590\ (PB\ 843)\ includes\ emissions\ from\ steam\ from\ No.\ 3\ Boiler\ House\ that\ were\ already\ permitted\ in\ No.\ 3\ Boiler\ House\ NO_x\ Reduction\ Project\ in\ 2008.$ 

#### PES Refinery Heater Firing Rate Increase Plan Approval Summary of Contemporaneous Period Emissions

F 1124	D't N	A of the	Effective Date of	PSD Net Emission Change, Ton/Yr									
Facility	Permit No.	Activity	Change	NO <sub>2</sub>	SO <sub>2</sub>	PM/PM <sub>10</sub>	CO	H <sub>2</sub> SO <sub>4</sub>	Lead	CO <sub>2</sub> e			
Girard Point	08080	No. 3 Boiler House NO <sub>x</sub> Reduction <sup>2</sup>	9/9/2008	n/a	n/a	n/a	82.40	n/a					
Girard Point	RFD	Unit 433 KOH Treater Lines	10/23/2008	0.19	0.05	0.01	0.10	n/a					
Point Breeze	RFD	Unit 866 Stripper Valve	12/22/2008	0.06	0.04	0.00	0.04	n/a					
Point Breeze	08255	Unit 865 Improvement Project	2/23/2009	9.42	5.94	0.27	12.01	n/a					
Girard Point	09022	Unit 137 RFG Changes	3/3/2009	0.00	0.00	0.00	0.00	n/a					
Girard Point	09116	Unit 433 ASO to Unit 137 Desalter	6/5/2009	0.00	0.00	0.00	0.00	n/a					
Point Breeze	06144	859 ULSD Project <sup>1</sup>	10/16/2009	note 3	23.49	7.50	87.67	n/a					
Marcus Hook	Pa23-0001AA	12 - 3 New Cooling Tower	10/28/2009	0.00	0.00	-0.40	0.00	0.00					
Girard Point	09040	Unit 1332 Heater SEP	2/1/2010	0.87	0.23	0.04	0.48	2.75					
Marcus Hook	Pa23-0001AD	CO controls for 6 WWTA diesels	5/17/2012	0.00	0.00	0.00	-1.65	0.00	0.00	0.00			
Point Breeze	non permit letter	22 Boilerhouse #2/#3	1/19/2010	-36.40	-1.25	-1.41	-0.38	n/a	0.00	-49,788			
Marcus Hook	non permit letter	15-1 CRUDE HTR shutdown	8/16/2012	-136.46	-0.15	-7.02	-77.24	n/a	0.00	-111,102			
Marcus Hook	non permit letter	17-2A H-01, H-02, H-03 HTR shutdown	8/16/2012	-57.04	-0.05	-3.75	-41.19	n/a	0.00	-44,912			
Marcus Hook	non permit letter	17-2A H-04 HTR shutdown	8/16/2012	-6.21	-0.01	-0.50	-5.25	n/a	0.00	-8,250			
Marcus Hook	non permit letter	12-3 CRUDE HTR H-3006 shutdown	8/16/2012	-89.48	-0.13	-6.36	-70.37	n/a	0.00	-92,084			
Marcus Hook	non permit letter	12-3 DESULF HTR	8/16/2012	-6.06	-0.01	-0.48	-5.09	n/a	0.00	-4,819			
Marcus Hook	non permit letter	111 Cooling Towers	8/16/2012	0.00	0.00	-10.24	0.00	n/a	0.00	0.00			
Gir. Pt./Pt. Br.	RFD	3-Unit Train - Crude Transfer Pipeline	1/18/2013	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
Point Breeze	13001	Tank P-590 (PB 843) Reactivation <sup>3</sup>	1/22/2013	0.27	0.18	0.05	0.45	0.00	0.00	0.00			
Gir. Pt./Pt. Br.	12270	Butane Truck Unloading at SRTF	3/5/2013	0.09	0.00	0.00	0.51	0.00	0.00	0.00			
Gir. Pt./Pt. Br.	13020	14-Unit Train - Crude Transfer Pipeline	4/8/2013	0.00	0.00	0.00	0.00	0.00	0.00	0.00			
	5-year increases and	decreases from 3rd Quarter 2013 (PES/Marcus Ho	ook)	-320.73	28.32	-22.26	-17.49	2.75	0.00	-310,956			

Notes:

Date of startup of Unit 859 following Plan Approval 06144 was October 16, 2009.

Net\* = Past five years (date of startup of new project back to date 5 years prior to start of construction, or back to last major PSD permit).

H<sub>2</sub>SO<sub>4</sub> is an issue with SCR installation due to small conversion of SO<sub>2</sub> to SO<sub>3</sub> and hydrolization to H<sub>2</sub>SO<sub>4</sub>.

 $<sup>3\</sup> Tank\ P-590\ (PB\ 843)\ includes\ emissions\ from\ steam\ from\ No.\ 3\ Boiler\ House\ that\ were\ already\ permitted\ in\ No.\ 3\ Boiler\ House\ NOx\ Reduction\ Project\ in\ 2008.$ 

Es allitar	Facility Permit No. Source Effective Date				Creditable Emissions Reductions, Tons								
racility	remit No.	Source	Effective Date	VOC	NO <sub>x</sub> /NO <sub>2</sub>	SO <sub>2</sub>	PM/PM <sub>10</sub> /PM <sub>2.5</sub>	CO	H <sub>2</sub> SO <sub>4</sub>	CO <sub>2</sub> e			
Point Breeze	non permit letter	22 Boilerhouse #2/#3	-0.99	-36.40	-1.25	-1.41	-0.38	n/a	-49,788				
Marcus Hook	non permit letter	15-1 CRUDE HTR shutdown	-5.05	-136.46	-0.15	-7.02	-77.24	n/a	-111,102				
Marcus Hook	non permit letter	17-2A H-01, H-02, H-03 HTR shutdown	-2.72	-57.04	-0.05	-3.75	-41.19	n/a	-44,912				
Marcus Hook	Marcus Hook non permit letter 17-2A H-04 HTR shutdown 8/16/2012					-0.01	-0.50	-5.25	n/a	-8,250			
Marcus Hook	Marcus Hook non permit letter 12-3 CRUDE HTR H-3006 shutdown 8/16/2012					-0.13	-6.36	-70.37	n/a	-92,084			
Marcus Hook	Marcus Hook non permit letter 12-3 DESULF HTR 8/16/2012					-0.01	-0.48	-5.09	n/a	-4,819			
Marcus Hook	non permit letter	111 Cooling Towers	8/16/2012	-19.94	0.00	0.00	-10.24	0.00	n/a	0			
		Total ERCs Generated		-33.97	-331.64	-1.60	-29.74	-199.50	0.00	-310,956			
	Ozone NA-NS	R 5-calendar year review netting credits required		-33.80	-195.95								
	Ozone NA	-NSR 10-year review netting credits required											
	PM2.5 NA	-NSR 5-year review netting credits required											
N	SR maximum netting	credits needed in the Heater Plan Approval Applie	cation	-33.80	-195.95	0.00	0.00	0.00		0			
	Total EF	Cs Remaining after Heater Plan Approval		-0.18	-135.69	-1.60	-29.74	-199.50	0.00	-310,956			

 $<sup>1 \ \</sup>text{The } 859 \ \text{project triggered PSD review for NO}_2. \ \text{Net emission increases for this pollutant were reset with ambient air quality modeling}.$ 

<sup>2</sup> SO<sub>2</sub> and PM reductions per No. 3 BH Consent Decree are not allowable as PSD/NSR credits.

PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Target Heaters with Proposed Increases in Firing Limits

Source	Emissions	Calculation	PM (TPY)	PM <sub>10</sub> (TPY)	PM <sub>2.5</sub> (TPY)	CO (TPY)	VOC (TPY)	NO <sub>x</sub> (TPY)	SO <sub>2</sub> (TPY)	Lead (TPY)	CO <sub>2</sub> e (TPY)
	(A) Baseline Actual Emissions (TPY)	See "Heater Monthly Emissions" tab	1.7	1.7	1.7	18.5	1.2	28.1	0.3	1.1E-04	26,515
	(B) Projected Actual Emissions (TPY)	See "Unit 231 B101 - Proj. Actual" tab	3.1	3.1	3.1	34.4	2.3	12.8	0.8	2.0E-04	49,253
H-1: 221 P101	(C) Baseline Increases (TPY)	(C) = (B) - (A)	1.4	1.4	1.4	15.9	1.0	-15.3	0.4	9.5E-05	22,738
Unit 231-B101	(D) Capable Emissions (TPY)	See "Unit 231 B101 - Capable" tab	1.5	1.5	1.5	16.8	1.1	-	0.4	1.0E-04	24,046
	(E) Capable Increases from Baseline (TPY)	(E) = (D) - (A)	-0.2	-0.2	-0.2	-1.7	-0.1	-	0.0	-1.0E-05	-2,469
	(F) Plan Approval Emissions Increase (TPY)	(F) = (C) - (E)	1.4	1.4	1.4	15.88	1.0	0.0	0.4	9.5E-05	22,738
	(A) Baseline Actual Emissions (TPY)	See "Heater Monthly Emissions" tab	1.7	1.7	1.7	18.9	1.2	26.2	0.4	1.1E-04	27,003
	(B) Projected Actual Emissions (TPY)	See "Unit 865 11H1 - Proj. Actual" tab	2.6	2.6	2.6	28.5	1.9	10.5	0.7	1.7E-04	40,777
Unit 865-11H1	(C) Baseline Increases (TPY)	(C) = (B) - (A)	0.9	0.9	0.9	9.6	0.6	-15.7	0.2	5.7E-05	13,774
OIII 865-11F11	(D) Capable Emissions (TPY)	See "Unit 865 11H1 - Capable" tab	1.9	1.9	1.9	20.8	1.4	-	0.5	1.2E-04	29,799
	(E) Capable Increases from Baseline (TPY)	(E) = (D) - (A)	0.2	0.2	0.2	2.0	0.1	-	0.1	1.2E-05	2,796
	(F) Plan Approval Emissions Increase (TPY)	(F) = (C) - (E)	0.7	0.7	0.7	7.67	0.5	0.0	0.2	4.6E-05	10,978
	(A) Baseline Actual Emissions (TPY)	See "Heater Monthly Emissions" tab	1.3	1.3	1.3	14.1	0.9	19.5	0.3	8.4E-05	20,131
	(B) Projected Actual Emissions (TPY)	See "Unit 865 11H2 - Proj. Actual"	1.8	1.8	1.8	20.4	1.3	28.3	0.5	1.2E-04	29,168
Unit 865-11H2	(C) Baseline Increases (TPY)	(C) = (B) - (A)	0.6	0.6	0.6	6.3	0.4	8.7	0.2	3.8E-05	9,038
OHI 803-11112	(D) Capable Emissions (TPY)	See "Unit 865 11H2 - Capable" tab	1.2	1.2	1.2	13.1	0.9	18.1	0.3	7.8E-05	18,698
	(E) Capable Increases from Baseline (TPY)	(E) = (D) - (A)	-0.1	-0.1	-0.1	-1.0	-0.1	-1.4	0.0	-6.0E-06	-1,432
	(F) Plan Approval Emissions Increase (TPY)	(F) = (C) - (E)	0.6	0.6	0.6	6.31	0.4	8.7	0.2	3.8E-05	9,038
	(A) Baseline Actual Emissions (TPY)	See "Heater Monthly Emissions" tab	5.2	5.2	5.2	56.9	3.7	62.1	2.0	3.4E-04	81,546
	(B) Projected Actual Emissions (TPY)	See "Unit 210 H101 - Proj. Actual"	6.1	6.1	6.1	66.9	4.4	73.1	2.7	4.0E-04	95,847
Unit 210-H101	(C) Baseline Increases (TPY)	(C) = (B) - (A)	0.9	0.9	0.9	10.0	0.7	11.0	0.7	5.9E-05	14,301
Clif 210-11101	(D) Capable Emissions (TPY)	See "Unit 210 H101 - Capable" tab	4.9	4.9	4.9	53.7	3.5	58.7	2.2	3.2E-04	76,940
	(E) Capable Increases from Baseline (TPY)	(E) = (D) - (A)	-0.3	-0.3	-0.3	-3.2	-0.2	-3.4	0.1	-1.9E-05	-4,606
	(F) Plan Approval Emissions Increase (TPY)	(F) = (C) - (E)	0.9	0.9	0.9	9.99	0.7	11.0	0.5	5.9E-05	14,301
	(A) Baseline Actual Emissions (TPY)	See "Heater Monthly Emissions" tab	5.9	5.9	5.9	65.1	4.3	20.1	2.1	3.9E-04	93,174
	(B) Projected Actual Emissions (TPY)	See "Unit 210 H201 - Proj. Actual" tab	8.0	8.0	8.0	88.5	5.8	32.6	3.2	5.3E-04	126,707
Unit 210-H201	(C) Baseline Increases (TPY)	(C) = (B) - (A)	2.1	2.1	2.1	23.4	1.5	12.5	1.1	1.4E-04	33,532
Clif 210-11201	(D) Capable Emissions (TPY)	See "Unit 210 H201 - Capable" tab	5.9	5.9	5.9	65.2	4.3	16.9	2.3	3.9E-04	93,422
	(E) Capable Increases from Baseline (TPY)	(E) = (D) - (A)	0.0	0.0	0.0	0.2	0.0	-3.1	0.2	1.0E-06	248
	(F) Plan Approval Emissions Increase (TPY)	(F) = (C) - (E)	2.1	2.1	2.1	23.24	1.5	12.5	0.8	1.4E-04	33,284
	(A) Baseline Actual Emissions (TPY)	See "Heater Monthly Emissions" tab	0.6	0.6	0.6	6.6	0.4	9.1	0.2	3.9E-05	9,446
	(B) Projected Actual Emissions (TPY)	See "Unit 866 12H1 - Proj. Actual" tab	1.7	1.7	1.7	18.6	1.2	25.8	0.5	1.1E-04	26,601
Unit 866-12H1	(C) Baseline Increases (TPY)	(C) = (B) - (A)	1.1	1.1	1.1	12.0	0.8	16.6	0.3	7.1E-05	17,156
CIII 000 12111	(D) Capable Emissions (TPY)	See "Unit 866 12H1 - Capable" tab	0.5	0.5	0.5	5.8	0.4	8.1	0.2	3.5E-05	8,367
	(E) Capable Increases from Baseline (TPY)	(E) = (D) - (A)	-0.1	-0.1	-0.1	-0.8	0.0	-1.0	0.0	-4.5E-06	-1,078
	(F) Plan Approval Emissions Increase (TPY)	(F) = (C) - (E)	1.1	1.1	1.1	11.98	0.8	16.6	0.3	7.1E-05	17,156
	(A) Baseline Actual Emissions (TPY)	See "Heater Monthly Emissions" tab	1.2	1.2	1.2	13.2	0.9	19.0	0.4	7.8E-05	18,877
	(B) Projected Actual Emissions (TPY)	See "Unit 868 8H101 - Proj. Actual" tab	1.7	1.7	1.7	18.9	1.2	27.1	0.6	1.1E-04	27,054
Unit 868-8H101	(C) Baseline Increases (TPY)	(C) = (B) - (A)	0.5	0.5	0.5	5.7	0.4	8.1	0.2	3.4E-05	8,177
C111 000 011101	(D) Capable Emissions (TPY)	See "Unit 868 8H101 - Capable" tab	1.4	1.4	1.4	15.5	1.0	22.2	0.5	9.2E-05	22,130
	(E) Capable Increases from Baseline (TPY)	(E) = (D) - (A)	0.2	0.2	0.2	2.3	0.1	3.2	0.1	1.4E-05	3,253
	(F) Plan Approval Emissions Increase (TPY)	(F) = (C) - (E)	0.3	0.3	0.3	3.44	0.2	4.9	0.1	2.0E-05	4,924
	(A) Baseline Actual Emissions (TPY)	Sum of all (A) rows above	17.5	17.5	17.5	193.2	12.7	184.1	5.8	1.2E-03	276,692
	(B) Projected Actual Emissions (TPY)	Sum of all (B) rows above	25.0	25.0	25.0	276.1	18.1	210.2	9.0	1.6E-03	395,408
Total	(C) Baseline Increases (TPY)	Sum of all (C) rows above	7.5	7.5	7.5	82.9	5.4	26.0	3.1	4.9E-04	118,716
10	(D) Capable Emissions (TPY)	Sum of all (D) rows above	17.3	17.3	17.3	190.9	12.5	124.0	6.4	1.1E-03	273,402
	(E) Capable Increases from Baseline (TPY)	Sum of all (E) rows above	-0.2	-0.2	-0.2	-2.3	-0.2	-60.1	0.5	-1.4E-05	-3,289
	Plan Approval Emissions Increase (TPY)	Sum of all (F) rows above	7.1	7.1	7.1	78.5	5.1	53.8	2.5	4.7E-04	112,420

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 2310-B101 Heater Projected Actual Emissions Analysis

Day	
Fig.   Unit 231-B101 Heater Future Annual Average Firing Rate   S7.75 MMBtu/hr   C  Unit 231-B101 Heater Future Hourly Maximum Firing Rate   S66,000 MMBtu/yr   S66	
C  Unit 231-B101 Heater Future Hourly Maximum Firing Rate   585,000 MMBtu/hr   590,000 MMBtu/hr   585,000	
D	
Fig.   Higher heating value of fuel gas   = 1,045.2 Btu/scf   24 month average of HHV of fuel gas   Fig.   SO <sub>2</sub> EF   = 0.0019   lb/MMBtu   Based on 2011 SO <sub>2</sub> emissions from Emission Inventory   Design rate for new ULNBs     Higher heating value of fuel gas   = 0.0010   lb/MMBtu   Design rate for new ULNBs     Higher heating value of fuel gas   = 0.030   lb/MMBtu   Design rate for new ULNBs     Higher heating value of fuel gas   = 0.030   lb/MMBtu   Design rate for new ULNBs     Higher heating value of fuel gas   = 0.030   lb/MMBtu   Design rate for new ULNBs     AP-42; 7/98; Table 1.4-2	
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$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
$ [H] \   PM  EF \\ [I] \   PM_{10}  EF \\ [I] \   PM_{10}  EF \\ [I] \   PM_{25}  Projected  Actual Emissions \\ [I] \   PM_{25}  Pro$	
$ [M]  SO_2 \text{ Projected Actual Emissions} \\ [N]  NO_x \text{ Projected Actual Emissions} \\ [O]  PM \text{ Projected Actual Emissions} \\ [O]  PM \text{ Projected Actual Emissions} \\ [O]  PM_{10} \text{ Projected Actual Emissions} \\ [O]  PM_{10} \text{ Projected Actual Emissions} \\ [O]  PM_{10} \text{ Projected Actual Emissions} \\ [O]  PM_{25}  Projected Actual Emis$	
$ [N]  NO_x \text{ Projected Actual Emissions } = 12.8 \text{ tpy } = [D] * [G] / 2000 \\ [O]  PM \text{ Projected Actual Emissions } = 3.1 \text{ tpy } = [D] * [H] / [E] / 2000 \\ [P]  PM_{10} \text{ Projected Actual Emissions } = 3.1 \text{ tpy } = [D] * [I] / [E] / 2000 \\ [Q]  PM_{2.5} \text{ Projected Actual Emissions } = 3.1 \text{ tpy } = [D] * [I] / [E] / 2000 \\ [R]  CO \text{ Projected Actual Emissions } = 34.4 \text{ tpy } = [D] * [K] / [E] / 2000 \\ [S]  VOC \text{ Projected Actual Emissions } = 2.3 \text{ tpy } = [D] * [L] / [E] / 2000 \\ [T]  CO_2 \text{ EF } = 53.02 \text{ kg/MMBtu } 40 \text{ CFR 98 Table C-1} \\ [U]  CH_4 \text{ EF } = 0.001 \text{ kg/MMBtu } 40 \text{ CFR 98 Table C-2} \\ [V]  N_2O \text{ EF } = 0.0001 \text{ kg/MMBtu } 40 \text{ CFR 98 Table C-2} \\ [W]  Default \text{ HHV } = 0.001028 \text{ MMBtu/scf} 40 \text{ CFR 98 Table C-1} \\ [X]  \text{Adjusted CO}_2 \text{ EF } = 52.15 \text{ kg/MMBtu } = [T] * [W] / 1,000,000 * [E] $	
$ [O] \  \   PM \   Projected \   Actual \   Emissions \\ [P] \   PM_{10} \   Projected \   Actual \   Emissions \\ [Q] \   PM_{2.5} \   Projected \   Actual \   Emissions \\ [R] \   CO \$	
$ \begin{array}{llllllllllllllllllllllllllllllllllll$	
$ [R]  \text{CO Projected Actual Emissions} \\ [S]  \text{VOC Projected Actual Emissions} \\ [S]  \text{VOC Projected Actual Emissions} \\ [T]  \text{CO}_2 \text{ EF} \\ [U]  \text{CH}_4 \text{ EF} \\ [V]  \text{N}_2 \text{O EF} \\ [W]  \text{Default HHV} \\ [X]  \text{Adjusted CO}_2 \text{ EF} \\ [V]  \text{N}_2 \text{O EF} \\ [V]  \text{N}_2 \text{O EF} \\ [V]  \text{Default HMV} \\ [V]  \text{Default CO}_2 \text{ EF} \\ [V]  \text{Default MBtu} \\ [V]  \text{Default CO}_2 \text{ EF} \\ [V]  \text{Default MBtu} \\ [V]  \text$	
$ [S] \ \ VOC \ Projected \ Actual \ Emissions \\ [T] \ \ CO_2 \ EF \\ [U] \ \ CH_4 \ EF \\ [V] \ \ N_2O \ EF \\ [W] \ \ Default \ HHV \\ [X] \ \ Adjusted \ CO_2 \ EF \\ [X] \ \ \ Adjusted \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	
$ \begin{array}{llllllllllllllllllllllllllllllllllll$	
[W] Default HHV = $0.001028 \text{ MMBtu/scf}$ 40 CFR 98 Table C-1 [X] Adjusted CO <sub>2</sub> EF = $52.15 \text{ kg/MMBtu}$ = [T] * [W] / $1,000,000 \text{ *}$ [E]	
[X] Adjusted $CO_2$ EF = 52.15 kg/MMBtu = [T] * [W] / 1,000,000 * [E]	
_	
[Z] Adjusted $N_2O$ EF = 0.0001 kg/MMBtu = [V] * [W] / 1,000,000 * [E]	
[AA] CH <sub>4</sub> Global Warming Potential = 21 40 CFR 98 Table A-1	
[AB] $N_2$ O Global Warming Potential = 310 40 CFR 98 Table A-1	
[AC] CO <sub>2</sub> e Projected Actual Emissions = $49,253 \text{ tpy CO}_{2}e$ = $(([D] * [X]) + ([D] * [X]) + ($	
[AD] Lead EF = $0.0005 \text{ lb/MMscf}$ AP-42; 7/98; Table 1.4-2	
[AE] Lead Projected Actual Emissions = $2.0\text{E-}04 \text{ tpy}$ = [D] * [AD] / [E] / 2000	
[AF] SO <sub>2</sub> maximum hourly $= 0.2 \text{ lb/hr} = [C] * [F]$	
[AG] $NO_x$ maximum hourly = 3.1 lb/hr = [C] * [G]	
[AH] PM maximum hourly $= 0.8 \text{ lb/hr} = [C] * [H] / [E]$	
[AI] $PM_{10}$ maximum hourly = 0.8 lb/hr = [C] * [I] / [E]	
[AJ] $PM_{2.5}$ maximum hourly = $0.8 \text{ lb/hr}$ = $[C] * [J] / [E]$	
[AK] CO maximum hourly $= 8.4 \text{ lb/hr} = [C] * [K] / [E]$	
[AL] VOC maximum hourly $= 0.5 \text{ lb/hr} = [C] * [L] / [E]$	
[AM] Lead maximum hourly $= 5.0\text{E-}05 \text{ lb/hr} = [\text{C}] * [\text{AD}] / [\text{E}]$	

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 231-B101 Heater Capable of Accommodating Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 231-B101 Heater Current Firing Rate Limit	=	91.00 MMBtu/hr	
[B]	Unit 231-B101 Heater Maximum Monthly Firing Rate	=	34,825 MMBtu/month	•
[C]	Unit 231-B101 Heater Maximum Monthly Firing Rate	=	48.37 MMBtu/hr	24 month period
[D]	Annual Firing Rate Projected from Maximum Monthly Rate	=	417,902 MMBtu/yr	= [B] * 12
[E]	Higher heating value of fuel gas	=	1,045.2 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0019 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	NO <sub>x</sub> EF	=	0.122 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	$PM_{2.5}$ EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	$SO_2$ PTE	=	0.4 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> PTE	=	25.5 tpy	= [D] * [G] / 2000
[O]	PM PTE	=	1.5 tpy	= [D] * [H] / [E] / 2000
[P]	$PM_{10}$ PTE	=	1.5 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> PTE	=	1.5 tpy	= [D] * [J] / [E] / 2000
[R]	CO PTE	=	16.8 tpy	= [D] * [K] / [E] / 2000
[S]	VOC PTE	=	1.1 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.15 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
[AC]	CO <sub>2</sub> e Projected Actual Emissions	=	24,046 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead PTE	=	1.0E-04 tpy	= [D] * [AD] / [E] / 2000
			• '	

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 865-11H1 Heater Projected Actual Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 865-11H1 Heater Current Firing Rate Limit	=	72.20 MMBtu/hr	
[B]	Unit 865-11H1 Heater Future Annual Average Firing Rate	=	79.75 MMBtu/hr	
[C]	Unit 865-11H1 Heater Future Hourly Maximum Firing Rate	=	87.30 MMBtu/hr	
[D]	Projected Maximum Annual Firing Rate	=	699,000 MMBtu/yr	= [B] * 8760 (Rounded to nearest thousand MMBtu)
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0019 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	$NO_x$ EF	=	0.030 lb/MMBtu	Design rate for new ULNBs
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> Projected Actual Emissions	=	0.7 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> Projected Actual Emissions	=	10.5 tpy	= [D] * [G] / 2000
[O]	PM Projected Actual Emissions	=	2.6 tpy	= [D] * [H] / [E] / 2000
[P]	PM <sub>10</sub> Projected Actual Emissions	=	2.6 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> Projected Actual Emissions	=	2.6 tpy	= [D] * [J] / [E] / 2000
[R]	CO Projected Actual Emissions	=	28.5 tpy	= [D] * [K] / [E] / 2000
[S]	VOC Projected Actual Emissions	=	1.9 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
	CO <sub>2</sub> e Projected Actual Emissions	=	40,777 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead Projected Actual Emissions	=	1.7E-04 tpy	= [D] * [AD] / [E] / 2000
	SO <sub>2</sub> maximum hourly	=	0.2 lb/hr	= [C] * [F]
	NO <sub>x</sub> maximum hourly	=	2.6 lb/hr	= [C] * [G]
	PM maximum hourly	=	0.6 lb/hr	= [C] * [H] / [E]
	PM <sub>10</sub> maximum hourly	=	0.6 lb/hr	= [C] * [I] / [E]
	PM <sub>25</sub> maximum hourly	=	0.6 lb/hr	= [C] * [J] / [E]
	CO maximum hourly	=	7.1 lb/hr	= [C] * [K] / [E]
	VOC maximum hourly	=	0.5 lb/hr	= [C] * [L] / [E]
	Lead maximum hourly	=	4.2E-05 lb/hr	= [C] * [AD] / [E]

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 865-11H1 Heater Capable of Accommodating Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 865-11H1 Heater Current Firing Rate Limit	=	72.20 MMBtu/hr	
[B]	Unit 865-11H1 Heater Maximum Monthly Firing Rate	=	42,568 MMBtu/month	•
[C]	Unit 865-11H1 Heater Maximum Monthly Firing Rate	=	59.12 MMBtu/hr	24 month period
[D]	Annual Firing Rate Projected from Maximum Monthly Rate	=	510,810 MMBtu/yr	= [B] * 12
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0019 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	NO <sub>x</sub> EF	=	0.113 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[]]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as PM <sub>10</sub> emission factor
[K]	COEF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> PTE		0.5 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> PTE	=	28.9 tpy	= [D] * [G] / 2000
[O]	PM PTE	=	1.9 tpy	= [D] * [H] / [E] / 2000
[P]	PM <sub>10</sub> PTE	=	1.9 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> PTE	=	1.9 tpy	= [D] * [J] / [E] / 2000
[R]	COPTE	=	20.8 tpy	= [D] * [K] / [E] / 2000
[S]	VOC PTE	=	1.4 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
	CO <sub>2</sub> e Projected Actual Emissions	=	29,799 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
[AE]	Lead PTE	=	1.2E-04 tpy	= [D] * [AD] / [E] / 2000

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 865-11H2 Heater Projected Actual Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 865-11H2 Heater Current Firing Rate Limit	=	49.90 MMBtu/hr	
[B]	Unit 865-11H2 Heater Future Annual Average Firing Rate	=	57.05 MMBtu/hr	
[C]	Unit 865-11H2 Heater Future Hourly Maximum Firing Rate	=	64.20 MMBtu/hr	
[D]	Projected Maximum Annual Firing Rate	=	500,000 MMBtu/yr	= [B] * 8760 (Rounded to nearest thousand MMBtu)
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0020 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	$NO_x$ EF	=	0.113 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> Projected Actual Emissions	=	0.5 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> Projected Actual Emissions	=	28.3 tpy	= [D] * [G] / 2000
[O]	PM Projected Actual Emissions	=	1.8 tpy	= [D] * [H] / [E] / 2000
[P]	PM <sub>10</sub> Projected Actual Emissions	=	1.8 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> Projected Actual Emissions	=	1.8 tpy	= [D] * [J] / [E] / 2000
[R]	CO Projected Actual Emissions	=	20.4 tpy	= [D] * [K] / [E] / 2000
[S]	VOC Projected Actual Emissions	=	1.3 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
	CO <sub>2</sub> e Projected Actual Emissions	=	29,168 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead Projected Actual Emissions	=	1.2E-04 tpy	= [D] * [AD] / [E] / 2000
	SO <sub>2</sub> maximum hourly	=	0.1 lb/hr	= [C] * [F]
	NO <sub>x</sub> maximum hourly	=	7.3 lb/hr	= [C] * [G]
	PM maximum hourly	=	0.5 lb/hr	= [C] * [H] / [E]
	PM <sub>10</sub> maximum hourly	=	0.5 lb/hr	= [C] * [I] / [E]
	PM <sub>25</sub> maximum hourly	=	0.5 lb/hr	= [C] * [J] / [E]
	CO maximum hourly	=	5.2 lb/hr	= [C] * [K] / [E]
	VOC maximum hourly	=	0.3 lb/hr	= [C] * [L] / [E]
	Lead maximum hourly	=	3.1E-05 lb/hr	= [C] * [AD] / [E]

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 865-11H2 Heater Capable of Accommodating Emissions Analysis

ID	Parameter		Value Units	Source/Basis
[A]	Unit 865-11H2 Heater Current Firing Rate Limit	=	49.90 MMBtu/hr	
[B]	Unit 865-11H2 Heater Maximum Monthly Firing Rate	=	26,710 MMBtu/month	
[C]	Unit 865-11H2 Heater Maximum Monthly Firing Rate	=	37.10 MMBtu/hr	24 month period
[D]	Annual Firing Rate Projected from Maximum Monthly Rate	=	320,524 MMBtu/yr	= [B] * 12
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	$SO_2$ EF	=	0.0020 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	$NO_x$ EF	=	0.113 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as PM <sub>10</sub> emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	$SO_2$ PTE	=	0.3 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> PTE	=	18.1 tpy	= [D] * [G] / 2000
[O]	PM PTE	=	1.2 tpy	= [D] * [H] / [E] / 2000
[P]	$PM_{10}$ PTE	=	1.2 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> PTE	=	1.2 tpy	= [D] * [J] / [E] / 2000
[R]	CO PTE	=	13.1 tpy	= [D] * [K] / [E] / 2000
[S]	VOC PTE	=	0.9 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
[AC]	CO <sub>2</sub> e Projected Actual Emissions	=	18,698 tpy CO₂e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
[AD]	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
[AE]	Lead PTE	=	7.8E-05 tpy	= [D] * [AD] / [E] / 2000

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 210-H101 Heater Projected Actual Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 210-H101 Heater Current Firing Rate Limit	=	183.00 MMBtu/hr	
[B]	Unit 210-H101 Heater Future Annual Average Firing Rate	=	187.50 MMBtu/hr	
[C]	Unit 210-H101 Heater Future Hourly Maximum Firing Rate	=	192.00 MMBtu/hr	
[D]	Projected Maximum Annual Firing Rate	=	1,643,000 MMBtu/yr	= [B] * 8760 (Rounded to nearest thousand MMBtu)
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0033 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	$NO_x$ EF	=	0.089 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> Projected Actual Emissions	=	2.7 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> Projected Actual Emissions	=	73.1 tpy	= [D] * [G] / 2000
[O]	PM Projected Actual Emissions	=	6.1 tpy	= [D] * [H] / [E] / 2000
[P]	PM <sub>10</sub> Projected Actual Emissions	=	6.1 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> Projected Actual Emissions	=	6.1 tpy	= [D] * [J] / [E] / 2000
[R]	CO Projected Actual Emissions	=	66.9 tpy	= [D] * [K] / [E] / 2000
[S]	VOC Projected Actual Emissions	=	4.4 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
	CO <sub>2</sub> e Projected Actual Emissions	=	95,847 tpy CO₂e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead Projected Actual Emissions	=	4.0E-04 tpy	= [D] * [AD] / [E] / 2000
	SO <sub>2</sub> maximum hourly	=	0.6 lb/hr	= [C] * [F]
[AG]	NO <sub>x</sub> maximum hourly	=	17.1 lb/hr	= [C] * [G]
	PM maximum hourly	=	1.4 lb/hr	= [C] * [H] / [E]
		=	1.4 lb/hr	= [C] * [I] / [E]
	PM <sub>2.5</sub> maximum hourly	=	1.4 lb/hr	= [C] * [J] / [E]
[AK]	CO maximum hourly	=	15.6 lb/hr	= [C] * [K] / [E]
	VOC maximum hourly	=	1.0 lb/hr	= [C] * [L] / [E]
[AM]	Lead maximum hourly	=	9.3E-05 lb/hr	= [C] * [AD] / [E]

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 210-H101 Heater Capable of Accommodating Emissions Analysis

ID	Parameter		Value Units	Source/Basis
[A]	Unit 210-H101 Heater Current Firing Rate Limit	=	183.00 MMBtu/hr	
[B]	Unit 210-H101 Heater Maximum Monthly Firing Rate	=	109,908 MMBtu/month	1
[C]	Unit 210-H101 Heater Maximum Monthly Firing Rate	=	152.65 MMBtu/hr	24 month period
[D]	Annual Firing Rate Projected from Maximum Monthly Rate	=	1,318,899 MMBtu/yr	= [B] * 12
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	$SO_2$ EF	=	0.0033 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	$NO_x$ EF	=	0.089 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as PM <sub>10</sub> emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	$SO_2$ PTE	=	2.2 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> PTE	=	58.7 tpy	= [D] * [G] / 2000
[O]	PM PTE	=	4.9 tpy	= [D] * [H] / [E] / 2000
[P]	$PM_{10}$ PTE	=	4.9 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> PTE	=	4.9 tpy	= [D] * [J] / [E] / 2000
[R]	COPTE	=	53.7 tpy	= [D] * [K] / [E] / 2000
[S]	VOC PTE	=	3.5 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
[AC]	CO <sub>2</sub> e Projected Actual Emissions	=	76,940 tpy CO₂e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
[AD]	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
[AE]	Lead PTE	=	3.2E-04 tpy	= [D] * [AD] / [E] / 2000

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 210-H201 Heater Projected Actual Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 210-H201 Heater Current Firing Rate Limit	=	242.00 MMBtu/hr	
[B]	Unit 210-H201 Heater Future Annual Average Firing Rate	=	248.00 MMBtu/hr	
[C]	Unit 210-H201 Heater Future Hourly Maximum Firing Rate	=	254.00 MMBtu/hr	
[D]	Projected Maximum Annual Firing Rate	=	2,172,000 MMBtu/yr	= [B] * 8760 (Rounded to nearest thousand MMBtu)
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0029 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	NO <sub>x</sub> EF	=	0.030 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> Projected Actual Emissions	=	3.2 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> Projected Actual Emissions	=	32.6 tpy	= [D] * [G] / 2000
[O]	PM Projected Actual Emissions	=	8.0 tpy	= [D] * [H] / [E] / 2000
[P]	PM <sub>10</sub> Projected Actual Emissions	=	8.0 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> Projected Actual Emissions	=	8.0 tpy	= [D] * [J] / [E] / 2000
[R]	CO Projected Actual Emissions	=	88.5 tpy	= [D] * [K] / [E] / 2000
[S]	VOC Projected Actual Emissions	=	5.8 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
	CO <sub>2</sub> e Projected Actual Emissions	=	126,707 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead Projected Actual Emissions	=	5.3E-04 tpy	= [D] * [AD] / [E] / 2000
	SO <sub>2</sub> maximum hourly	=	0.7 lb/hr	= [C] * [F]
	NO <sub>x</sub> maximum hourly	=	7.6 lb/hr	= [C] * [G]
	PM maximum hourly	=	1.9 lb/hr	= [C] * [H] / [E]
	PM <sub>10</sub> maximum hourly	=	1.9 lb/hr	= [C] * [I] / [E]
	PM <sub>2.5</sub> maximum hourly	=	1.9 lb/hr	= [C] * [J] / [E]
[AK]	CO maximum hourly	=	20.7 lb/hr	= [C] * [K] / [E]
	VOC maximum hourly	=	1.4 lb/hr	= [C] * [L] / [E]
	Lead maximum hourly	=	1.2E-04 lb/hr	= [C] * [AD] / [E]

ID	Parameter		Value Units	Source / Basis
[A]	Unit 210-H201 Heater Current Firing Rate Limit	=	242.00 MMBtu/hr	
[B]	Unit 210-201 Heater Maximum Monthly Firing Rate	=	133,453 MMBtu/month	
[C]	Unit 210-H201 Heater Maximum Monthly Firing Rate	=	185.35 MMBtu/hr	24 month period
[D]	Annual Firing Rate Projected from Maximum Monthly Rate	=	1,601,440 MMBtu/yr	= [B] * 12
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0029 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	NO <sub>x</sub> EF	=	0.021 lb/MMBtu	Actual NOx emission rate during June 2010
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as PM <sub>10</sub> emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	$SO_2$ PTE	=	2.3 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> PTE	=	16.9 tpy	= [D] * [G] / 2000
[O]	PM PTE	=	5.9 tpy	= [D] * [H] / [E] / 2000
[P]	$PM_{10}$ PTE	=	5.9 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> PTE	=	5.9 tpy	= [D] * [J] / [E] / 2000
[R]	COPTE	=	65.2 tpy	= [D] * [K] / [E] / 2000
[S]	VOC PTE	=	4.3 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
	CO <sub>2</sub> e Projected Actual Emissions	=	93,422 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
[AD]	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
[AE]	Lead PTE	=	3.9E-04 tpy	= [D] * [AD] / [E] / 2000

	10-H201 Actua		n rates
Month	MMBtu fired	Tons NO <sub>x</sub>	lb/MMBtu
1/1/2010	167,474	2.44	0.029
2/1/2010	145,603	1.99	0.027
3/1/2010	148,902	1.78	0.024
4/1/2010	135,703	1.51	0.022
5/1/2010	139,001	1.41	0.020
6/1/2010	133,453	1.41	0.021
7/1/2010	132,743	1.41	0.021
8/1/2010	161,623	1.98	0.024
9/1/2010	141,423	1.72	0.024
10/1/2010	137,769	1.65	0.024
11/1/2010	143,317	1.87	0.026
12/1/2010	133,952	1.57	0.023
1/1/2011	131,607	1.45	0.022
2/1/2011	119,956	1.08	0.018
3/1/2011	116,369	1.39	0.024
4/1/2011	104,737	1.33	0.025
5/1/2011	122,289	1.60	0.026
6/1/2011	115,614	1.52	0.026
7/1/2011	111,253	1.60	0.029
8/1/2011	88,518	1.23	0.028
9/1/2011	122,327	2.28	0.037
10/1/2011	149,238	2.19	0.029
11/1/2011	143,349	1.84	0.026
12/1/2011	152,579	1.90	0.025

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 866-12H1 Heater Projected Actual Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 866-12H1 Heater Current Firing Rate Limit	=	43.00 MMBtu/hr	
[B]	Unit 866-12H1 Heater Future Annual Average Firing Rate	=	52.10 MMBtu/hr	
[C]	Unit 866-12H1 Heater Future Hourly Maximum Firing Rate	=	61.20 MMBtu/hr	
[D]	Projected Maximum Annual Firing Rate	=	456,000 MMBtu/yr	= [B] * 8760 (Rounded to nearest thousand MMBtu)
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0022 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	$NO_x$ EF	=	0.113 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> Projected Actual Emissions	=	0.5 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> Projected Actual Emissions	=	25.8 tpy	= [D] * [G] / 2000
[O]	PM Projected Actual Emissions	=	1.7 tpy	= [D] * [H] / [E] / 2000
[P]	PM <sub>10</sub> Projected Actual Emissions	=	1.7 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> Projected Actual Emissions	=	1.7 tpy	= [D] * [J] / [E] / 2000
[R]	CO Projected Actual Emissions	=	18.6 tpy	= [D] * [K] / [E] / 2000
[S]	VOC Projected Actual Emissions	=	1.2 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH₄ EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
[AC]	CO <sub>2</sub> e Projected Actual Emissions	=	26,601 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead Projected Actual Emissions	=	1.1E-04 tpy	= [D] * [AD] / [E] / 2000
	SO <sub>2</sub> maximum hourly	=	0.1 lb/hr	= [C] * [F]
[AG]	NO <sub>x</sub> maximum hourly	=	6.9 lb/hr	= [C] * [G]
[AH]	PM maximum hourly	=	0.5 lb/hr	= [C] * [H] / [E]
[AI]	PM <sub>10</sub> maximum hourly	=	0.5 lb/hr	= [C] * [I] / [E]
	PM <sub>2.5</sub> maximum hourly	=	0.5 lb/hr	= [C] * [J] / [E]
[AK]	CO maximum hourly	=	5.0 lb/hr	= [C] * [K] / [E]
[AL]	VOC maximum hourly	=	0.3 lb/hr	= [C] * [L] / [E]
[AM]	Lead maximum hourly	=	3.0E-05 lb/hr	= [C] * [AD] / [E]

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 866-12H1 Heater Capable of Accommodating Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 866-12H1 Heater Current Firing Rate Limit	=	43.00 MMBtu/hr	
[B]	Unit 866-12H1 Heater Maximum Monthly Firing Rate	=	11,953 MMBtu/month	•
[C]	Unit 866-12H1 Heater Maximum Monthly Firing Rate	=	16.60 MMBtu/hr	24 month period
[D]	Annual Firing Rate Projected from Maximum Monthly Rate	=	143,435 MMBtu/yr	= [B] * 12
[E]	Higher heating value of fuel gas	=	1,030.9 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0022 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	NO <sub>x</sub> EF	=	0.113 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	$PM_{2.5}$ EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	$SO_2$ PTE	=	0.2 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> PTE	=	8.1 tpy	= [D] * [G] / 2000
[O]	PM PTE	=	0.5 tpy	= [D] * [H] / [E] / 2000
[P]	$PM_{10}$ PTE	=	0.5 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> PTE	=	0.5 tpy	= [D] * [J] / [E] / 2000
[R]	CO PTE	=	5.8 tpy	= [D] * [K] / [E] / 2000
[S]	VOC PTE	=	0.4 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	52.87 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
[AC]	CO <sub>2</sub> e Projected Actual Emissions	=	8,367 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead PTE	=	3.5E-05 tpy	= [D] * [AD] / [E] / 2000
			• /	

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 868-8H101 Heater Projected Actual Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 868-8H101 Heater Current Firing Rate Limit	=	49.50 MMBtu/hr	
[B]	Unit 868-8H101 Heater Future Annual Average Firing Rate	=	54.75 MMBtu/hr	
[C]	Unit 868-8H101 Heater Future Hourly Maximum Firing Rate	=	60.00 MMBtu/hr	
[D]	Projected Maximum Annual Firing Rate	=	480,000 MMBtu/yr	= [B] * 8760 (Rounded to nearest thousand MMBtu)
[E]	Higher heating value of fuel gas	=	1,067.0 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0026 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	$NO_x$ EF	=	0.113 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as $PM_{10}$ emission factor
[K]	CO EF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> Projected Actual Emissions	=	0.6 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> Projected Actual Emissions	=	27.1 tpy	= [D] * [G] / 2000
[O]	PM Projected Actual Emissions	=	1.7 tpy	= [D] * [H] / [E] / 2000
[P]	PM <sub>10</sub> Projected Actual Emissions	=	1.7 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> Projected Actual Emissions	=	1.7 tpy	= [D] * [J] / [E] / 2000
[R]	CO Projected Actual Emissions	=	18.9 tpy	= [D] * [K] / [E] / 2000
[S]	VOC Projected Actual Emissions	=	1.2 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	51.08 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
	CO <sub>2</sub> e Projected Actual Emissions	=	27,054 tpy CO₂e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
	Lead Projected Actual Emissions	=	1.1E-04 tpy	= [D] * [AD] / [E] / 2000
	SO <sub>2</sub> maximum hourly	=	0.2 lb/hr	= [C] * [F]
	NO <sub>x</sub> maximum hourly	=	6.8 lb/hr	= [C] * [G]
	PM maximum hourly	=	0.4 lb/hr	= [C] * [H] / [E]
	PM <sub>10</sub> maximum hourly	=	0.4 lb/hr	= [C] * [I] / [E]
	PM <sub>2.5</sub> maximum hourly	=	0.4 lb/hr	= [C] * [J] / [E]
		=	4.7 lb/hr	= [C] * [K] / [E]
	VOC maximum hourly	=	0.3 lb/hr	= [C] * [L] / [E]
	Lead maximum hourly	=	2.8E-05 lb/hr	= [C] * [AD] / [E]

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 868-8H101 Heater Capable of Accommodating Emissions Analysis

ID	Parameter		Value Units	Source / Basis
[A]	Unit 868-8H101 Heater Current Firing Rate Limit	=	49.50 MMBtu/hr	
[B]	Unit 868-8H101 Heater Maximum Monthly Firing Rate	=	32,720 MMBtu/month	±
[C]	Unit 868-8H101 Heater Maximum Monthly Firing Rate	=	45.44 MMBtu/hr	24 month period
[D]	Annual Firing Rate Projected from Maximum Monthly Rate	=	392,635 MMBtu/yr	= [B] * 12
[E]	Higher heating value of fuel gas	=	1,067.0 Btu/scf	24 month average of HHV of fuel gas
[F]	SO <sub>2</sub> EF	=	0.0026 lb/MMBtu	Based on 2011 SO <sub>2</sub> emissions from Emission Inventory
[G]	NO <sub>x</sub> EF	=	0.113 lb/MMBtu	Proposed NO <sub>x</sub> RACT Limits
[H]	PM EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[I]	$PM_{10}$ EF	=	7.6 lb/MMscf	AP-42; 7/98; Table 1.4-2
[J]	PM <sub>2.5</sub> EF	=	7.6 lb/MMscf	Assumed to be the same as PM <sub>10</sub> emission factor
[K]	COEF	=	84 lb/MMscf	AP-42; 7/98; Table 1.4-1
[L]	VOC EF	=	5.5 lb/MMscf	AP-42; 7/98; Table 1.4-2
[M]	SO <sub>2</sub> PTE	=	0.5 tpy	= [D] * [F] / 2000
[N]	NO <sub>x</sub> PTE	=	22.2 tpy	= [D] * [G] / 2000
[O]	PM PTE	=	1.4 tpy	= [D] * [H] / [E] / 2000
[P]	$PM_{10}$ PTE	=	1.4 tpy	= [D] * [I] / [E] / 2000
[Q]	PM <sub>2.5</sub> PTE	=	1.4 tpy	= [D] * [J] / [E] / 2000
[R]	COPTE	=	15.5 tpy	= [D] * [K] / [E] / 2000
[S]	VOC PTE	=	1.0 tpy	= [D] * [L] / [E] / 2000
[T]	CO <sub>2</sub> EF	=	53.02 kg/MMBtu	40 CFR 98 Table C-1
[U]	CH <sub>4</sub> EF	=	0.001 kg/MMBtu	40 CFR 98 Table C-2
[V]	$N_2O$ EF	=	0.0001 kg/MMBtu	40 CFR 98 Table C-2
[W]	Default HHV	=	0.001028 MMBtu/scf	40 CFR 98 Table C-1
[X]	Adjusted CO <sub>2</sub> EF	=	51.08 kg/MMBtu	= [T] * [W] / 1,000,000 * [E]
[Y]	Adjusted CH <sub>4</sub> EF	=	0.001 kg/MMBtu	= [U] * [W] / 1,000,000 * [E]
[Z]	Adjusted N <sub>2</sub> O EF	=	0.0001 kg/MMBtu	= [V] * [W] / 1,000,000 * [E]
[AA]	CH <sub>4</sub> Global Warming Potential	=	21	40 CFR 98 Table A-1
[AB]	N <sub>2</sub> O Global Warming Potential	=	310	40 CFR 98 Table A-1
[AC]	CO <sub>2</sub> e Projected Actual Emissions	=	22,130 tpy CO <sub>2</sub> e	= ( ([D] * [X]) + ([D] * [Y] * [AA]) + ([D] * [Z] * [AB]) ) / 1,000 * 1.102311311
[AD]	Lead EF	=	0.0005 lb/MMscf	AP-42; 7/98; Table 1.4-2
[AE]	Lead PTE	=	9.2E-05 tpy	= [D] * [AD] / [E] / 2000

**PES Refinery** Heater Firing Rate Increase Plan Approval **Target Heater Fired Duties** 

	FIRED DUTY	Total FIRED						
Month	Unit 231-B101	Unit 865-11H1	Unit 865-11H2	Unit 210-H101	Unit 210-H201	Unit 866-12H1	Unit 868-8H101	DUTY
	MMBTU	MMBTU						
Jan-10	42,375	47,785	34,153	124,270	167,474	17,754	35,848	469,660
Feb-10	35,110	45,973	31,864	112,764	145,603	18,345	32,741	422,400
Mar-10	46,464	25,650	19,329	114,528	148,902	11,094	31,858	397,826
Apr-10	43,228	42,885	29,961	116,996	135,703	12,919	30,229	411,920
May-10	43,178	47,847	29,954	112,894	139,001	11,979	36,307	421,161
Jun-10	34,825	42,568	26,710	109,908	133,453	11,953	32,720	392,137
Jul-10	34,167	45,644	27,578	113,417	132,743	13,376	23,973	390,897
Aug-10	43,897	43,338	32,173	116,118	161,623	15,245	35,846	448,240
Sep-10	42,980	38,133	29,818	109,541	141,423	13,665	19,965	395,526
Oct-10	37,453	44,274	33,225	119,057	137,769	21,000	26,517	419,296
Nov-10	35,040	39,540	33,058	118,019	143,317	2,011	35,237	406,223
Dec-10	38,046	33,851	32,372	120,112	133,952	10,247	34,539	403,119
Jan-11	45,834	40,264	31,414	117,352	131,607	12,599	35,770	414,840
Feb-11	7,762	35,740	29,138	111,444	119,956	12,047	32,771	348,857
Mar-11	4,080	12,005	9,889	128,112	116,369	15,316	27,437	313,207
Apr-11	28,545	1,545	7,209	122,999	104,737	4,607	22,103	291,745
May-11	47,328	43,406	32,653	116,662	122,289	10,671	25,041	398,051
Jun-11	37,365	38,421	30,314	115,660	115,614	8,960	25,144	371,478
Jul-11	42,374	38,816	29,391	119,003	111,253	11,306	27,107	379,249
Aug-11	42,641	40,901	30,388	123,501	88,518	13,817	30,067	369,833
Sep-11	41,780	39,866	31,807	108,280	122,327	16,926	21,729	382,715
Oct-11	51,500	39,063	32,018	117,347	149,238	16,975	26,829	432,968
Nov-11	47,964	48,434	32,648	117,078	143,349	19,973	12,284	421,730
Dec-11	47,970	51,031	33,368	107,605	152,579	20,627	10,024	423,205
	MMBTU	1						
24-month	34,825	42,568	26,710	109,908	133,453	11,953	32,720	1
Month	Jun-10	1						
Hours per month	720	720	720	720	720	720	720	

<sup>&</sup>lt;sup>1</sup> Conservatively used the highest crude throughput month (June 2010) for the capable of accommodating (demand growth) analysis for both the target heaters and ancillary units. However, the highest crude throughput month does not coincide with the highest firing month for the target heaters (January 2010).

PES Refinery Heater Firing Rate Increase Plan Approval Total Crude Charge

Nr. at 1	GP - 137	PB - 210	Total		Total
Month <sup>1</sup>	MBbl/month	MBbl/month	MBbl/month	Days/month	MBbl/day
Jan-10	5602	3987	9589	31	309.31
Feb-10	4930	3451	8382	28	299.35
Mar-10	5304	3700	9004	31	290.45
Apr-10	5530	3797	9327	30	310.89
May-10	5660	4114	9774	31	315.28
Jun-10	5313	4183	9496	30	316.54
Jul-10	5548	4116	9664	31	311.74
Aug-10	5502	4220	9722	31	313.63
Sep-10	5160	3839	9000	30	299.99
Oct-10	4664	3834	8498	31	274.14
Nov-10	3952	3880	7832	30	261.05
Dec-10	3989	3697	7687	31	247.96
Jan-11	5314	3750	9064	31	292.39
Feb-11	1658	3254	4912	28	175.45
Mar-11	3344	3290	6634	31	214.00
Apr-11	3525	3091	6616	30	220.52
May-11	5696	3596	9292	31	299.74
Jun-11	5418	3493	8911	30	297.04
Jul-11	5801	3681	9482	31	305.87
Aug-11	5134	3364	8498	31	274.13
Sep-11	5165	3401	8566	30	285.53
Oct-11	5812	3678	9489	31	306.11
Nov-11	5408	3503	8911	30	297.02
Dec-11	5699	3562	9261	31	298.74

<sup>&</sup>lt;sup>1</sup> Conservatively used the highest crude throughput month (June 2010) for the capable of accommodating (demand growth) analysis for both the target heaters and ancillary units. However, the highest crude throughput month does not coincide with the highest firing month for the target heaters (January 2010).

#### PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Emission Factors

	231-B101 HHV	865-11H1 HHV	865-11H2 HHV	210-H101 HHV	210-H201 HHV	866-12H1 HHV	868-8H101 HHV
Period	BTU/SCF						
2010	1,063.20	1,061.85	1,061.85	1,061.85	1,061.85	1,061.85	1,116.46
2011	1,027.21	999.98	999.98	999.98	999.98	999.98	1,017.56

		AP-42 C		lb/MMBtu			
Source	PM 2010	PM 2011	CO	VOC	Lead	$NO_x$	$SO_2$
231-B101	7.6	7.6	84	5.5	0.0005	0.122	0.0019
865-11H1	7.6	7.6	84	5.5	0.0005	0.113	0.0019
865-11H2	7.6	7.6	84	5.5	0.0005	0.113	0.0020
210-H101	7.6	7.6	84	5.5	0.0005	0.089	0.0033
210-H201	7.6	7.6	84	5.5	0.0005	CEMS	0.0029
866-12H1	7.6	7.6	84	5.5	0.0005	0.113	0.0022
868-H101	7.6	7.6	84	5.5	0.0005	0.113	0.0026

	40 CFR 98 I	Emission factors (l	kg/MMBtu)				kg/MM	Btu				lb/M	MBtu
				2010 Adjusted	2010 Adjusted	2010 Adjusted	2010 Adjusted	2011 Adjusted	2011 Adjusted CH <sub>4</sub>	2011 Adjusted	2011	2010	2011
	$CO_2$	$CH_4$	N <sub>2</sub> O	CO <sub>2</sub> factor	CH₄ factor	N <sub>2</sub> O factor	CO₂e factor	CO <sub>2</sub> factor	factor	N₂O factor	Adjusted	Adjusted	Adjusted
Source				2	4	.2	2	2	ractor	-2-	CO <sub>2</sub> e factor	CO₂e factor	CO₂e factor
231-B101	53.02	0.001	0.0001	51.3	0.001	0.0001	51.3	53.1	0.001	0.0001	53.1	113.1	117.1
865-11H1	53.02	0.001	0.0001	51.3	0.001	0.0001	51.4	54.5	0.001	0.0001	54.6	113.3	120.3
865-11H2	53.02	0.001	0.0001	51.3	0.001	0.0001	51.4	54.5	0.001	0.0001	54.6	113.3	120.3
210-H101	53.02	0.001	0.0001	51.3	0.001	0.0001	51.4	54.5	0.001	0.0001	54.6	113.3	120.3
210-H201	53.02	0.001	0.0001	51.3	0.001	0.0001	51.4	54.5	0.001	0.0001	54.6	113.3	120.3
866-12H1	53.02	0.001	0.0001	51.3	0.001	0.0001	51.4	54.5	0.001	0.0001	54.6	113.3	120.3
868-H101	53.02	0.001	0.0001	48.8	0.001	0.0001	48.9	53.6	0.001	0.0001	53.6	107.7	118.2

40 CFR 98 Defaults										
GWP	$CO_2$	CH <sub>4</sub>	N <sub>2</sub> O							
GWF	1	21	310							
Default natural gas HHV (MMBtu/scf)	0.001028									

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Monthly Emissions

Ī				PM (	TPY)			
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total
Jan-10	0.15	0.17	0.12	0.44	0.60	0.06	0.12	1.67
Feb-10	0.13	0.16	0.11	0.40	0.52	0.07	0.11	1.51
Mar-10	0.17	0.09	0.07	0.41	0.53	0.04	0.11	1.42
Apr-10	0.15	0.15	0.11	0.42	0.49	0.05	0.10	1.47
May-10	0.15	0.17	0.11	0.40	0.50	0.04	0.12	1.50
Jun-10	0.12	0.15	0.10	0.39	0.48	0.04	0.11	1.40
Jul-10	0.12	0.16	0.10	0.41	0.48	0.05	0.08	1.39
Aug-10	0.16	0.16	0.12	0.42	0.58	0.05	0.12	1.60
Sep-10	0.15	0.14	0.11	0.39	0.51	0.05	0.07	1.41
Oct-10	0.13	0.16	0.12	0.43	0.49	0.08	0.09	1.50
Nov-10	0.13	0.14	0.12	0.42	0.51	0.01	0.12	1.45
Dec-10	0.14	0.12	0.12	0.43	0.48	0.04	0.12	1.44
Jan-11	0.17	0.15	0.12	0.45	0.50	0.05	0.13	1.57
Feb-11	0.03	0.14	0.11	0.42	0.46	0.05	0.12	1.32
Mar-11	0.02	0.05	0.04	0.49	0.44	0.06	0.10	1.19
Apr-11	0.11	0.01	0.03	0.47	0.40	0.02	0.08	1.10
May-11	0.18	0.16	0.12	0.44	0.46	0.04	0.09	1.51
Jun-11	0.14	0.15	0.12	0.44	0.44	0.03	0.09	1.41
Jul-11	0.16	0.15	0.11	0.45	0.42	0.04	0.10	1.44
Aug-11	0.16	0.16	0.12	0.47	0.34	0.05	0.11	1.40
Sep-11	0.15	0.15	0.12	0.41	0.46	0.06	0.08	1.45
Oct-11	0.19	0.15	0.12	0.45	0.57	0.06	0.10	1.64
Nov-11	0.18	0.18	0.12	0.44	0.54	0.08	0.05	1.60
Dec-11	0.18	0.19	0.13	0.41	0.58	0.08	0.04	1.60

		PM (TPY)										
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total				
2010	1.70	1.78	1.29	4.97	6.16	0.57	1.28	17.75				
2011	1.65	1.63	1.25	5.34	5.62	0.62	1.11	17.22				
2010-2011 average	1.68	1.71	1.27	5.15	5.89	0.60	1.19	17.48				

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Monthly Emissions

-				CO	TPY)			
Ī	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total
Jan-10	1.67	1.89	1.35	4.92	6.62	0.70	1.35	18.51
Feb-10	1.39	1.82	1.26	4.46	5.76	0.73	1.23	16.64
Mar-10	1.84	1.01	0.76	4.53	5.89	0.44	1.20	15.67
Apr-10	1.71	1.70	1.19	4.63	5.37	0.51	1.14	16.23
May-10	1.71	1.89	1.18	4.47	5.50	0.47	1.37	16.59
Jun-10	1.38	1.68	1.06	4.35	5.28	0.47	1.23	15.45
Jul-10	1.35	1.81	1.09	4.49	5.25	0.53	0.90	15.41
Aug-10	1.73	1.71	1.27	4.59	6.39	0.60	1.35	17.66
Sep-10	1.70	1.51	1.18	4.33	5.59	0.54	0.75	15.60
Oct-10	1.48	1.75	1.31	4.71	5.45	0.83	1.00	16.53
Nov-10	1.38	1.56	1.31	4.67	5.67	0.08	1.33	16.00
Dec-10	1.50	1.34	1.28	4.75	5.30	0.41	1.30	15.88
Jan-11	1.87	1.69	1.32	4.93	5.53	0.53	1.48	17.35
Feb-11	0.32	1.50	1.22	4.68	5.04	0.51	1.35	14.62
Mar-11	0.17	0.50	0.42	5.38	4.89	0.64	1.13	13.13
Apr-11	1.17	0.06	0.30	5.17	4.40	0.19	0.91	12.21
May-11	1.94	1.82	1.37	4.90	5.14	0.45	1.03	16.65
Jun-11	1.53	1.61	1.27	4.86	4.86	0.38	1.04	15.54
Jul-11	1.73	1.63	1.23	5.00	4.67	0.47	1.12	15.86
Aug-11	1.74	1.72	1.28	5.19	3.72	0.58	1.24	15.46
Sep-11	1.71	1.67	1.34	4.55	5.14	0.71	0.90	16.01
Oct-11	2.11	1.64	1.34	4.93	6.27	0.71	1.11	18.11
Nov-11	1.96	2.03	1.37	4.92	6.02	0.84	0.51	17.65
Dec-11	1.96	2.14	1.40	4.52	6.41	0.87	0.41	17.71

-		CO (TPY)										
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total				
2010	18.83	19.68	14.25	54.89	68.07	6.31	14.14	196.16				
2011	18.20	18.04	13.87	59.01	62.07	6.88	12.23	190.30				
2010-2011 average	18.52	18.86	14.06	56.95	65.07	6.60	13.18	193.23				

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Monthly Emissions

•				VOC	(TPY)			
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total
Jan-10	0.11	0.12	0.09	0.32	0.43	0.05	0.09	1.21
Feb-10	0.09	0.12	0.08	0.29	0.38	0.05	0.08	1.09
Mar-10	0.12	0.07	0.05	0.30	0.39	0.03	0.08	1.03
Apr-10	0.11	0.11	0.08	0.30	0.35	0.03	0.07	1.06
May-10	0.11	0.12	0.08	0.29	0.36	0.03	0.09	1.09
Jun-10	0.09	0.11	0.07	0.28	0.35	0.03	0.08	1.01
Jul-10	0.09	0.12	0.07	0.29	0.34	0.03	0.06	1.01
Aug-10	0.11	0.11	0.08	0.30	0.42	0.04	0.09	1.16
Sep-10	0.11	0.10	0.08	0.28	0.37	0.04	0.05	1.02
Oct-10	0.10	0.11	0.09	0.31	0.36	0.05	0.07	1.08
Nov-10	0.09	0.10	0.09	0.31	0.37	0.01	0.09	1.05
Dec-10	0.10	0.09	0.08	0.31	0.35	0.03	0.09	1.04
Jan-11	0.12	0.11	0.09	0.32	0.36	0.03	0.10	1.14
Feb-11	0.02	0.10	0.08	0.31	0.33	0.03	0.09	0.96
Mar-11	0.01	0.03	0.03	0.35	0.32	0.04	0.07	0.86
Apr-11	0.08	0.00	0.02	0.34	0.29	0.01	0.06	0.80
May-11	0.13	0.12	0.09	0.32	0.34	0.03	0.07	1.09
Jun-11	0.10	0.11	0.08	0.32	0.32	0.02	0.07	1.02
Jul-11	0.11	0.11	0.08	0.33	0.31	0.03	0.07	1.04
Aug-11	0.11	0.11	0.08	0.34	0.24	0.04	0.08	1.01
Sep-11	0.11	0.11	0.09	0.30	0.34	0.05	0.06	1.05
Oct-11	0.14	0.11	0.09	0.32	0.41	0.05	0.07	1.19
Nov-11	0.13	0.13	0.09	0.32	0.39	0.05	0.03	1.16
Dec-11	0.13	0.14	0.09	0.30	0.42	0.06	0.03	1.16

		VOC (TPY)										
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total				
2010	1.23	1.29	0.93	3.59	4.46	0.41	0.93	12.84				
2011	1.19	1.18	0.91	3.86	4.06	0.45	0.80	12.46				
2010-2011 average	1.21	1.23	0.92	3.73	4.26	0.43	0.86	12.65				

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Monthly Emissions

_	NOx (TPY)										
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total			
Jan-10	2.58	2.70	1.93	5.53	2.44	1.00	2.03	18.21			
Feb-10	2.14	2.60	1.80	5.02	1.99	1.04	1.85	16.44			
Mar-10	2.83	1.45	1.09	5.10	1.78	0.63	1.80	14.68			
Apr-10	2.64	2.42	1.69	5.21	1.51	0.73	1.71	15.90			
May-10	2.63	2.70	1.69	5.02	1.41	0.68	2.05	16.19			
Jun-10	2.12	2.41	1.51	4.89	1.41	0.68	1.85	14.87			
Jul-10	2.08	2.58	1.56	5.05	1.41	0.76	1.35	14.79			
Aug-10	2.68	2.45	1.82	5.17	1.98	0.86	2.03	16.97			
Sep-10	2.62	2.15	1.68	4.87	1.72	0.77	1.13	14.96			
Oct-10	2.28	2.50	1.88	5.30	1.65	1.19	1.50	16.29			
Nov-10	2.14	2.23	1.87	5.25	1.87	0.11	1.99	15.46			
Dec-10	2.32	1.91	1.83	5.34	1.57	0.58	1.95	15.51			
Jan-11	2.80	2.27	1.77	5.22	1.45	0.71	2.02	16.25			
Feb-11	0.47	2.02	1.65	4.96	1.08	0.68	1.85	12.71			
Mar-11	0.25	0.68	0.56	5.70	1.39	0.87	1.55	10.99			
Apr-11	1.74	0.09	0.41	5.47	1.33	0.26	1.25	10.55			
May-11	2.89	2.45	1.84	5.19	1.60	0.60	1.41	15.99			
Jun-11	2.28	2.17	1.71	5.15	1.52	0.51	1.42	14.76			
Jul-11	2.58	2.19	1.66	5.30	1.60	0.64	1.53	15.50			
Aug-11	2.60	2.31	1.72	5.50	1.23	0.78	1.70	15.83			
Sep-11	2.55	2.25	1.80	4.82	2.28	0.96	1.23	15.88			
Oct-11	3.14	2.21	1.81	5.22	2.19	0.96	1.52	17.04			
Nov-11	2.93	2.74	1.84	5.21	1.84	1.13	0.69	16.38			
Dec-11	2.93	2.88	1.89	4.79	1.90	1.17	0.57	16.12			

-				NOx	(TPY)						
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total			
2010	29.08	.08 28.11 20.35 61.75 20.72 9.02 21.23									
2011	27.15	24.27	18.66	62.52	19.41	9.26	16.74	178.01			
2010-2011 average	28.12	26.19	19.50	62.14	20.07	9.14	18.99	184.14			

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Monthly Emissions

•				SO <sub>2</sub> (TPY)										
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total						
Jan-10	0.06	0.01	0.01	0.03	0.05	0.01	0.03	0.20						
Feb-10	0.03	0.02	0.01	0.04	0.05	0.01	0.03	0.19						
Mar-10	0.01	0.02	0.01	0.57	0.59	0.08	0.03	1.31						
Apr-10	0.02	0.02	0.02	0.07	0.08	0.01	0.02	0.23						
May-10	0.02	0.04	0.03	0.10	0.12	0.01	0.03	0.35						
Jun-10	0.03	0.04	0.02	0.09	0.11	0.01	0.03	0.33						
Jul-10	0.02	0.03	0.02	0.06	0.07	0.01	0.03	0.24						
Aug-10	0.03	0.10	0.07	0.26	0.36	0.03	0.04	0.89						
Sep-10	0.03	0.08	0.06	0.23	0.29	0.03	0.02	0.75						
Oct-10	0.01	0.05	0.04	0.13	0.16	0.02	0.02	0.45						
Nov-10	0.01	0.03	0.02	0.08	0.09	0.00	0.07	0.30						
Dec-10	0.01	0.02	0.02	0.08	0.09	0.01	0.04	0.28						
Jan-11	0.00	0.04	0.03	0.12	0.14	0.01	0.03	0.38						
Feb-11	0.00	0.06	0.05	0.19	0.21	0.02	0.04	0.57						
Mar-11	0.00	0.03	0.02	0.28	0.25	0.04	0.04	0.66						
Apr-11	0.00	0.00	0.01	0.91	0.74	0.01	0.03	1.70						
May-11	0.02	0.03	0.02	0.07	0.08	0.01	0.02	0.25						
Jun-11	0.07	0.06	0.05	0.18	0.18	0.01	0.07	0.62						
Jul-11	0.06	0.04	0.03	0.13	0.12	0.01	0.06	0.45						
Aug-11	0.05	0.03	0.02	0.11	0.06	0.02	0.04	0.33						
Sep-11	0.03	0.03	0.03	0.09	0.11	0.01	0.03	0.33						
Oct-11	0.03	0.03	0.03	0.10	0.12	0.01	0.02	0.34						
Nov-11	0.07	0.02	0.02	0.06	0.07	0.01	0.01	0.26						
Dec-11	0.07	0.03	0.02	0.06	0.09	0.01	0.01	0.29						

				SO <sub>2</sub> (	TPY)										
	231-B101	231-B101 865-11H1 865-11H2 210-H101 210-H201 866-12H1 868-8H101 Total													
2010	0.28	0.45	0.33	1.75	2.06	0.23	0.40	5.50							
2011	0.41	0.42	0.33	2.30	2.16	0.18	0.39	6.19							
2010-2011 average	0.35	0.43	0.33	2.02	2.11	0.20	0.39	5.85							

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Monthly Emissions

-				Lead	(TPY)			
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total
Jan-10	1.0E-05	1.1E-05	8.0E-06	2.9E-05	3.9E-05	4.2E-06	8.0E-06	1.1E-04
Feb-10	8.3E-06	1.1E-05	7.5E-06	2.7E-05	3.4E-05	4.3E-06	7.3E-06	9.9E-05
Mar-10	1.1E-05	6.0E-06	4.6E-06	2.7E-05	3.5E-05	2.6E-06	7.1E-06	9.3E-05
Apr-10	1.0E-05	1.0E-05	7.1E-06	2.8E-05	3.2E-05	3.0E-06	6.8E-06	9.7E-05
May-10	1.0E-05	1.1E-05	7.1E-06	2.7E-05	3.3E-05	2.8E-06	8.1E-06	9.9E-05
Jun-10	8.2E-06	1.0E-05	6.3E-06	2.6E-05	3.1E-05	2.8E-06	7.3E-06	9.2E-05
Jul-10	8.0E-06	1.1E-05	6.5E-06	2.7E-05	3.1E-05	3.1E-06	5.4E-06	9.2E-05
Aug-10	1.0E-05	1.0E-05	7.6E-06	2.7E-05	3.8E-05	3.6E-06	8.0E-06	1.1E-04
Sep-10	1.0E-05	9.0E-06	7.0E-06	2.6E-05	3.3E-05	3.2E-06	4.5E-06	9.3E-05
Oct-10	8.8E-06	1.0E-05	7.8E-06	2.8E-05	3.2E-05	4.9E-06	5.9E-06	9.8E-05
Nov-10	8.2E-06	9.3E-06	7.8E-06	2.8E-05	3.4E-05	4.7E-07	7.9E-06	9.5E-05
Dec-10	8.9E-06	8.0E-06	7.6E-06	2.8E-05	3.2E-05	2.4E-06	7.7E-06	9.5E-05
Jan-11	1.1E-05	1.0E-05	7.9E-06	2.9E-05	3.3E-05	3.1E-06	8.8E-06	1.0E-04
Feb-11	1.9E-06	8.9E-06	7.3E-06	2.8E-05	3.0E-05	3.0E-06	8.1E-06	8.7E-05
Mar-11	9.9E-07	3.0E-06	2.5E-06	3.2E-05	2.9E-05	3.8E-06	6.7E-06	7.8E-05
Apr-11	6.9E-06	3.9E-07	1.8E-06	3.1E-05	2.6E-05	1.2E-06	5.4E-06	7.3E-05
May-11	1.2E-05	1.1E-05	8.2E-06	2.9E-05	3.1E-05	2.7E-06	6.2E-06	9.9E-05
Jun-11	9.1E-06	9.6E-06	7.6E-06	2.9E-05	2.9E-05	2.2E-06	6.2E-06	9.3E-05
Jul-11	1.0E-05	9.7E-06	7.3E-06	3.0E-05	2.8E-05	2.8E-06	6.7E-06	9.4E-05
Aug-11	1.0E-05	1.0E-05	7.6E-06	3.1E-05	2.2E-05	3.5E-06	7.4E-06	9.2E-05
Sep-11	1.0E-05	1.0E-05	8.0E-06	2.7E-05	3.1E-05	4.2E-06	5.3E-06	9.5E-05
Oct-11	1.3E-05	9.8E-06	8.0E-06	2.9E-05	3.7E-05	4.2E-06	6.6E-06	1.1E-04
Nov-11	1.2E-05	1.2E-05	8.2E-06	2.9E-05	3.6E-05	5.0E-06	3.0E-06	1.1E-04
Dec-11	1.2E-05	1.3E-05	8.3E-06	2.7E-05	3.8E-05	5.2E-06	2.5E-06	1.1E-04

-				Lead	(TPY)									
	231-B101 865-11H1 865-11H2 210-H101 210-H201 866-12H1 868-8H101 Total													
2010	1.1E-04	1.2E-04	8.4E-05	1.2E-03										
2011	1.1E-04	1.1E-04	8.3E-05	3.5E-04	3.7E-04	4.1E-05	7.3E-05	1.1E-03						
2010-2011 average	1.1E-04	1.1E-04	8.4E-05	3.4E-04	3.9E-04	3.9E-05	7.8E-05	1.2E-03						

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater Monthly Emissions

•				CO <sub>2</sub> e (TPY)									
	231-B101	865-11H1	865-11H2	210-H101	210-H201	866-12H1	868-8H101	Total					
Jan-10	2,397	2,706	1,934	7,038	9,485	1,006	1,931	26,498					
Feb-10	1,986	2,604	1,805	6,387	8,247	1,039	1,764	23,830					
Mar-10	2,628	1,453	1,095	6,487	8,433	628	1,716	22,440					
Apr-10	2,445	2,429	1,697	6,626	7,686	732	1,628	23,243					
May-10	2,442	2,710	1,697	6,394	7,873	678	1,956	23,750					
Jun-10	1,970	2,411	1,513	6,225	7,558	677	1,762	22,116					
Jul-10	1,933	2,585	1,562	6,424	7,518	758	1,291	22,070					
Aug-10	2,483	2,455	1,822	6,577	9,154	863	1,931	25,285					
Sep-10	2,431	2,160	1,689	6,204	8,010	774	1,075	22,343					
Oct-10	2,119	2,508	1,882	6,743	7,803	1,189	1,428	23,672					
Nov-10	1,982	2,239	1,872	6,684	8,117	114	1,898	22,907					
Dec-10	2,152	1,917	1,833	6,803	7,587	580	1,860	22,733					
Jan-11	2,683	2,421	1,889	7,058	7,915	758	2,114	24,839					
Feb-11	454	2,149	1,752	6,702	7,214	724	1,937	20,934					
Mar-11	239	722	595	7,705	6,999	921	1,622	18,802					
Apr-11	1,671	93	434	7,397	6,299	277	1,306	17,477					
May-11	2,771	2,610	1,964	7,016	7,355	642	1,480	23,838					
Jun-11	2,188	2,311	1,823	6,956	6,953	539	1,486	22,255					
Jul-11	2,481	2,334	1,768	7,157	6,691	680	1,602	22,713					
Aug-11	2,496	2,460	1,828	7,427	5,324	831	1,777	22,143					
Sep-11	2,446	2,398	1,913	6,512	7,357	1,018	1,284	22,928					
Oct-11	3,015	2,349	1,926	7,057	8,975	1,021	1,586	25,929					
Nov-11	2,808	2,913	1,964	7,041	8,621	1,201	726	25,274					
Dec-11	2,808	3,069	2,007	6,471	9,176	1,241	592	25,365					

				CO₂e	(TPY)										
	231-B101	231-B101 865-11H1 865-11H2 210-H101 210-H201 866-12H1 868-8H101 Total													
2010	26,968	26,968 28,176 20,400 78,591 97,470 9,039 20,242 2													
2011	26,062	25,830	19,861	84,501	88,878	9,853	17,512	272,496							
2010-2011 average	ge 26,515 27,003 20,131 81,546 93,174 9,446 18,877 276,6														

PES Refinery Heater Firing Rate Increase Plan Approval Target Heater SO<sub>2</sub> Emissions

Month	Unit 231-B101	Unit 865-11H1	Unit 865-11H2	Unit 210-H101	Unit 210-H201	Unit 866-12H1	Unit 868-8H101
Month	SO <sub>2</sub> , pounds						
Jan-10	115.62	28.68	19.46	69.14	90.92	10.19	69.19
Feb-10	62.47	31.02	22.16	78.31	104.99	12.54	59.53
Mar-10	21.10	31.78	25.45	1145.24	1177.73	165.60	59.07
Apr-10	34.22	47.17	33.19	130.91	152.81	13.41	49.36
May-10	39.74	86.65	53.97	193.65	237.08	23.04	56.72
Jun-10	51.43	70.43	44.39	183.89	221.00	19.97	61.95
Jul-10	44.54	50.86	33.40	125.88	144.94	15.35	61.34
Aug-10	51.17	194.10	144.96	521.67	726.90	67.99	75.29
Sep-10	69.51	159.49	126.53	464.22	577.50	55.28	47.80
Oct-10	27.48	103.74	75.17	268.43	317.77	49.06	49.03
Nov-10	27.93	54.66	44.48	150.13	187.08	1.76	136.81
Dec-10	16.88	45.25	44.63	167.56	185.73	16.84	74.96
Jan-11	3.04	87.29	66.89	243.78	279.18	26.14	55.15
Feb-11	0.76	122.61	98.17	376.82	411.41	41.22	87.95
Mar-11	4.32	54.66	47.95	553.88	492.18	77.93	86.03
Apr-11	9.58	2.31	18.13	1810.99	1475.46	19.87	58.01
May-11	48.68	60.10	40.29	140.75	158.92	11.91	38.66
Jun-11	133.76	121.80	96.13	363.20	362.81	28.59	134.76
Jul-11	118.26	83.45	63.41	254.23	240.79	23.85	110.59
Aug-11	107.58	58.33	43.48	218.54	124.43	30.20	80.02
Sep-11	61.12	69.72	55.94	189.19	212.47	29.29	50.75
Oct-11	63.82	63.23	52.19	190.95	239.08	27.98	47.79
Nov-11	137.18	49.02	33.63	120.99	149.00	21.85	12.95
Dec-11	138.27	61.20	39.39	129.90	182.13	25.86	12.08
$2011  \mathrm{SO}_2  \mathrm{EF}$ $\left(\mathrm{lb/MMBtu}\right)^1$	0.00186	0.00194	0.00199	0.00327	0.00293	0.00223	0.00261

<sup>&</sup>lt;sup>1</sup> The target heaters only became subject to refinery fuel gas sulfur limits required by New Source Performance Standards Subpart J for Petroleum Refineries in 2011. Therefore, for this plan approval, the 2011 actual SO<sub>2</sub> emissions and 2011 actual fired rates for the each target heater were used to derive a heater-specific SO<sub>2</sub> emission factor.

PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Ancillary Upstream/Downstream Units

#### Crude Increase Basis

Crude Unit	24-month Actual Rate (MBPD)	Capable Rate - June 2010 (MBPD)	Capable increase from baseline (%)	Future Projected Actual Rate (MBPD)	Expected increase from this plan approval (%)
TOTAL	284.4	316.5	111%	346.0	122%

-	A	В	С	D	Е	F	G	Н	I	J	K	L	M	N	O
Source		2010 AC	CTUAL EMISS	SIONS (TPY)		2011 A	CTUAL	EMISSIO	NS (TPY	)		2010-11 Baseline Actual Emissions (TPY)			
	VOC	SOx	NOx	CO	PM	VOC	VOC SOx NOx CO			PM	VOC	SOx	NOx	CO	PM
TANKS*	176.09	-	-	-	-	159.95	-	-	-	-	168.02	-	-	-	-
SRTF TANKS*	66.79	-	-	-	-	68.38	-	-	-	-	67.58	-	-	-	-
WWTP	61.53	-	-	-	-	51.64	-	-	-	-	56.58	-	-	-	-
SRTF WWTP	0.93	-	-	-	-	2.29	-	-	-	-	1.61	-	-	-	-
GP BARGE LOADING (MVRU)	8.34	-	35.28	2.05	0.31	8.28	-	36.89	2.15	0.32	8.31	-	36.08	2.10	0.31
PB WHARF	31.51	-	-	-	-	40.17	-	-	-	-	35.84	-	-	-	-
GP BUTANE/PP LOADING	1.03	-	-	-	-	1.04	-	-	-	-	1.04	-	-	-	-
Sulfur Recovery Unit	-	14.11	4.36	171.33	-	-	10.37	4.83	189.98	-	-	12.24	4.59	180.66	-
Total Increases	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Calculation Formula											= Average(A,F)	= Average(B,G)	= Average(C,H)	= Average(D,I)	= Average(E,J)

<sup>\*</sup> For Tanks working losses are approximately 4% of emissions and will increase by throughput change:

Expected increases for plan approval from tanks = 0.96 + .04\*1.22 = 1.009 Capable increases from baseline for tanks = 0.96 + .04\*1.11 = 1.005

Note: 868 and 1232 FCCUs are generally operated at optimal rates and feed purchased (or transferred from MH) in 2010-11 will be replaced by increased production at 137 and 210 and should therefore show no significant change in emissions in the future.

<sup>\*\*</sup> Only capable % increases that are greater than zero are subtracted from the expected % increases.

PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Ancillary Upstream/Downstream Units

	P	Q R S T U V W X						W	Х	Y	Z	AA	AB	AC	AD
Source							eases fi (%)	om ba	seline		Projected F	uture Actual Emiss	sions (TPY)		
	VOC	SOx	NOx	CO	PM	VOC	SOx	NOx	CO	PM	VOC	SOx	NOx	CO	PM
TANKS*	0.87%	-	-	-	-	0.45%	-	-	-	-	169.47	-	-	-	-
SRTF TANKS*	0.87%	-	-	-	-	0.45%	-	-	-	-	68.17	-	-	-	-
WWTP	22%	-	-	-	-	11%	-	-	-	-	68.84	-	-	-	-
SRTF WWTP	22%	-	-	-	-	11%	-	-	-	-	1.96	-	-	-	-
GP BARGE LOADING (MVRU)	22%	-	22%	22%	22%	11%	-	11%	11%	11%	10.11	-	43.90	2.55	0.38
PB WHARF	22%	-	-	-	-	11%	-	-	-	-	43.60	-	-	-	-
GP BUTANE/PP LOADING	22%	-	-	-	-	11%	-	-	-	-	1.26	-	-	-	-
Sulfur Recovery Unit	-	22%	22%	22%	-	-	11%	11%	11%	-	-	14.89	5.59	219.79	-
Total Increases	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
Calculation Formula							·	·			= K * (1+P)	= L * (1+Q)	= M * (1+R)	= N * (1+S)	= O * (1+T)

PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Ancillary Upstream/Downstream Units

	AE	AF	AG	AH	AI	AJ	AK	AL	AM	AN
Source		Capable of Ac	ccommodating Em	issions (TPY)**			Emission	ns Increases from Plan Ap	oproval (TPY)	
	VOC	SOx	NOx	CO	PM	VOC	SOx	NOx	CO	PM
TANKS*	168.78					0.70	-	-	-	-
SRTF TANKS*	67.89					0.28	-	=	=	-
WWTP	62.98					5.86	-	-	-	-
SRTF WWTP	1.79					0.17	-	-	-	-
GP BARGE LOADING (MVRU)	9.25		40.16	2.34	0.35	0.86	-	3.74	0.22	0.03
PB WHARF	39.89					3.71	-	-	-	-
GP BUTANE/PP LOADING	1.15					0.11	-	-	-	-
Sulfur Recovery Unit		13.62	5.11	201.08		-	1.27	0.48	18.71	-
Total Increases						11.68	1.27	4.21	18.93	0.03
Calculation Formula	= K * (1+U)	= L * (1+V)	= M * (1+W)	= N * (1+X)	= O * (1+Y)	= (Z - K) - (AE - K)	= (AA - L) - (AF - L)	= (AB - M) - (AG - M)	= (AC - N) - (AH - N)	= (AD - O) - (AI - O)

#### PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Ancillary Upstream/Downstream Unmodified Heaters/Boiler

## Crude Increase Basis

Crude Unit	24-month Actual Rate (MBPD)	Capable Rate - June 2010 (MBPD)	Capable increase from baseline (%)	Future Projected Actual Rate (MBPD)	Expected increase from this plan approval (%)
TOTAL	284.4	316.5	111%	346.0	122%

137			A	В	С	D	E	F	G	Н	I	J	K	L
SOK   NOK   CO   PM   VOC   Lead   SOK   NOK   CO   PM   VOC	T I:A	Haston			2010 ACTU	AL EMISSIONS	(TPY)			2011 AC	TUAL EMIS	SSIONS (TI	PY)	-
137   F-2   0.86   48.73   26.70   0.60   1.75   1.6E-04   1.33   37.33   24.06   2.18   1.58   1.37   F-3   0.41   6.91   12.20   0.28   0.80   7.3E-05   0.65   6.42   11.61   1.05   0.76   1.3H-1   1.60   87.40   52.40   1.18   3.43   3.1E-04   1.87   83.80   50.30   4.55   3.30   1.332   H-400**   2.25   67.10   40.10   0.91   2.62   2.4E-04   1.27   14.00   46.17   4.18   3.02   1.332   H-401**   2.73   83.10   49.80   1.13   3.26   3.0E-04   1.69   17.84   62.19   5.63   4.07   1.332   H-601   0.43   4.03   6.69   0.15   0.44   4.0E-05   0.20   4.78   7.83   0.71   0.51   1.332   H-602   0.66   7.62   12.80   0.29   0.84   7.6E-05   0.44   9.30   1.55   1.41   10.2   1.332   H-62   0.66   7.62   12.80   0.29   0.84   7.6E-05   0.44   9.30   1.55   1.41   10.2   1.332   H-1	Offit	Heater	SOx	NOx	CO	PM	VOC	Lead	SOx	NOx	CO	PM	VOC	Lead
137	137	F-1	3.88	209.56	120.36	2.72	7.88	7.1E-04	8.02	179.81	117.59	10.64	7.70	7.2E-04
210   13H-1   1.60   87.40   52.40   1.18   3.43   3.1E-04   1.87   83.80   50.30   4.55   3.30   1332   H-400**   2.25   67.10   40.10   0.91   2.62   2.4E-04   1.27   14.00   46.17   4.18   3.02   1332   H-401**   2.73   83.10   49.80   1.13   3.26   3.0E-04   1.69   17.84   62.19   5.63   4.07   1332   H-601   0.43   4.03   6.69   0.15   0.44   4.0E-05   0.20   4.78   7.83   0.71   0.51   1332   H-602   0.66   7.62   12.80   0.29   0.84   7.6E-05   0.44   9.30   15.53   1.41   1.02   1332   H-1   0.05   0.03   0.05   0.00   0.00   0.00   3.1E-07   0.00   0.22   0.36   0.03   0.02   1332   H-2   0.52   4.25   1.37   0.25   0.71   6.2E-05   0.25   4.98   1.61   1.19   0.86   1332   H-3   0.39   3.88   6.48   0.15   0.42   3.9E-05   0.25   5.43   9.3   0.82   0.59   1.37   0.25   0.71   6.2E-05   0.25   5.43   9.3   0.82   0.59   0.86   0.2H3   1.01   61.60   36.20   0.82   2.37   2.2E-04   1.02   64.20   3.400   3.08   2.23   860   2.2H3   1.01   61.60   36.20   0.82   2.37   2.2E-04   1.02   64.20   3.400   3.08   2.23   860   2.2H5   1.13   6.960   40.80   0.92   2.67   2.5E-04   1.05   65.70   3.49   3.16   2.28   860   2.2H5   1.13   6.960   40.80   0.92   2.67   2.5E-04   1.05   65.70   3.49   3.16   2.28   860   2.2H5   0.42   9.24   15.20   0.34   1.00   9.2E-05   0.38   8.31   1.2.40   1.12   0.81   864   PH1   0.45   9.17   14.80   0.34   0.97   9.2E-05   0.38   8.31   1.2.40   1.12   0.81   864   PH1   0.45   9.17   14.80   0.34   0.97   9.2E-05   0.38   8.31   1.2.40   1.12   0.81   864   PH1   0.44   8.91   14.40   0.33   0.95   8.9E-05   0.30   7.44   1.280   1.16   0.84   864   PH1   0.44   8.91   14.40   0.33   0.95   8.9E-05   0.30   7.44   1.280   1.16   0.84   864   PH1   0.44   8.91   14.40   0.33   0.95   8.9E-05   0.30   7.44   1.280   1.16   0.84   864   PH1   0.44   8.99   14.40   0.33   0.95   8.9E-05   0.30   7.44   1.280   1.16   0.84   8.64   PH1   0.44   8.99   14.40   0.03   0.95   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.99   0.9	137	F-2	0.86	48.73	26.70	0.60	1.75	1.6E-04	1.33	37.33	24.06	2.18	1.58	1.5E-04
1332	137	F-3	0.41	6.91	12.20	0.28	0.80	7.3E-05	0.65	6.42	11.61	1.05	0.76	7.2E-05
1332	210	13H-1	1.60	87.40	52.40	1.18	3.43	3.1E-04	1.87	83.80	50.30	4.55	3.30	3.4E-04
1332	1332	H-400**	2.25	67.10	40.10	0.91	2.62	2.4E-04	1.27	14.00	46.17	4.18	3.02	2.8E-04
1332	1332	H-401**	2.73	83.10	49.80	1.13	3.26	3.0E-04	1.69	17.84	62.19	5.63	4.07	3.7E-04
1332	1332	H-601	0.43	4.03	6.69	0.15	0.44	4.0E-05	0.20	4.78	7.83	0.71	0.51	4.8E-05
1332	1332	H-602	0.66	7.62	12.80	0.29	0.84	7.6E-05	0.44	9.30	15.53	1.41	1.02	9.3E-05
1332	1332	H-1	0.05	0.03	0.05	0.00	0.00	3.1E-07	0.00	0.22	0.36	0.03	0.02	2.2E-06
860 2H12 0.40 8.71 14.30 0.32 0.94 8.7E-05 0.38 8.47 12.60 1.14 0.82 860 2H3 1.01 61.60 36.20 0.82 2.37 2.2E-04 1.02 64.20 34.00 3.08 2.23 860 2H4 0.52 11.40 18.70 0.42 1.23 1.1E-04 0.50 11.70 17.40 1.58 1.14 860 2.H5 1.13 69.60 40.80 0.92 2.67 2.5E-04 1.05 65.70 34.90 3.16 2.28 860 2.H7 0.42 9.24 15.20 0.34 1.00 9.2E-05 0.38 8.31 12.40 1.12 0.81 860 2.H8 0.01 7.80 12.60 0.29 0.82 7.8E-05 0.19 6.92 11.10 1.01 0.73 864 PH1 0.45 9.17 14.80 0.34 0.97 9.2E-05 0.34 8.02 13.70 1.24 0.90 864 PH1 0.45 9.17 14.80 0.34 0.97 9.2E-05 0.34 8.02 13.70 1.24 0.90 864 PH11 0.44 8.91 14.40 0.33 0.95 8.9E-05 0.30 7.44 12.80 1.16 0.84 864 PH11 0.44 8.91 14.40 0.33 0.95 8.9E-05 0.30 7.44 12.80 1.16 0.84 864 PH11 0.44 6.98 9.98 0.62 1.81 1.7E-04 0.79 5.44 7.77 2.07 1.49 (870 H-01) 0.05 4.09 5.29 0.88 0.62 1.81 1.7E-04 0.79 5.44 7.77 0.03 0.88 0.06 12.32 B-104 0.01 0.05 4.09 5.29 0.88 0.38 0.14 7.E-05 0.11 4.98 55.66 5.04 39.85 0.62 1.23 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 870 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 870 H-02 0.23 4.22 0.08 0.38 0.34 0.14 7.E-05 0.36 3.63 0.03 0.33 0.12 Calculation Formula	1332	H-2	0.52	4.25	1.37	0.25	0.71	6.2E-05	0.25	4.98	1.61	1.19	0.86	7.8E-05
860 2H3 1.01 61.60 36.20 0.82 2.37 2.2E-04 1.02 64.20 34.00 3.08 2.23 860 2H4 0.52 11.40 18.70 0.42 1.23 1.1E-04 0.50 11.70 17.40 1.58 1.14 1.40 1.05 1.1E-04 1.05 65.70 34.90 3.16 2.28 860 2.H5 1.13 69.60 40.80 0.92 2.67 2.5E-04 1.05 65.70 34.90 3.16 2.28 860 2.H7 0.42 9.24 15.20 0.34 1.00 9.2E-05 0.38 8.31 12.40 1.12 0.81 860 2.H8 0.01 7.80 12.60 0.29 0.82 7.8E-05 0.39 8.31 12.40 1.12 0.81 864 PH1 0.45 9.17 14.80 0.34 0.97 9.2E-05 0.34 8.02 13.70 1.24 0.90 864 PH7 0.23 4.70 7.62 0.17 0.50 4.7E-05 0.18 4.49 7.71 0.70 0.51 864 PH11 0.44 8.91 14.40 0.33 0.95 8.9E-05 0.30 7.44 12.80 1.16 0.84 864 PH11 0.44 6.98 9.98 0.62 1.81 1.7E-04 0.79 5.44 7.77 2.07 1.49 (870 H-01 0.05 4.09 5.29 0.88 0.06 1.5E-05 0.11 4.07 0.03 0.88 0.06 1.25E-04 1.30 1.49 \$55.66 5.04 3.64 1232 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 870 H-02 0.23 4.29 0.88 0.38 0.14 7.1E-05 0.36 3.63 0.03 0.33 0.12 Calculation Formula	1332	H-3	0.39	3.88	6.48	0.15	0.42	3.9E-05	0.25	5.43	9.03	0.82	0.59	5.4E-05
860 2H4 0.52 11.40 18.70 0.42 1.23 1.1E-04 0.50 11.70 17.40 1.58 1.14 860 2H5 1.13 69.60 40.80 0.92 2.67 2.5E-04 1.05 65.70 34.90 3.16 2.28 860 2H7 0.42 9.24 15.20 0.34 1.00 9.2E-05 0.38 8.31 12.40 1.12 0.81 860 2H8 0.01 7.80 12.60 0.29 0.82 7.8E-05 0.19 6.92 11.10 1.01 0.73 864 PH1 0.45 9.17 14.80 0.34 0.97 9.2E-05 0.34 8.02 13.70 1.24 0.90 864 PH1 0.45 8.91 14.40 0.33 0.95 8.9E-05 0.30 7.44 12.80 1.16 0.84 8.91 14.40 0.33 0.95 8.9E-05 0.30 7.44 12.80 1.16 0.84 864 PH12 0.37 7.59 12.30 0.28 0.80 7.6E-05 0.28 6.61 11.40 1.03 0.74 859 1H1 0.44 6.98 9.98 0.62 1.81 1.7E-04 0.79 5.44 7.77 2.07 1.49 0.87 870 H-01 0.05 4.09 5.29 0.88 0.06 1.5E-05 0.11 4.07 0.03 0.88 0.06 1.23 B-104 0.01 0.29 0.45 0.01 0.09 0.27 2.5E-04 1.30 14.98 55.66 5.04 3.64 1232 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 880 -14 -14 -14 -14 -14 -14 -14 -14 -14 -14	860	2H2	0.40	8.71	14.30	0.32	0.94	8.7E-05	0.38	8.47	12.60	1.14	0.82	8.5E-05
860 2H5 1.13 69.60 40.80 0.92 2.67 2.5E-04 1.05 65.70 34.90 3.16 2.28 860 2H7 0.42 9.24 15.20 0.34 1.00 9.2E-05 0.38 8.31 12.40 1.12 0.81 860 2H8 0.01 7.80 12.60 0.29 0.82 7.8E-05 0.19 6.92 11.10 1.01 0.73 864 PH1 0.45 9.17 14.80 0.34 0.97 9.2E-05 0.34 8.02 13.70 1.24 0.90 864 PH1 0.44 8.91 14.40 0.33 0.95 8.9E-05 0.30 7.44 12.80 1.16 0.84 864 PH12 0.37 7.59 12.30 0.28 0.80 7.6E-05 0.28 6.61 11.40 1.03 0.74 859 1H1 0.44 6.98 9.98 0.62 1.81 1.7E-04 0.79 5.44 7.77 2.07 1.49 (870 H-01 0.05 4.09 5.29 0.88 0.06 1.5E-05 0.11 4.07 0.03 0.88 0.06 1.232 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 870 H-02 0.23 4.22 0.08 0.38 0.38 0.14 7.1E-05 0.36 3.63 0.03 0.33 0.12 Calculation Formula	860	2H3	1.01	61.60	36.20	0.82	2.37	2.2E-04	1.02	64.20	34.00	3.08	2.23	2.3E-04
860 2H7 0.42 9.24 15.20 0.34 1.00 9.2E-05 0.38 8.31 12.40 1.12 0.81 860 2H8 0.01 7.80 12.60 0.29 0.82 7.8E-05 0.19 6.92 11.10 1.01 0.73 864 PH1 0.45 9.17 14.80 0.34 0.97 9.2E-05 0.34 8.02 13.70 1.24 0.90 864 PH7 0.23 4.70 7.62 0.17 0.50 4.7E-05 0.18 4.49 7.71 0.70 0.51 864 PH11 0.44 8.91 14.40 0.33 0.95 8.9E-05 0.30 7.44 12.80 1.16 0.84 864 PH12 0.37 7.59 12.30 0.28 0.80 7.6E-05 0.28 6.61 11.40 1.03 0.74 859 1H1 0.44 6.98 9.98 0.62 1.81 1.7E-04 0.79 5.44 7.77 2.07 1.49 0 870 H-01 0.05 4.09 5.29 0.88 0.06 1.5E-05 0.11 4.07 0.03 0.88 0.06 433 H-1 2.43 24.97 42.40 0.96 2.77 2.5E-04 1.30 14.98 55.66 5.04 3.64 1232 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 Calculation Formula	860	2H4	0.52	11.40	18.70	0.42	1.23	1.1E-04	0.50	11.70	17.40	1.58	1.14	1.2E-04
860	860	2H5	1.13	69.60	40.80	0.92	2.67	2.5E-04	1.05	65.70	34.90	3.16	2.28	2.3E-04
864         PHI         0.45         9.17         14.80         0.34         0.97         9.2E-05         0.34         8.02         13.70         1.24         0.90           864         PH7         0.23         4.70         7.62         0.17         0.50         4.7E-05         0.18         4.49         7.71         0.70         0.51           864         PH11         0.44         8.91         14.40         0.33         0.95         8.9E-05         0.30         7.44         12.80         1.16         0.84           864         PH12         0.37         7.59         12.30         0.28         0.80         7.6E-05         0.28         6.61         11.40         1.03         0.74           859         1H1         0.44         6.98         9.98         0.62         1.81         1.7E-04         0.79         5.44         7.77         2.07         1.49         0           870         H-01         0.05         4.09         5.29         0.88         0.06         1.5E-05         0.11         4.07         0.03         0.88         0.06           433         H-1         2.43         24.97         42.40         0.96         2.77         2.5E-	860	2H7	0.42	9.24	15.20	0.34	1.00	9.2E-05	0.38	8.31	12.40	1.12	0.81	8.3E-05
864         PH7         0.23         4.70         7.62         0.17         0.50         4.7E-05         0.18         4.49         7.71         0.70         0.51           864         PH11         0.44         8.91         14.40         0.33         0.95         8.9E-05         0.30         7.44         12.80         1.16         0.84           864         PH12         0.37         7.59         12.30         0.28         0.80         7.6E-05         0.28         6.61         11.40         1.03         0.74           859         1H1         0.44         6.98         9.98         0.62         1.81         1.7E-04         0.79         5.44         7.77         2.07         1.49         0.77         1.49         0.79         1.44         7.77         2.07         1.49         0.79         1.44         7.77         2.07         1.49         0.79         1.49         0.79         1.49         0.79         1.49         0.79         1.49         0.79         1.49         0.79         1.49         0.79         1.49         0.79         1.49         0.79         0.79         1.49         0.79         0.79         1.49         0.79         0.79         0.79 <t< td=""><td>860</td><td>2H8</td><td>0.01</td><td>7.80</td><td>12.60</td><td>0.29</td><td>0.82</td><td>7.8E-05</td><td>0.19</td><td>6.92</td><td>11.10</td><td>1.01</td><td>0.73</td><td>6.8E-05</td></t<>	860	2H8	0.01	7.80	12.60	0.29	0.82	7.8E-05	0.19	6.92	11.10	1.01	0.73	6.8E-05
864         PH11         0.44         8.91         14.40         0.33         0.95         8.9E-05         0.30         7.44         12.80         1.16         0.84           864         PH12         0.37         7.59         12.30         0.28         0.80         7.6E-05         0.28         6.61         11.40         1.03         0.74           859         1H1         0.44         6.98         9.98         0.62         1.81         1.7E-04         0.79         5.44         7.77         2.07         1.49         0           870         H-01         0.05         4.09         5.29         0.88         0.06         1.5E-05         0.11         4.07         0.03         0.88         0.06           433         H-1         2.43         24.97         42.40         0.96         2.77         2.5E-04         1.30         14.98         55.66         5.04         3.64           1232         B-104         0.01         0.29         0.45         0.01         0.03         2.9E-06         0.09         0.99         0.99         1.69         0.15         0.11           870         H-02         0.23         4.22         0.08         0.38         0	864	PH1	0.45	9.17	14.80	0.34	0.97	9.2E-05	0.34	8.02	13.70	1.24	0.90	4.5E-05
864         PH12         0.37         7.59         12.30         0.28         0.80         7.6E-05         0.28         6.61         11.40         1.03         0.74           859         1H1         0.44         6.98         9.98         0.62         1.81         1.7E-04         0.79         5.44         7.77         2.07         1.49         0           870         H-01         0.05         4.09         5.29         0.88         0.06         1.5E-05         0.11         4.07         0.03         0.88         0.06           433         H-1         2.43         24.97         42.40         0.96         2.77         2.5E-04         1.30         14.98         55.66         5.04         3.64           1232         B-104         0.01         0.29         0.45         0.01         0.03         2.9E-06         0.09         0.99         1.69         0.15         0.11           870         H-02         0.23         4.22         0.08         0.38         0.14         7.1E-05         0.36         3.63         0.03         0.33         0.12           Calculation Formula           No. 3 Boilerhouse         12.91         199.60	864	PH7	0.23	4.70	7.62	0.17	0.50	4.7E-05	0.18	4.49	7.71	0.70	0.51	7.4E-05
859	864	PH11	0.44	8.91	14.40	0.33	0.95	8.9E-05	0.30	7.44	12.80	1.16	0.84	6.6E-05
870 H-01 0.05 4.09 5.29 0.88 0.06 1.5E-05 0.11 4.07 0.03 0.88 0.06 433 H-1 2.43 24.97 42.40 0.96 2.77 2.5E-04 1.30 14.98 55.66 5.04 3.64 1232 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 870 H-02 0.23 4.22 0.08 0.38 0.14 7.1E-05 0.36 3.63 0.03 0.33 0.12 Calculation Formula    Calculation Formula   Calculation	864	PH12	0.37	7.59	12.30	0.28	0.80	7.6E-05	0.28	6.61	11.40	1.03	0.74	1.1E-04
433         H-1         2.43         24.97         42.40         0.96         2.77         2.5E-04         1.30         14.98         55.66         5.04         3.64           1232         B-104         0.01         0.29         0.45         0.01         0.03         2.9E-06         0.09         0.99         1.69         0.15         0.11           870         H-02         0.23         4.22         0.08         0.38         0.14         7.1E-05         0.36         3.63         0.03         0.33         0.12           Calculation Formula           Heater Total         21.92         761.88         574.07         14.74         39.20         3.7E-03         23.24         584.87         579.46         56.04         39.85           No. 3 Boilerhouse         12.91         199.60         316.24         9.24         20.69         2.3E-03         6.69         156.54         330.38         29.89         21.63	859	1H1	0.44	6.98	9.98	0.62	1.81	1.7E-04	0.79	5.44	7.77	2.07	1.49	0.0E+00
1232 B-104 0.01 0.29 0.45 0.01 0.03 2.9E-06 0.09 0.99 1.69 0.15 0.11 870 H-02 0.23 4.22 0.08 0.38 0.14 7.1E-05 0.36 3.63 0.03 0.33 0.12 Calculation Formula Heater Total 21.92 761.88 574.07 14.74 39.20 3.7E-03 23.24 584.87 579.46 56.04 39.85 No. 3 Boilerhouse 12.91 199.60 316.24 9.24 20.69 2.3E-03 6.69 156.54 330.38 29.89 21.63 Calculation Formula	870	H-01	0.05	4.09	5.29	0.88	0.06	1.5E-05	0.11	4.07	0.03	0.88	0.06	2.2E-05
870 H-02 0.23 4.22 0.08 0.38 0.14 7.1E-05 0.36 3.63 0.03 0.33 0.12 Calculation Formula Heater Total 21.92 761.88 574.07 14.74 39.20 3.7E-03 23.24 584.87 579.46 56.04 39.85  No. 3 Boilerhouse 12.91 199.60 316.24 9.24 20.69 2.3E-03 6.69 156.54 330.38 29.89 21.63 Calculation Formula	433	H-1	2.43	24.97	42.40	0.96	2.77	2.5E-04	1.30	14.98	55.66	5.04	3.64	3.4E-04
Calculation Formula         Heater Total       21.92       761.88       574.07       14.74       39.20       3.7E-03       23.24       584.87       579.46       56.04       39.85         No. 3 Boilerhouse       12.91       199.60       316.24       9.24       20.69       2.3E-03       6.69       156.54       330.38       29.89       21.63         Calculation Formula	1232	B-104	0.01	0.29	0.45	0.01	0.03	2.9E-06	0.09	0.99	1.69	0.15	0.11	9.8E-06
Heater Total     21.92     761.88     574.07     14.74     39.20     3.7E-03     23.24     584.87     579.46     56.04     39.85       No. 3 Boilerhouse     12.91     199.60     316.24     9.24     20.69     2.3E-03     6.69     156.54     330.38     29.89     21.63       Calculation Formula	870	H-02	0.23	4.22	0.08	0.38	0.14	7.1E-05	0.36	3.63	0.03	0.33	0.12	6.7E-05
No. 3 Boilerhouse 12.91 199.60 316.24 9.24 20.69 2.3E-03 6.69 156.54 330.38 29.89 21.63 Calculation Formula		Calculation Formula												•
Calculation Formula		Heater Total	21.92	761.88	574.07	14.74	39.20	3.7E-03	23.24	584.87	579.46	56.04	39.85	3.7E-03
Calculation Formula								•						
		No. 3 Boilerhouse	12.91	199.60	316.24	9.24	20.69	2.3E-03	6.69	156.54	330.38	29.89	21.63	1.9E-03
		Calculation Formula	ì	•		1								
TI - /D 1 TI - 1 200 201 200 201 200 201 200 201 200 201 200 201 201														
Heater/Boiler Lotal 34.82   961.48   890.31   23.98   59.89   6.0E-03   29.93   741.41   909.84   85.93   61.48		Heater/Boiler Total	34.82	961.48	890.31	23.98	59.89	6.0E-03	29.93	741.41	909.84	85.93	61.48	5.7E-03

<sup>\*</sup> Only capable % increases that are greater than zero are subtracted from the expected % increases.

<sup>\*\*</sup> Future projected emissions are only based on 2011 actual emissions because of the SCR install in January 2011

PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Ancillary Upstream/Downstream Unmodified Heaters/Boiler

137			M	N	О	P	Q	R	S	T	U	V	W	X	Y	Z	AA A	AB A	C AD
SON   NON   CO   PM   VOC   Lead   SON   NON   CO   PM   PM   PM   PM   PM   PM   PM   P	T I:4	Haston		20	10-11 Baseline Act	ual Emissions (TP)	Y)		Exp	ected i	ncrease	es fror	n this p	olan	Capal	ole inci	eases f	rom ba	seline (%)
137   F.2   1.10   43.03   25.88   1.39   1.67   1.5E.04   22%   22%   22%   22%   22%   21%   11%	Unit	rieater	SOx	NOx	CO	PM	VOC	Lead	SOx	NOx	CO	PM	VOC	Lead	SOx	NOx	CO I	PM VO	OC Lead
F3	137	F-1	5.95	194.69	118.97	6.68	7.79	7.2E-04	22%	22%	22%	22%	22%	22%	11%	11%	11% 1	11% 11	11%
210	137	F-2	1.10	43.03	25.38	1.39	1.67	1.5E-04	22%	22%	22%	22%	22%	22%	11%	11%	11% 1	11% 11	11%
H-400°   1.27	137	F-3	0.53	6.67	11.91	0.66	0.78	7.2E-05	22%	22%	22%	22%			11%	11%	11% 1	11% 11	11%
H-401**   1.69	210	13H-1	1.73	85.60	51.35	2.87	3.37	3.3E-04	22%	22%					11%	11%	11% 1	11% 11	11%
1332   H-601   0.31	1332	H-400**	1.27	14.00	46.17		3.02	2.8E-04								11%	11% 1	11% 11	11%
1332	1332	H-401**	1.69	17.84	62.19	5.63	4.07	3.7E-04		22%			22%						11%
1332	1332	H-601	0.31	4.41	7.26	0.43	0.48	4.4E-05	22%	22%	22%	22%			11%	11%	11% 1	11% 11	11%
1332	1332	H-602	0.55	8.46	14.17	0.85	0.93	8.5E-05		22%									11%
1332	1332	H-1	0.03	0.12	0.20	0.02	0.01	1.2E-06	22%	22%									11%
860   2H2   0.39   8.59   13.45   0.73   0.88   8.6E-05   22%   22%   22%   22%   22%   22%   11%   11%   11%   11%   119   119   860   2H4   0.51   11.55   18.05   1.00   1.19   1.2E-04   22%   22%   22%   22%   22%   22%   22%   22%   21%   11%	1332	H-2	0.38	4.62	1.49	0.72	0.78	7.0E-05											11%
860 2H3 1.01 62.90 35.10 1.95 2.30 2.2E-04 22% 22% 22% 22% 22% 22% 11% 11% 11% 11%	1332	H-3	0.32		7.76			4.7E-05		22%									11%
860 2H4 0.51 11.55 18.05 1.00 1.19 1.2E-04 22% 22% 22% 22% 22% 21% 11% 11% 11% 11%	860	2H2	0.39	8.59	13.45	0.73	0.88	8.6E-05											11%
860 2H5 1.09 67.65 37.85 2.04 2.48 2.4E-04 22% 22% 22% 22% 22% 22% 11% 11% 11% 11%	860	2H3	1.01	62.90	35.10			2.2E-04		22%									11%
860 2H7 0.40 8.78 13.80 0.73 0.90 8.8E-05 22% 22% 22% 22% 22% 11% 11% 11% 11% 119 860 2H8 0.10 7.36 11.85 0.65 0.78 7.3E-05 22% 22% 22% 22% 22% 22% 22% 11% 11% 11%	860	2H4	0.51			1.00	1.19	1.2E-04											11%
860 2H8 0.10 7.36 11.85 0.65 0.78 7.3E-05 22% 22% 22% 22% 22% 22% 11% 11% 11% 11%	860	2H5	1.09	67.65	37.85	2.04	2.48	2.4E-04		22%				22%					11%
864 PH1 0.39 8.60 14.25 0.79 0.94 6.8E-05 22% 22% 22% 22% 22% 21% 11% 11% 11% 11%	860	2H7	0.40		13.80						22%	22%		22%					
864 PH7 0.21 4.60 7.67 0.43 0.50 6.1E-05 22% 22% 22% 22% 22% 22% 11% 11% 11% 11%	860	2H8	0.10	7.36	11.85	0.65	0.78	7.3E-05	22%	22%	22%	22%		22%					11%
864 PH11 0.37 8.18 13.60 0.74 0.89 7.8E-05 22% 22% 22% 22% 22% 11% 11% 11% 11% 11%		PH1									22%	22%		22%					
864 PH12 0.32 7.10 11.85 0.65 0.77 9.0E-05 22% 22% 22% 22% 22% 22% 11% 11% 11% 11%	864	PH7		4.60	7.67	0.43							22%	22%					
859		PH11		8.18	13.60			7.8E-05			22%	22%	22%	22%					
870 H-01 0.08 4.08 2.66 0.88 0.06 1.9E-05 22% 22% 22% 22% 22% 22% 22% 11% 11% 11%		PH12										22%	22%	22%					
433 H-1 1.86 19.98 49.03 3.00 3.21 2.9E-04 22% 22% 22% 22% 22% 22% 22% 11% 11% 11%					8.88			8.3E-05											
1232 B-104 0.05 0.64 1.07 0.08 0.07 6.4E-06 22% 22% 22% 22% 22% 22% 22% 11% 11% 11%		H-01			2.66			1.9E-05			22%	22%	22%	22%					
870 H-02 0.30 3.93 0.06 0.36 0.13 6.9E-05 22% 22% 22% 22% 22% 22% 22% 11% 11% 11%																			
Calculation Formula = Average(A,G) = Average(B,H) = Average(C,I) = Average(D,J) = Average(E,K) = Average(F,L) =																			
Heater Total 21.57 614.20 586.00 39.27 40.13 3.8E-03  No. 3 Boilerhouse 9.80 178.07 323.31 19.57 21.16 2.1E-03 22% 22% 22% 22% 22% 22% 11% 11% 11% 11%	870	H-02	0.30	3.93	0.06	0.36	0.13	6.9E-05	22%	22%	22%	22%	22%	22%	11%	11%	11% 1	11% 11	11%
No. 3 Boilerhouse 9.80 178.07 323.31 19.57 21.16 2.1E-03 22% 22% 22% 22% 22% 22% 11% 11% 11% 11%		Calculation Formula	= Average(A,G)	= Average(B,H)	= Average(C,I)	= Average(D,J)	= Average(E,K)	= Average(F,L)											
$Calculation Formula \qquad = Average(A,G) \qquad = Average(B,H) \qquad = Average(C,I) \qquad = Average(D,J) \qquad = Average(E,K) \qquad = Average(F,L)$		Heater Total	21.57	614.20	586.00	39.27	40.13	3.8E-03											
$Calculation Formula \qquad = Average(A,G) \qquad = Average(B,H) \qquad = Average(C,I) \qquad = Average(D,J) \qquad = Average(E,K) \qquad = Average(F,L)$																			
		No. 3 Boilerhouse	9.80	178.07	323.31	19.57	21.16	2.1E-03	22%	22%	22%	22%	22%	22%	11%	11%	11% 1	1% 11	% 11%
Heater/Boiler Total 31.37 792.26 909.31 58.84 61.29 5.9F-03		Calculation Formula	= Average(A,G)	= Average(B,H)	= Average(C,I)	= Average(D,J)	= Average(E,K)	= Average(F,L)					-						
Heater/Boiler Total 31.37 792.26 909.31 58.84 61.29 5.9F-03			. ,						•										
7700		Heater/Boiler Total	31.37	792.26	909.31	58.84	61.29	5.9E-03											

PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Ancillary Upstream/Downstream Unmodified Heaters/Boiler

		AE	AF	AG	AH	AI	AJ	AK	AL	AM	AN	AO	AP
Unit	Heater		Projec	ted Future Act	tual Emissions	(TPY)			Capa	able of Accommo	dating Emission	ns (TPY)*	
Offic	Heater	SOx	NOx	CO	PM	VOC	Lead	SOx	NOx	CO	PM	VOC	Lead
137	F-1	7.24	236.86	144.74	8.13	9.48	8.7E-04	6.62	216.69	132.42	7.44	8.67	8.0E-04
137	F-2	1.33	52.35	30.88	1.69	2.03	1.9E-04	1.22	47.89	28.25	1.55	1.85	1.7E-04
137	F-3	0.65	8.11	14.48	0.81	0.95	8.8E-05	0.59	7.42	13.25	0.74	0.87	8.1E-05
210	13H-1	2.11	104.14	62.47	3.49	4.09	4.0E-04	1.93	95.28	57.15	3.19	3.75	3.6E-04
1332	H-400**	1.54	17.03	56.17	5.08	3.67	3.4E-04	1.41	15.58	51.39	4.65	3.36	3.1E-04
1332	H-401**	2.06	21.70	75.66	6.85	4.95	4.5E-04	1.88	19.86	69.22	6.27	4.53	4.1E-04
1332	H-601	0.38	5.36	8.83	0.52	0.58	5.4E-05	0.35	4.90	8.08	0.48	0.53	4.9E-05
1332	H-602	0.67	10.29	17.23	1.03	1.13	1.0E-04	0.61	9.42	15.77	0.94	1.03	9.4E-05
1332	H-1	0.03	0.15	0.25	0.02	0.02	1.5E-06	0.03	0.14	0.23	0.02	0.01	1.4E-06
1332	H-2	0.47	5.61	1.81	0.87	0.95	8.5E-05	0.43	5.14	1.66	0.80	0.87	7.8E-05
1332	H-3	0.39	5.66	9.43	0.59	0.62	5.7E-05	0.36	5.18	8.63	0.54	0.57	5.2E-05
860	2H2	0.48	10.45	16.36	0.89	1.07	1.0E-04	0.44	9.56	14.97	0.81	0.98	9.6E-05
860	2H3	1.23	76.52	42.70	2.37	2.80	2.7E-04	1.13	70.01	39.07	2.17	2.56	2.5E-04
860	2H4	0.62	14.05	21.96	1.22	1.44	1.4E-04	0.57	12.86	20.09	1.11	1.32	1.3E-04
860	2H5	1.32	82.30	46.05	2.48	3.01	2.9E-04	1.21	75.30	42.13	2.27	2.75	2.7E-04
860	2H7	0.49	10.68	16.79	0.89	1.10	1.1E-04	0.44	9.77	15.36	0.81	1.01	9.8E-05
860	2H8	0.12	8.95	14.42	0.79	0.95	8.9E-05	0.11	8.19	13.19	0.72	0.86	8.1E-05
864	PH1	0.48	10.46	17.34	0.96	1.14	8.3E-05	0.44	9.57	15.86	0.88	1.04	7.6E-05
864	PH7	0.25	5.59	9.33	0.53	0.61	7.4E-05	0.23	5.11	8.53	0.48	0.56	6.8E-05
864	PH11	0.45	9.95	16.55	0.90	1.08	9.4E-05	0.41	9.10	15.14	0.82	0.99	8.6E-05
864	PH12	0.39	8.64	14.42	0.79	0.94	1.1E-04	0.36	7.90	13.19	0.73	0.86	1.0E-04
859	1H1	0.75	7.56	10.80	1.64	2.01	1.0E-04	0.69	6.91	9.88	1.50	1.84	9.2E-05
870	H-01	0.10	4.96	3.24	1.07	0.07	2.3E-05	0.09	4.54	2.96	0.98	0.06	2.1E-05
433	H-1	2.27	24.30	59.65	3.65	3.90	3.6E-04	2.07	22.23	54.57	3.34	3.57	3.3E-04
1232	B-104	0.06	0.77	1.30	0.10	0.09	7.7E-06	0.06	0.71	1.19	0.09	0.08	7.1E-06
870	H-02	0.36	4.78	0.07	0.43	0.16	8.4E-05	0.33	4.37	0.06	0.40	0.14	7.7E-05
	Calculation Formula	= M * (1+S)	= N * (1+T)	= O * (1+U)	= P * (1+V)	= Q * (1+W)	= R * (1+X)	= M * (1+Y)	= N * (1+Z)	= O * (1+AA)	= P * (1+AB)	= Q * (1+AC)	= R * (1+AD)
	Heater Total	26.24	747.23	712.93	47.78	48.82	4.6E-03	24.01	683.62	652.23	43.71	44.67	4.2E-03
	17 A D 11 1							1000	100.00	950.05			<b>9</b> 47 09
	No. 3 Boilerhouse	11.92	216.64	393.34	23.81	25.74	2.6E-03	10.90	198.20	359.85	21.78	23.55	2.4E-03
	Calculation Formula	= M * (1+S)	= N * (1+T)	= O * (1+U)	= P * (1+V)	= Q * (1+W)	= R * (1+X)	= M * (1+Y)	= N * (1+Z)	= O * (1+AA)	= P * (1+AB)	= Q * (1+AC)	= R * (1+AD)
	Heater/Boiler Total	38.16	963.87	1106.27	71.59	74.57	7.2E-03	34.91	881.81	1012.09	65.49	68.22	6.5E-03
	reater, boner rotai	50.10	700.07	1100.27	11.07	7 1.07	7.2E 00	01.71	001.01	1012.07	00.17	00.22	0.01 00

PES Refinery Heater Firing Rate Increase Plan Approval Emission Estimates for Ancillary Upstream/Downstream Unmodified Heaters/Boiler

		AQ	AR	AS	AT	AU	AV
Unit	Heater			Emissions Increases from	n Plan Approval (TPY)		
Cilit	Heater	SOx	NOx	CO	PM	VOC	Lead
137	F-1	0.62	20.16	12.32	0.69	0.81	7.4E-05
137	F-2	0.11	4.46	2.63	0.14	0.17	1.6E-05
137	F-3	0.06	0.69	1.23	0.07	0.08	7.5E-06
210	13H-1	0.18	8.87	5.32	0.30	0.35	3.4E-05
1332	H-400**	0.13	1.45	4.78	0.43	0.31	2.9E-05
1332	H-401**	0.18	1.85	6.44	0.58	0.42	3.9E-05
1332	H-601	0.03	0.46	0.75	0.04	0.05	4.6E-06
1332	H-602	0.06	0.88	1.47	0.09	0.10	8.8E-06
1332	H-1	0.00	0.01	0.02	0.00	0.00	1.3E-07
1332	H-2	0.04	0.48	0.15	0.07	0.08	7.2E-06
1332	H-3	0.03	0.48	0.80	0.05	0.05	4.8E-06
860	2H2	0.04	0.89	1.39	0.08	0.09	8.9E-06
860	2H3	0.10	6.51	3.64	0.20	0.24	2.3E-05
860	2H4	0.05	1.20	1.87	0.10	0.12	1.2E-05
860	2H5	0.11	7.01	3.92	0.21	0.26	2.5E-05
860	2H7	0.04	0.91	1.43	0.08	0.09	9.1E-06
860	2H8	0.01	0.76	1.23	0.07	0.08	7.5E-06
864	PH1	0.04	0.89	1.48	0.08	0.10	7.1E-06
864	PH7	0.02	0.48	0.79	0.05	0.05	6.3E-06
864	PH11	0.04	0.85	1.41	0.08	0.09	8.0E-06
864	PH12	0.03	0.74	1.23	0.07	0.08	9.4E-06
859	1H1	0.06	0.64	0.92	0.14	0.17	8.6E-06
870	H-01	0.01	0.42	0.28	0.09	0.01	1.9E-06
433	H-1	0.19	2.07	5.08	0.31	0.33	3.0E-05
1232	B-104	0.01	0.07	0.11	0.01	0.01	6.6E-07
870	H-02	0.03	0.41	0.01	0.04	0.01	7.1E-06
	Calculation Formula	= (AE - M) - (AK - M)	= (AF - N) - (AL - N)	= (AG - O) - (AM - O)	= (AH - P) - (AN - P)	= (AI - Q) - (AO - Q)	= (AJ - R) - (AP - R)
	Heater Total	2.23	63.62	60.69	4.07	4.16	3.9E-04
	No. 3 Boilerhouse	1.01	18.44	33.49	2.03	2.19	2.2E-04
	Calculation Formula	= (AE - M) - (AK - M)	= (AF - N) - (AL - N)	= (AG - O) - (AM - O)	= (AH - P) - (AN - P)	= (AI - Q) - (AO - Q)	= (AJ - R) - (AP - R)
	Heater/Boiler Total	3.25	82.06	94.18	6.09	6.35	6.1E-04

## PES Refinery Heater Firing Rate Increase Plan Approval Greenhouse Gas Emission Estimates for Ancillary Units

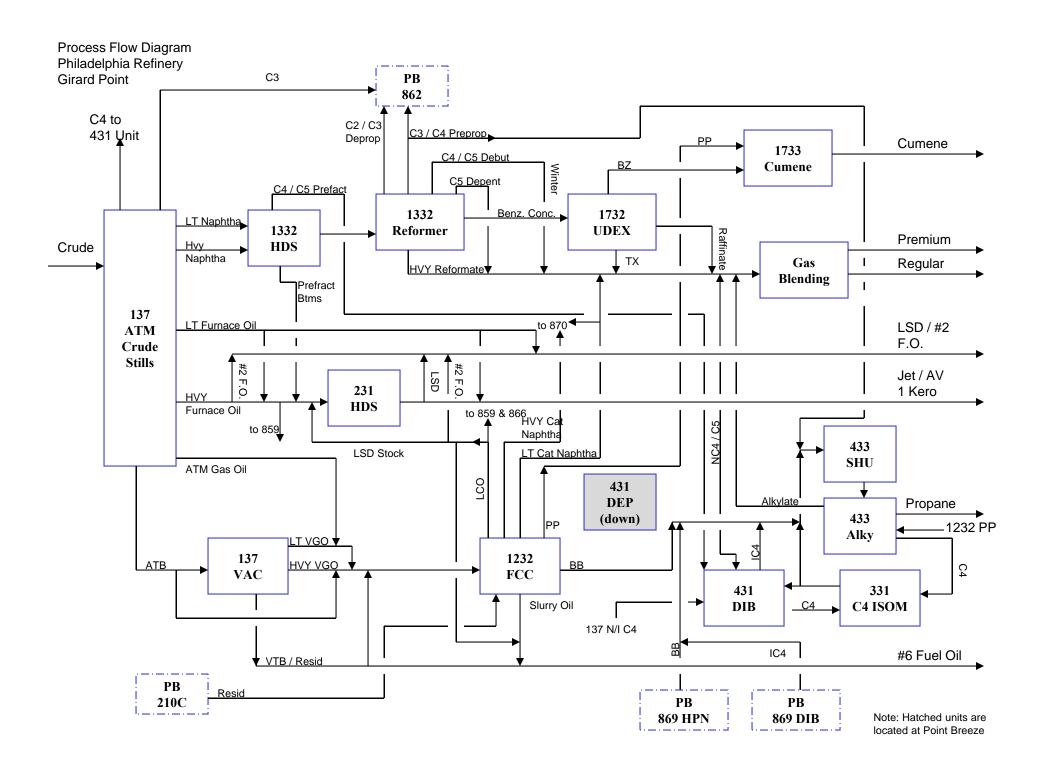
#### **Crude Increase Basis**

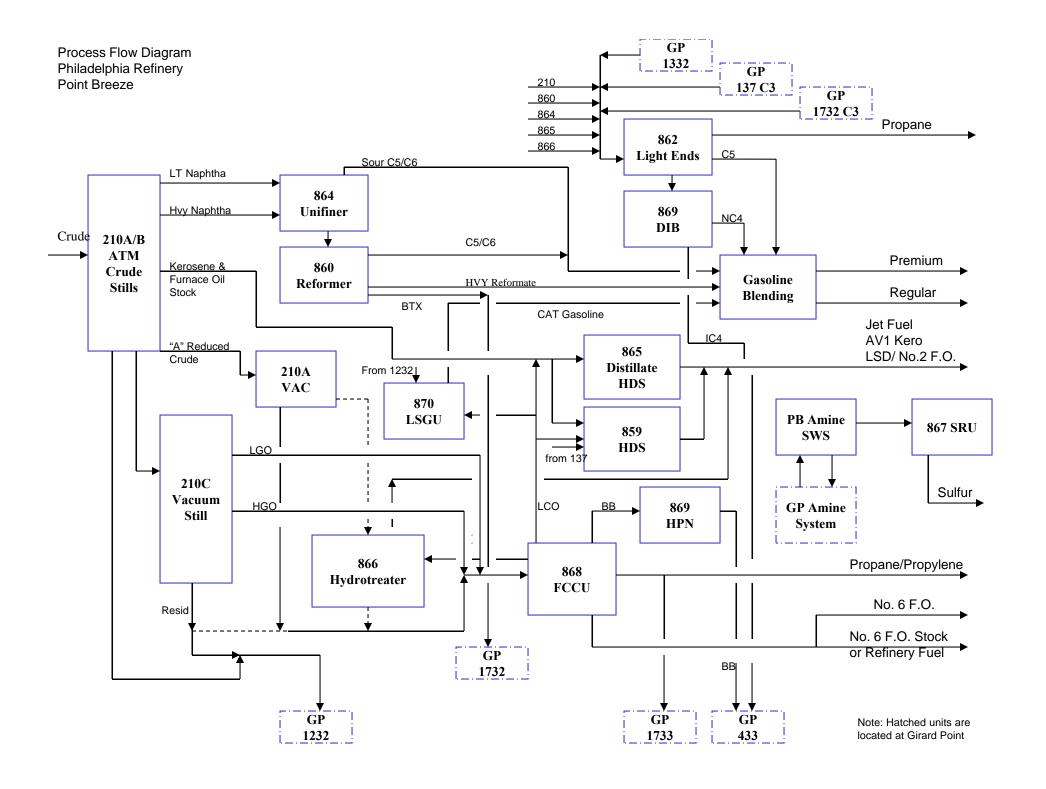
Crude Unit	24-month Actual Rate (MBPD)	Capable Rate - June 2010 (MBPD)	Capable increase from baseline (%)	Future Projected Actual Rate (MBPD)	Expected increase from this plan approval (%)
TOTAL	284.4	316.5	111%	346.0	122%

	A	В	С	D	E	F	G
Source	-	GHGe Report 2011 (mtons)	GHGe 24-month average (mtons)	GHGe Capable Increases from Baseline (%)	Expected increase from this plan approval (%)	Projected Future Actual Emissions (mton/year)*	Emissions Increases from Plan Approval (mton/year)
137 Unit	212,881	197,415	205,148	11%	22%	226,396	21,248
210 Unit Except H101 & H201	90,715	76,740	83,727	11%	22%	92,399	8,672
All Other (non-targeted) Heaters/Boiler	915,999	934,903	925,451	11%	22%	1,021,304	95,853
Unit 867 SRU	16,773	19,255	18,014	11%	22%	19,880	1,866
Girard Point MVRU	19,748	19,748	19,748	11%	22%	21,793	2,045
All LDAR	496	496	496	-	-	496	0
All Tanks	259	249	254	0.45%	0.87%	255	1.1
All Flares	45,068	17,138	31,103	-	-	31,103	0
Total	1,301,939	1,265,944	1,283,941			1,413,627	129,686
Calculation Formula	-		= Average(A,B)			= C * (1 + (E-D))	= F - C

<sup>\*</sup> Only capable % increases that are greater than zero are subtracted from the expected % increases.

Attachment E Process Flow Diagrams/Site Location Map









Penrose Avenue Sewer Pollock Street Sewer Passyunk Avenue Sewer Shunk Street Sewer

Wells Omitted From Contouring

N-30 3.77



# Attachment F CO Dispersion Modeling

## CO DISPERSION MODELING



Philadelphia Energy Solutions Refining and Marketing, LLC. (PES).

CO Dispersion Modeling for the Heater Firing Rate Increase

September 2013 Supplement

**Environmental Resources Management** 

75 Valley Stream Parkway Suite 200 Malvern, Pennsylvania 19355

## **TABLE OF CONTENTS**

1.0	INTE	RODUC	TION AND AIR QUALITY MODELING METHODOLOGY	1
2.0	PLA	N APPI	ROVAL EMISSIONS AND SOURCE CHARACTERIZATION	2
	2.1	BUIL	DING WAKE EFFECTS	4
3.0	MOI	DELING	S METHODOLOGY	5
	3.1	MOD	EL SELECTION AND APPLICATION	5
	3.2	AMB	IENT AIR QUALITY STANDARDS	5
	3.3	<b>GEO</b> (3.3.1 3.3.2		<b>5</b> 5
	3.4	RECE	PTOR GRID	6
	3.5	METI	EOROLOGY	6
4.0	МО	DEL RI	ESULTS PRESENTATION	9
LIST	T <b>OF T</b> A	BLES		
7	Table 2-1		Modeling Emissions Inventory (Source Parameters and Emissions)	
7	Table 3-1		Ambient Standards for Carbon Monoxide (CO)	
7	Table 4-1		Model Results	
LIST	OF AI	PPEND	ICES	
F	Appendiz	x A	Facility Location	
F	Appendi	x B	Source Locations	
F	Appendi	x C	Building Downwash	
F	Appendi	x D	Receptors	
F	Appendi	хE	PHL Annual Precipitation	

## 1.0 INTRODUCTION AND AIR QUALITY MODELING METHODOLOGY

On behalf of Philadelphia Energy Solutions (PES), Environmental Resources Management (ERM) has performed an air quality modeling analysis to assess compliance with the carbon monoxide (CO) Significant Impact Level (SIL) for the proposed plan approval at the Philadelphia Refinery.

ERM has performed the air quality modeling analysis in conformance with EPA's AERMOD implementation guidance. The key elements of the modeling analysis include:

- Use of the latest version of AERMOD (version 12345);
- Develop a comprehensive receptor grid designed to identify maximum plan approval concentration impacts;
- Use of surface meteorological data from Philadelphia International Airport (PHL) and upper air data from Sterling, VA for the period 2007-2011;
- Use of AERMET (version 12345) to process the meteorological data, with associated processors AERMINUTE (version 11325) and AERSURFACE (version 13016);
- Conduct air quality modeling to determine the magnitude and location of maximum ambient concentrations due to emissions of CO from the plan approval; and
- Compare maximum predicted impacts to the 1-hr and 8-hr CO SILs.

### 2.0 PLAN APPROVAL EMISSIONS AND SOURCE CHARACTERIZATION

A facility location map is presented in Appendix A of this report. Table 2-1 presents the emissions and modeled source parameters associated with all plan approval related sources. The CO emissions shown in Table 2-1 are the total plan approval emission increases from the target heaters and the upstream/downstream ancillary units. To be conservative, only the contemporaneous CO emissions increases are included in the analysis. For this air quality modeling analysis, the emissions decreases that occurred contemporaneously at Marcus Hook have not been included. Appendix B of this report presents the locations of all modeled sources.

Table 2-1 - Emission Rates and Modeled Source Parameters

		Exit				Base				
Height	Diameter	Velocity	Temp.	UTME	UTM N	Elevation	CO	CO	AERMOD ID	Source Name
m	m	m/s	° K	m	m	m	(tpy)	(g/s)		Unit 137 F-1 Heater
60.96	3.96	4.61	450.2	481824	4417696.91	2.30	12.32	0.354	1	Unit 231-B101 Heater
22.86	1.05	19.85	561.2	482193	4416912.34	2.38	15.88	0.457	2	
60.96	3.96	1.91	450.2	481807	4417719.35	2.46	2.63	0.076	3	Unit 137 F-2 Heater
23.01	1.37	4.63	505.2	481807	4417719.57	2.47	1.23	0.035	4	Unit 137 F-3 Heater
30.48	2.29	6.05	527.2	482178	4417034.35	2.47	4.78	0.138	5	Unit 1332 H-400 Heater
30.48	2.29	7.58	416.2	482235.3	4416966.19	2.69	6.92	0.199	6	Unit 1332 H-401 Heater
25.60	1.37	7.46	661.2	482219	4416978.75	2.47	0.75	0.022	7	Unit 1332 H-601 Heater
26.82	1.45	5.73	755.2	482229	4416983.31	2.40	1.47	0.042	8	Unit 1332 H-602 Heater
27.43	1.98	3.60	519.2	482204.87	4417002.24	2.41	0.02	0.001	9	Unit 1332 H-1 Heater
26.82	1.37	10.40	782.2	482208.83	4416994.20	2.38	0.15	0.004	10	Unit 1332 H-2 Heater
27.43	1.98	2.46	637.2	482214.67	4416986.24	2.44	0.80	0.023	11	Unit 1332 H-3 Heater
41.45	2.90	5.65	505.2	482104.31	4417244.63	2.5	5.18	0.149	12	Unit 433 H-1 Heater
35.05	2.44	5.85	755.2	482215.86	4417502.42	2.6	0.11	0.003	13	Unit 1232 B-104 Heater
60.96	5.79	12.07	489.2	481877.7	4416989.67	2.36	115.89	3.334	14	No. 3 Boilerhouse
16.76	3.05	4.52	1110.9	482653.65	4416170.07	1.66	0.22	0.006	15	GP BARGE LOADING (MVRU)
76.64	6.46	20.00	1273	481621.96	4416503.93	2.61	0.51	0.015	16	Butane Truck Unloading at SRTF
42.68	1.83	5.82	589.2	483138.63	4418599.73	7.31	19.68	0.566	18	Unit 865-11H1 Heater
55.17	1.88	3.05	555.4	483153.74	4418600.53	7.28	6.31	0.182	19	Unit 865-11H2 Heater
41.61	2.25	9.04	611.2	482862.71	4418515.03	6.63	9.99	0.287	20	Unit 210-H101 Heater
60.82	2.90	8.40	519.2	482881.52	4418507.91	6.74	23.24	0.669	21	Unit 210-H201 Heater
38.10	1.52	3.67	460.9	483180.68	4418601.49	7.35	12.02	0.346	22	Unit 866-12H1 Heater
35.95	1.31	6.64	533.2	483241.27	4418379.69	6.41	3.44	0.099	23	Unit 868-8H101 Heater
66.40	3.23	6.13	627.2	482935.72	4418489.91	7.06	5.32	0.153	24	Unit 210 13H-1 Heater
35.64	1.91	16.16	623.2	482900.35	4418267.46	5.1	1.39	0.040	25	Unit 860 2H2 Heater
33.53	2.05	22.57	623.2	482895.26	4418244.61	5.22	3.64	0.105	26	Unit 860 2H3 Heater
35.64	1.91	16.16	623.2	482903.55	4418244.14	5.12	1.87	0.054	27	Unit 860 2H4 Heater
33.53	2.05	22.57	623.2	482921.44	4418256.98	5.11	3.92	0.113	28	Unit 860 2H5 Heater
33.53	1.37	8.50	633.2	482918.85	4418286.84	5.05	1.43	0.041	29	Unit 860 2H7 Heater
33.53	1.37	7.66	626.2	482922.88	4418292.60	5.17	1.23	0.035	30	Unit 860 2H8 Heater
39.09	1.49	10.29	680.4	483162.38	4418496.84	7.26	1.48	0.042	31	Unit 864 PH1 Heater
33.53	1.37	6.56	610.2	483171.37	4418500.49	7.27	0.79	0.023	32	Unit 864 PH7 Heater
33.53	1.49	9.21	686.2	483171.37	4418499.69	7.24	1.41	0.023	33	Unit 864 PH11 Heater
36.58	1.63	9.68	655.2	483193.84	4418501.33	7.24	1.23	0.041	34	Unit 864 PH12 Heater
			703.7			5.02			35	Unit 859 1H1 Heater
44.81	1.93	6.80 7.58		482731.53	4418221.67	5.99	88.59	0.008	36	Unit 870 H-01 Heater
	1.80	7.58	701.2	483157.79	4418158.45		0.28	0.008		Unit 870 H-02 Heater
69.80	1.14	10.32	873.2	483165.8	4418146.56	5.99	18 71	0.000	37 38	Sulfur Recovery Unit
09.80	1.01 Release	29.22	802.2	482696.29	4418207.43	5.07 Base	18.71	0.538	38	Januar Recovery Offic
	Height	Sigma Y	Sigma Z	UTME	UTM N	Elevation	CO	СО	AERMOD ID	Source Name
	m	m	m	m	m	m	(tpy)	(g/s)		
	3.048	11.39	2.84	483059.95	4417975.87	4.39	0.45	0.013	39	Tank P-590 (PB 843) Reactivation

## 2.1 BUILDING WAKE EFFECTS

The EPA's Building Profile Input Program (BPIP), Version 04274, were used to calculate downwash effects for the modeled emission sources. Buildings were identified that could potentially affect the modeled sources. A figure showing the locations of sources and buildings is presented in Appendix C.

#### 3.0 MODELING METHODOLOGY

#### 3.1 MODEL SELECTION AND APPLICATION

The latest version of EPA's AERMOD model (version 12345) was used for predicting ambient impacts for carbon monoxide (CO). Regulatory default options were used in the analysis. The highest predicted impacts (H1H) are reported for the analyses presented in this report.

## 3.2 AMBIENT AIR QUALITY STANDARDS

Ambient air quality standards that were addressed are different for criteria pollutants (for which NAAQS have been established) and non-criteria pollutants for which ESLs have been established. Table 3-1 presents a summary of the air quality standards that were addressed for PM<sub>10</sub>, PM<sub>2.5</sub>, and CO (PSD pollutants), and for SO<sub>2</sub> (subject to a State NAAQS analysis). The SILs are presented, along with the significant monitoring concentrations (SMCs), PSD increments, and NAAQS. If plan approval impacts are shown to be less than the SILs and SMCs, then no further analysis is required. If the SILs are exceeded, additional analysis would be necessary including the development of a background source inventory and background measured concentrations. Section 4 of this report contains the results of the air quality modeling analyses for all pollutants. The results presented in Section 4 show that the proposed plan approval is less than the applicable SILs for CO.

Table 3-1 Ambient Standards for Carbon Monoxide (CO)

Parameter	Averaging Period	SIL	SMC	Increment	NAAQS
CO	1 Hour	2,000	-	-	40,000
CO	8 Hour	500	575	<del>-</del>	10,000

NOTE: All concentrations are shown in micrograms/cubic meter

### 3.3 GEOGRAPHIC SETTING AND AREA MAPS

#### 3.3.1 Land Use Characteristics

A facility location map is presented in Appendix A. The map was created using aerial imagery. In order to determine the appropriateness of

AERMOD's urban source option, the land use classification within a 3-km radius of the facility was determined using USGS 1992 LULC data. Land use within three kilometers of the facility was determined to be approximately 72% urban land use classification. Therefore, the urban option available in AERMOD will be used. The population of Philadelphia County, estimated for 2011 at 1,536,471 individuals by the US Census, will be used in AERMOD as input in the nighttime urban boundary layer algorithm.

### 3.3.2 Terrain

Terrain elevations and hill scales were determined for use in this analysis. The latest version of EPA's AERMAP program (version 11103) was used to determine the ground elevation and hill scale for each receptor, based on data obtained from the USGS National Elevation Database (NED).

### 3.4 RECEPTOR GRID

For this modeling analysis, a total of four separate receptor grids were combined to create an overall grid pattern:

- 1. Receptors at 25-m spacing located along the property fence-line;
- 2. Receptors spaced at 75-m out to 500 m from the fence-line;
- 3. Receptors at 100-m spacing located from 100 m from the approximate center of the facility to a distance of 2 km;
- 4. Receptors at 500-m spacing located from 2 km from the approximate center of the facility to a distance of 5 km; and
- 5. Receptors at 1-km spacing located from 5 km from the approximate center of the facility to a distance of 15 km.

Appendix D presents a figure of the inner portion of the receptor grid. As noted previously, AERMAP was used to define ground elevations and hill scales for each receptor.

#### 3.5 METEOROLOGY

The met data approved for use in this dispersion modeling analyses is based on surface observations from Philadelphia International Airport (PHL), and upper air measurements from Sterling, VA. The PHL AutomaTIC Surface observation Station (ASOS) is located approximately 4 km to the southwest of the central area of the PES Refinery.

Meteorological data from 2007 through 2011 were used, which represents the most recent available and complete five year continuous data period.

The surface and upper air meteorological data were processed using AERMET. The micrometeorological variables necessary for AERMET were generated by the AERSURFACE land use processing program. AERSURFACE was executed using the location of the PHL ASOS station available from the National Climatic Data Center (NCDC). The output from AERSURFACE was then merged with the meteorological data from PHL and Sterling, VA to create the data ready for input into AERMOD. The following assumptions and settings were used in the execution of AERMET and AERSURFACE:

- 2007-2011 surface data, ISHD data format
- Upper air data from Sterling, VA, FSL format
- Most recent version of AERMET, version 12345
- Location of PHL (from NCDC): 39.885 N, 75.236 W
- Elevation of PHL (from ISHD data file): **3.05 m**
- Anemometer Height (standard ASOS station height): 7.92 m
- Location of Sterling Upper Air Station (from FSL): 3 38.98 N, 77.47 W
- 1-minute ASOS winds from PHL processed with AERMINUTE
  - o Ice-free wind sensor installation date for PHL: 7/30/2009
- Surface data derived from AERSURFACE
  - o 1-km radius for surface roughness
  - 10x10km area for Bowen ratio and albedo
  - 12 sector surface roughness
  - o AERSURFACE Options:
    - Generated by AERSURFACE, dated 13016
    - Center Latitude (decimal degrees): 39.884913
    - Center Longitude (decimal degrees): -75.235735
    - Datum: NAD83
    - Study radius (km) for surface roughness: 1.0
    - Airport? **Yes**
    - Continuous snow cover? **No**
    - Surface moisture? Varies, see below
    - Arid region? **No**
    - Month/Season assignments? Default

- Late autumn after frost and harvest, or winter with no snow: 12
   12
- Winter with continuous snow on the ground: 0
- Transitional spring (partial green coverage, short annuals): 3 4 5
- Midsummer with lush vegetation: 6 7 8
- Autumn with unharvested cropland: 9 10 11
- Surface moisture was determined year by year following the methodology in the AERMOD implementation guide, using rainfall from PHL for the period of record for 1982-2011. The implementation guidance states that years with rainfall above the 70th percentile should use the WET option in AERSURFACE, years with less than the 30th percentile should use the DRY option, and the middle 30th percentile to 70th percentile should use the AVERAGE option. Rainfall data were obtained for PHL from NCDC for the 30 year period. Appendix E of this report contains a summary of these data, as well as the calculated percentile of each year's rainfall with respect to the 30 year period.
- No substitution for missing data.

### 4.0 MODEL RESULTS PRESENTATION

The result of the CO SIL modeling analysis is shown in Table 4-1. The highest 1-hr and 8-hr modeled concentrations over the five year model period are well below the SILs. As a result, the plan approval increase in carbon monoxide (CO) will not cause or contribute to any exceedance of the CO NAAQS, and no further air quality modeling analyses are required.

Table 4-1 SIL Analysis Results - Carbon Monoxide (CO)

#### **Maximum Modeled Concentrations**

	Averaging	Maximum	Significant	Impact					
Pollutant	Period	Concentration	Impact Level	Significant?	2007	2008	2009	2010	2011
CO	8-hr	12.81	500	No	11.97	12.14	12.81	11.25	11.55
	1-hr	16.22	2000	No	15.57	15.31	16.22	15.78	15.87

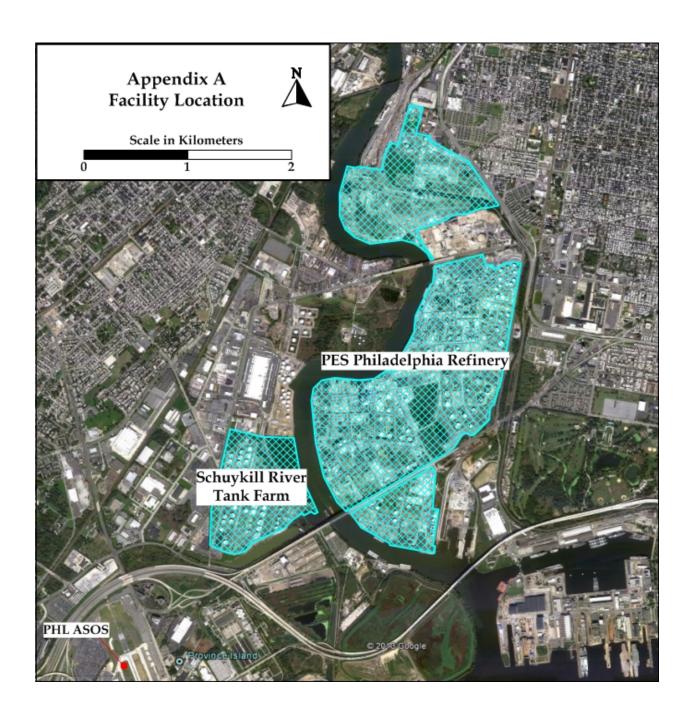
#### **Location of Maximum Modeled Concentrations**

	Averaging	Maximum				Elevation	Flagpole
Pollutant	Period	Concentration	Year	UTME (m)	UTMN (m)	(m)	(m)
CO	8-hr	12.81	2009	482504	4417967	5.9	0
	1-hr	16.22	2009	482540	4418033	6.4	0

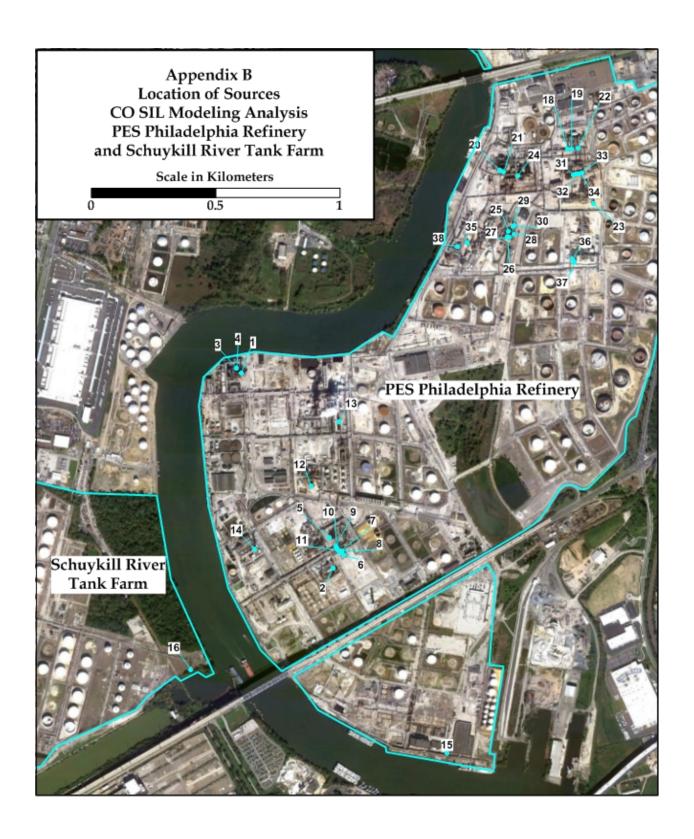
#### Notes:

1. All concentrations are in  $\mu g/m^3$ 

# Appendix A Facility Location

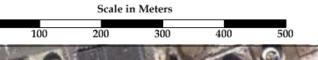


# Appendix B Source Location

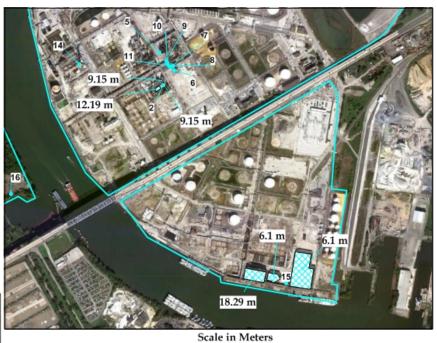


# Appendix C Building Downwash Structures

Appendix C Location of Sources and Downwash Structures CO SIL Modeling Analysis PES Philadelphia Refinery

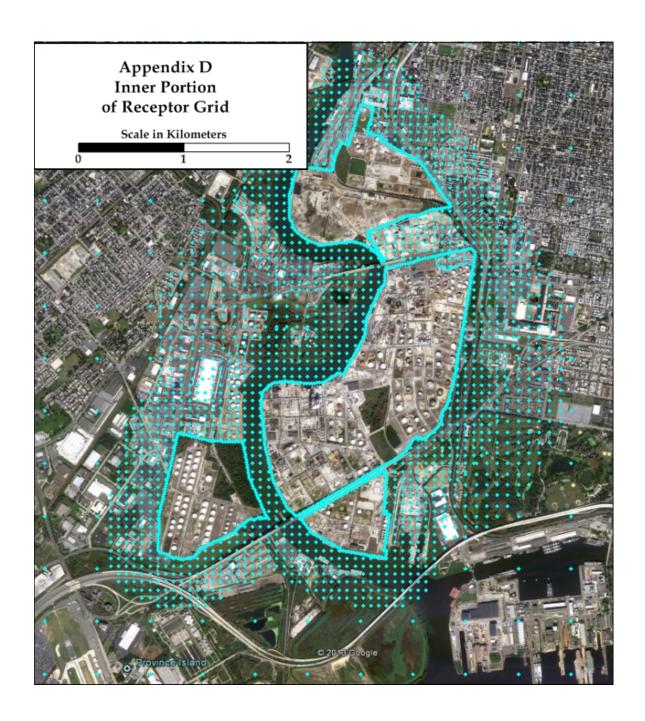






0 100 200 300 400 500 600 700 800 900 1000

# Appendix D Receptor Grid



Appendix E 30 Year Annual Rainfall – Philadelphia International Airport (PHL)

Appendix E						
		Pl	HL - Annual Rai	nfall		
	Rainfall	Percentile of 30 Year	30th Percentile	70th percentile		
Year	(in.)	Record	(in.)	(in.)		
1982	40.43	0.448	37.75	45.84		Dry
1983	54.66	0.931				Average
1984	43.66	0.586				Wet
1985	35.2	0.206				
1986	40.42	0.413				
1987	33.4	0.172				
1988	38.41	0.31				
1989	48.66	0.827				
1990	35.79	0.241				
1991	36.22	0.275				
1992	30.41	0				
1993	42.18	0.517				
1994	44.92	0.689				
1995	31.53	0.068				
1996	56.45	0.965				
1997	32.52	0.137				
1998	31.65	0.103				
1999	48.49	0.793				
2000	44.57	0.655				
2001	31.01	0.034				
2002	39.34	0.344				
2003	47.98	0.724				
2004	49.19	0.862				
2005	42.22	0.551				
2006	48.2	0.758				
2007	42.13	0.482				
2008	40.33	0.379				
2009	52.5	0.896				
2010	44.46	0.62				
2011	64.32	1				

Attachment G RBLC and BAAQMD BACT Search Results

#### **Summary**

#### NOx

RBLCID	FACILITY NAME	CORPORATE OR COMPANY NAME	FACILITY STATE	DATE DETERMINATION LAST UPDATED	FACILITY DESCRIPTION	PROCESS NAME	PROCCESS TYPE	PRIMARY FUEL
PA-0252 WA-0324	SUNOCO, INC. (R&M) FERNDALE REFINERY	SUNOCO, INC. (R&M) CONOCOPHILLIPS REFINING COMPANY	PA WA	-,,	PETROLEUM REFINERY PETROLEUM REFINERY	433 H-1 HEATER CGD FEED HEATER (MODEL ID SRC19)	11.3 11.31	REFINERY FUEL GAS NATURAL GAS
LA-0211	GARYVILLE REFINERY	MARATHON PETROLEUM CO LLC	LA	7/16/2008 F	PETROLEUM REFINERY	A&B CRUDE HEATERS (1-08 & 2-08); COKER CHARGE HEATER (15-08)	11.39	REFINERY FUEL GAS
LA-0211	GARYVILLE REFINERY	MARATHON PETROLEUM CO LLC	LA	7/16/2008 F	PETROLEUM REFINERY	PLATFORMER HEATER CELLS NO. 1-3 (7A-08, 7B-08, 7C-08); HCU FRACTIONATOR HEATER (13-08)	11.39	REFINERY FUEL GAS
LA-0213	ST. CHARLES REFINERY	VALERO REFINING - NEW ORLEANS, LLC	LA		PETROLEUM REFINERY	HEATER F-72-703 (7-81)	11.39	REFINERY FUEL GAS
NM-0050	ARTESIA REFINERY	NAVAJO REFINING COMPANY LLC	NM	-,-,	PETROLEUM REFINERY	ROSE 2 HOT OIL HEATER	12.3	REFINERY FUEL GAS
OK-0126 DE-0020	SUNOCO INC TULSA REFINERY VALERO DELAWARE CITY REFINERY	SUNOCO INC VALERO ENERGY CORP	OK DE		PETROLEUM REFINERY PETROLEUM REFINERY	PROCESS HEATER CRUDE UNIT VACUUM HEATER 21-H-2	12.31 12.39	REFINERY FUEL GAS REFINERY FUEL GAS
*WY-0071	SINCLAIR REFINERY	SINCLAIR WYOMING REFINING COMPANY	WY		PETROLEUM REFINERY	BSI Heater	13.3	Refinery Fuel Gas
WA-0301	BP CHERRY POINT REFINERY	BRITISH PETROLEUM	WA		PETROLEUM REFINERY	PROCESS HEATER, IHT	13.31	NATURAL GAS
PA-0256	SUNOCO, INC. (R&M)	SUNOCO, INC. (R&M)	PA	4/24/2008 F	PETROLEUM REFINERY	1H-5 HEATER	13.39	REFINERY FUEL GAS
PM								
RBLCID	FACILITY NAME	CORPORATE OR COMPANY NAME	FACILITY STATE	DATE DETERMINATION LAST UPDATED	FACILITY DESCRIPTION	PROCESS NAME	PROCCESS TYPE	PRIMARY FUEL
MT-0030	BILLINGS REFINERY	CONOCOPHILLIPS COMPANY	MT	3/9/2009 F	PETROLEUM REFINERY	NO. 1 H2 HEATER	11.3	REFINERY FUEL GAS/ PSA GAS
NM-0050	ARTESIA REFINERY	NAVAJO REFINING COMPANY LLC	NM	8/1/2008 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER	11.3	NATURAL GAS AND REFORMER OFF-GAS
LA-0211	GARYVILLE REFINERY	MARATHON PETROLEUM CO LLC	LA	7/16/2008 F	PETROLEUM REFINERY	PLATFORMER HEATER CELLS NO. 1-3 (7A-08, 7B-08, 7C-08); HCU FRACTIONATOR HEATER (13-08)	11.39	REFINERY FUEL GAS
LA-0213	ST. CHARLES REFINERY	VALERO REFINING - NEW ORLEANS, LLC	LA	3/5/2010 F	PETROLEUM REFINERY	CPF HEATER H-39-03; H-39-02 (94-28; 94-30)	13.39	REFINERY FUEL GAS
LA-0211	GARYVILLE REFINERY	MARATHON PETROLEUM CO LLC	LA	7/16/2008 F	PETROLEUM REFINERY	THERMAL DRYING UNIT HEATEC HEATER (124-1-91)	13.39	REFINERY FUEL GAS
LA-0211	GARYVILLE REFINERY	MARATHON PETROLEUM CO LLC	LA	7/16/2008 F	PETROLEUM REFINERY	A&B VACUUM TOWER HEATERS (3-08; 4-08)	12.39	REFINERY FUEL GAS
LA-0213	ST. CHARLES REFINERY	VALERO REFINING - NEW ORLEANS, LLC	LA	3/5/2010 F	PETROLEUM REFINERY	HEATERS (2008-1 - 2008-9)	12.39	PROCESS FUEL GAS
со								
RBLCID	FACILITY NAME	CORPORATE OR COMPANY NAME	FACILITY STATE	DATE DETERMINATION LAST UPDATED	FACILITY DESCRIPTION	PROCESS NAME	PROCCESS TYPE	PRIMARY FUEL
RBLCID NM-0050	FACILITY NAME  ARTESIA REFINERY	CORPORATE OR COMPANY NAME  NAVAJO REFINING COMPANY LLC		LAST UPDATED	FACILITY DESCRIPTION PETROLEUM REFINERY	PROCESS NAME  STEAM METHANE REFORMER HEATER	PROCCESS TYPE	PRIMARY FUEL  NATURAL GAS AND REFORMER OFF-GAS
			STATE	8/1/2008 F		STEAM METHANE REFORMER HEATER HEATER F-72-703 (7-81)		NATURAL GAS AND
NM-0050	ARTESIA REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC	NM	8/1/2008 F 3/5/2010 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A	11.3	NATURAL GAS AND REFORMER OFF-GAS
NM-0050 LA-0213	ARTESIA REFINERY ST. CHARLES REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC	NM LA	8/1/2008 F 3/5/2010 F 3/4/2010 F	PETROLEUM REFINERY PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER HEATER F-72-703 (7-81)	11.3 11.39	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS
NM-0050 LA-0213 MS-0086	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY	NM LA MS	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F	PETROLEUM REFINERY PETROLEUM REFINERY PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK	11.3 11.39 11.39	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYVILLE REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC	NM LA MS NM LA LA	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F	PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81) FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER	11.3 11.39 11.39 12.3 12.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY FUEL GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY	NM LA MS NM LA	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F	PETROLEUM REFINERY PETROLEUM REFINERY PETROLEUM REFINERY PETROLEUM REFINERY PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER	11.3 11.39 11.39 12.3 12.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYVILLE REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC	NM LA MS NM LA LA	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F	PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY  PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)	11.3 11.39 11.39 12.3 12.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY GAS REFINERY GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYVILLE REFINERY SINCLAIR REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY	NM LA MS NM LA LA LA WY	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater	11.3 11.39 11.39 12.3 12.31 12.39	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY GAS REFINERY GAS REFINERY FUEL GAS REFINERY FUEL GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071 *WY-0071 NM-0050 WA-0301	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYVILLE REFINERY SINCLAIR REFINERY SINCLAIR REFINERY ARTESIA REFINERY BY CHERRY POINT REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM	NM LA MS NM LA LA WY WY NM WA	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F 8/1/2008 F 8/16/2008 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER  PROCESS HEATER, IHT	11.3 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.3 13.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS NATURAL GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071 *WY-0071 NM-0050 WA-0301 *WY-0071	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYULLE REFINERY SINCLAIR REFINERY SINCLAIR REFINERY ARTESIA REFINERY BP CHERRY POINT REFINERY SINCLAIR REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM  SINCLAIR WYOMING REFINING COMPANY	NM LA MS NM LA LA WY WY NM WA WY	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F 8/1/2008 F 5/16/2006 E 10/15/2012 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER PROCESS HEATER, IHT Naphtha Splitter Heater	11.3 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.3 13.31 13.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071 NM-0050 WA-0301 *WY-0071 LA-0213	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYVILLE REFINERY SINCLAIR REFINERY SINCLAIR REFINERY ARTESIA REFINERY BY CHERRY POINT REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM	NM LA MS NM LA LA WY WY NM WA	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F 8/1/2008 F 5/16/2006 E 10/15/2012 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER  PROCESS HEATER, IHT	11.3 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.3 13.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS NATURAL GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071 *WY-0071 NM-0050 WA-0301 *WY-0071	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYULLE REFINERY SINCLAIR REFINERY SINCLAIR REFINERY ARTESIA REFINERY BP CHERRY POINT REFINERY SINCLAIR REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM  SINCLAIR WYOMING REFINING COMPANY	NM LA MS NM LA LA WY WY NM WA WY LA	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F 8/1/2008 F 5/16/2006 F 10/15/2012 F 8/1/2008 F 3/16/2006 F 10/15/2012 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER PROCESS HEATER, IHT Naphtha Splitter Heater	11.3 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.3 13.31 13.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071 NM-0050 WA-0301 *WY-0071 LA-0213	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYULLE REFINERY SINCLAIR REFINERY SINCLAIR REFINERY ARTESIA REFINERY BP CHERRY POINT REFINERY SINCLAIR REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM  SINCLAIR WYOMING REFINING COMPANY	NM LA MS NM LA LA WY WY NM WA WY	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F 8/1/2008 F 5/16/2006 E 10/15/2012 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER PROCESS HEATER, IHT Naphtha Splitter Heater	11.3 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.3 13.31 13.31	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS RATURAL GAS NATURAL GAS REFINERY FUEL GAS R
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071 *WY-0071 NM-0050 WA-0301 *WY-0071 LA-0213	ARTESIA REFINERY  ST. CHARLES REFINERY  CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY  ALLIANCE REFINERY  GARYVILLE REFINERY  SINCLAIR REFINERY  ARTESIA REFINERY  ARTESIA REFINERY  BP CHERRY POINT REFINERY  SINCLAIR REFINERY  ST. CHARLES REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM  SINCLAIR WYOMING REFINING COMPANY  VALERO REFINING - NEW ORLEANS, LLC	NM LA MS NM LA LA UY WY NM WA WY LA FACILITY	8/1/2008 F 3/5/2010 F 3/4/2010 F 8/1/2008 F 5/18/2012 F 7/16/2008 F 10/15/2012 F 10/15/2012 F 8/1/2008 F 5/16/2008 F 10/15/2012 F 3/5/2010 F  DATE DETERMINATION LAST UPDATED	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER PROCESS HEATER, IHT Naphtha Splitter Heater  DHT HEATERS (4-81, 5-81)	11.3 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.3 13.31 13.39	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS RATURAL GAS NATURAL GAS REFINERY FUEL GAS R
NM-0050 LA-0213 MS-0086 NM-0050 LA-0238 LA-0211 *WY-0071 *WY-0071 NM-0050 WA-0301 *WY-0071 LA-0213  VOC  RBLCID	ARTESIA REFINERY ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYVILLE REFINERY SINCLAIR REFINERY SINCLAIR REFINERY ARTESIA REFINERY BY CHERRY POINT REFINERY SINCLAIR REFINERY ST. CHARLES REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM  SINCLAIR WYOMING REFINING COMPANY  VALERO REFINING - NEW ORLEANS, LLC  CORPORATE OR COMPANY NAME	NM LA MS NM LA LA WY WY LA FACILITY STATE	8/1/2008 F  8/1/2008 F  3/5/2010 F  3/4/2010 F  8/1/2008 F  5/18/2012 F  7/16/2008 F  10/15/2012 F  8/1/2008 F  5/16/2006 F  10/15/2012 F  3/5/2010 F  DATE DETERMINATION LAST UPDATED	PETROLEUM REFINERY  PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER PROCESS HEATER, IHT  Naphtha Splitter Heater  DHT HEATERS (4-81, 5-81)	11.3 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.31 13.39 13.39	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS NATURAL GAS REFINERY FUEL GAS REFINERY FUEL GAS REFINERY FUEL GAS NATURAL GAS REFINERY FUEL GAS
NM-0050  LA-0213  MS-0086  NM-0050  LA-0238  LA-0211  *WY-0071  NM-0050  WA-0301  *WY-0071  LA-0213  VOC  RBLCID	ARTESIA REFINERY  ST. CHARLES REFINERY  CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY  ALLIANCE REFINERY  GARVYILLE REFINERY  SINCLAIR REFINERY  BY CHERRY POINT REFINERY  SINCLAIR REFINERY  ST. CHARLES REFINERY  FACILITY NAME	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM  SINCLAIR WYOMING REFINING COMPANY  VALERO REFINING - NEW ORLEANS, LLC  CORPORATE OR COMPANY NAME	NM LA MS NM LA LA WY WY NM WA WY LA  FACILITY STATE	8/1/2008 F  3/5/2010 F  3/4/2010 F  8/1/2008 F  5/18/2012 F  7/16/2008 F  10/15/2012 F  8/1/2008 F  10/15/2012 F  3/5/2010 F  DATE DETERMINATION LAST UPDATED  8/1/2008 F  7/16/2008 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER PROCESS HEATER, HIT Naphtha Splitter Heater  DHT HEATERS (4-81, 5-81)  PROCESS NAME  STEAM METHANE REFORMER HEATER  PLATFORMER HEATER CELLS NO. 1-3 (7A-08, 7B-08, & amp; 7C-	11.3 11.39 11.39 12.31 12.39 12.39 13.3 13.31 13.39 13.39	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS NATURAL GAS REFINERY FUEL GAS NATURAL GAS REFINERY FUEL GAS NATURAL GAS REFINERY FUEL GAS
NM-0050  LA-0213  MS-0086  NM-0050  LA-0238  LA-0211  *WY-0071  *WY-0071  NM-0050  WA-0301  *WY-0071  LA-0213  VOC  RBLCID  NM-0050  LA-0211	ARTESIA REFINERY  ST. CHARLES REFINERY CHEVRON PRODUCTS COMPANY, PASCAGOL ARTESIA REFINERY ALLIANCE REFINERY GARYVILLE REFINERY SINCLAIR REFINERY SINCLAIR REFINERY BY CHERRY POINT REFINERY SINCLAIR REFINERY ST. CHARLES REFINERY  FACILITY NAME  ARTESIA REFINERY  GARYVILLE REFINERY	NAVAJO REFINING COMPANY LLC  VALERO REFINING - NEW ORLEANS, LLC  UL CHEVRON PRODUCTS COMPANY  NAVAJO REFINING COMPANY LLC  CONOCOPHILLIPS COMPANY  MARATHON PETROLEUM CO LLC  SINCLAIR WYOMING REFINING COMPANY  SINCLAIR WYOMING REFINING COMPANY  NAVAJO REFINING COMPANY LLC  BRITISH PETROLEUM  SINCLAIR WYOMING REFINING COMPANY  VALERO REFINING - NEW ORLEANS, LLC  CORPORATE OR COMPANY LLC  MARATHON PETROLEUM CO LLC  MARATHON PETROLEUM CO LLC	NM LA MS NM LA LA WY WY LA FACILITY STATE  NM	8/1/2008 F  8/1/2008 F  3/5/2010 F  3/4/2010 F  8/1/2008 F  5/18/2012 F  7/16/2008 F  10/15/2012 F  8/1/2008 F  5/16/2006 F  10/15/2012 F  3/5/2010 F  DATE DETERMINATION LAST UPDATED  8/1/2008 F  7/16/2008 F	PETROLEUM REFINERY	STEAM METHANE REFORMER HEATER  HEATER F-72-703 (7-81)  FOUR PLATFORMER FEED/INTERSTAGE HEATER WITH A COMMON STACK ROSE 2 HOT OIL HEATER  FCCU FEED HEATER  A B VACUUM TOWER HEATERS (3-08; 4-08)  581 Crude Heater  BSI Heater  SULFUR RECOVERY HOT OIL HEATER PROCESS HEATER, IHT  Naphtha Spikter Heater  DHT HEATERS (4-81, 5-81)  PROCESS NAME  STEAM METHANE REFORMER HEATER  PLATFORMER HEATER CELLS NO. 1-3 (7A-08, 78-08, & Dec. 18)  PLATFORMER HEATER CELLS NO. 1-3 (7A-08, 78-08, & Dec. 18)  PROCESS NAME  PLATFORMER HEATER CELLS NO. 1-3 (7A-08, 78-08, & Dec. 18)  B Aump; HCU FRACTIONATOR HEATER (13-08)	11.3 11.39 11.39 11.39 12.3 12.31 12.39 12.39 13.3 13.31 13.31 13.39 13.39	NATURAL GAS AND REFORMER OFF-GAS REFINERY FUEL GAS NATURAL GAS NATURAL GAS REFINERY FUEL GAS

#### **Summary**

#### NOx

(VOC)

NOx RBLCID	FACILITY NAME	THROUGHPUT	THROUGHPUT UNIT	POLLUTANT	CONTROL METHOD DESCRIPTION	EMISSION LIMIT EMISSION LIMIT 1	EMISSION LIMIT 1 AVG TIME CONDITION	CASE-BY-CAS BASIS
PA-0252 WA-0324	SUNOCO, INC. (R&M) FERNDALE REFINERY		260 MMBTU/H	Nitrogen Oxides (NOx) Nitrogen Oxides (NOx)	ULTRALOW LOW NOX BURNER	0.035 LB/MMBTU 17 PPMDV	HOURLY 7% O2 OVER A 1-HOUR AVERAGING	BACT-PSD BACT-PSD
LA-0211	GARYVILLE REFINERY		0	0 Nitrogen Oxides (NOx)	ULTRA LOW NOX BURNERS (ULNB) AND SELECTIVE CATALYTIC REDUCTION (SCR VOLUNTARY)	0.0125 LB/MMBTU	ANNUAL AV	BACT-PSD
LA-0211	GARYVILLE REFINERY		0	0 Nitrogen Oxides (NOx)	ULTRA LOW NOX BURNERS (ULNB) WITHOUT AIR PREHEAT	0.03 LB/MMBTU	ANNUAL AVERAGE	BACT-PSD
LA-0213	ST. CHARLES REFINERY		633 MMBTU/H	Nitrogen Oxides (NOx)	LOW NOX BURNERS	0.08 LB/MMBTU	THREE ONE HOUR AVERAGE	BACT-PSD
NM-0050	ARTESIA REFINERY		120 MMBTU/H	Nitrogen Oxides (NOx)	ULTRA LOW NOX BURNERS	0.03 LB/MMBTU	3-HOUR ROLLING AVERAGE @ 3% O2	BACT-PSD
OK-0126 DE-0020	SUNOCO INC TULSA REFINERY VALERO DELAWARE CITY REFINERY		44 MMBTU/H 240 MMBTU/H	Nitrogen Oxides (NOx)	ULTRA LOW-NOX BURNERS SCR	0.03 LB/MMBTU 0.04 LB/MMBTU	3 HOUR AVERAGE 3-HR ROLLING AV	BACT-PSD RACT
*WY-0071	SINCLAIR REFINERY		50 MMBtu/hr	Nitrogen Oxides (NOx) Nitrogen Oxides (NOx)	Ultra Low NOx Burners	0.04 LB/MMBTU	3-HR AVERAGE	BACT-PSD
WA-0301	BP CHERRY POINT REFINERY		13 MMBTU/H	Nitrogen Oxides (NOx)	ULTRA LOW NOX BURNERS	0.1 LB/MMBTU	7% O2, 24 hr ave	BACT-PSD
PA-0256	SUNOCO, INC. (R&M)		98 MMBTU/H	Nitrogen Oxides (NOx)	ULTRA LOW NOX BURNERS	0.02 LBS/MMBTU	THREE 1-HOUR TESTS	LAER
PM						EMISSION LIMIT EMISSION LIMIT 1		CASE-BY-CAS
RBLCID	FACILITY NAME	THROUGHPUT	THROUGHPUT UNIT	POLLUTANT	CONTROL METHOD DESCRIPTION	1 UNIT	EMISSION LIMIT 1 AVG TIME CONDITION	BASIS
MT-0030	BILLINGS REFINERY		266 MMBTU/H	10 μ (FPM10)	GOOD COMBUSTION PRACTICES/USE OF CLEAN BURNING FUELS	0.0075 LB/MMBTU	PER ROLLING 12-MONTH TIME PERIOD	BACT-PSD
NM-0050	ARTESIA REFINERY		337 MMBTU/H	Particulate matter, filterable < 10 μ (FPM10)	GASEOUS FUEL COMBUSTION ONLY	0.0075 LB/MMBTU	HOURLY	BACT-PSD
LA-0211	GARYVILLE REFINERY			Particulate matter, filterable < 10 μ (FPM10)	PROPER DESIGN, OPERATION, AND GOOD ENGINEERING PRACTICES	0.0075 LB/MMBTU	3-HOUR AVERAGE	BACT-PSD
LA-0213	ST. CHARLES REFINERY			Particulate matter, total < 10 $\mu$ (TPM10)	PROPER EQUIPMENT DESIGN AND OPERATION, GOOD COMBUSTION PRACTICES, AND USE OF GASEOUS FUELS	0.0074 LB/MMBTU	ANNUAL AVERAGE	BACT-PSD
LA-0211	GARYVILLE REFINERY		9.6 MM BTU/H	Particulate matter, filterable < $10 \mu (FPM10)$		0.05 MAX LB/H		BACT-PSD
LA-0211	GARYVILLE REFINERY	15	55.2 MMBTU/H EA.	Particulate matter, filterable < 10 μ (FPM10)	PROPER DESIGN, OPERATION, AND GOOD ENGINEERING PRACTICES	0.0075 LB/MMBTU	3 HR AV	BACT-PSD
LA-0213	ST. CHARLES REFINERY			Particulate matter, total < 10 $\mu$ (TPM10)	COMPLY WITH 40 CFR 60 SUBPARTS NNN AND RRR	0	SEE NOTE	BACT-PSD
CO RBLCID	FACILITY NAME	THROUGHPUT	THROUGHPUT UNIT	POLLUTANT	CONTROL METHOD DESCRIPTION	EMISSION LIMIT EMISSION LIMIT 1	EMISSION LIMIT 1 AVG TIME CONDITION	CASE-BY-CAS BASIS
NM-0050	ARTESIA REFINERY		337 MMBTU/H	Carbon Monoxide	GASEOUS FUEL COMBUSTION ONLY	0.06 LB/MMBTU	3-HOUR ROLLING AVERAGE	BACT-PSD
LA-0213	ST. CHARLES REFINERY		633 MMBTU/H	Carbon Monoxide	PROPER DESIGN AND OPERATION, GOOD COMBUSTION PRACTICES	0.08 LB/MMBTU	THREE ONE HOUR TEST AVERAGE	BACT-PSD
MS-0086	CHEVRON PRODUCTS COMPANY, PASCAGOUL		850 MMBTU/H	Carbon Monoxide		132.6 LB/H	3-HR AVERAGE	BACT-PSD
NM-0050	ARTESIA REFINERY		120 MMBTU/H	Carbon Monoxide	GASEOUS FUEL COMBUSTION ONLY	0.06 LB/MMBTU	3-HOUR ROLLING AVERAGE @ 3% O2	BACT-PSD
LA-0238	ALLIANCE REFINERY	18	31.7 MMBTU/H	Carbon Monoxide	EQUIPPED WITH VORTOMETRIC HIGH INTENSITY COMBUSTION UNIT	0.55 LB/H	HOURLY MAXIMUM	BACT-PSD
LA-0211	GARYVILLE REFINERY	15	55.2 MMBTU/H EA.	Carbon Monoxide	PROPER DESIGN, OPERATION, AND GOOD ENGINEERING PRACTICES	0.04 LB/MMBTU	30 DAY ROLLING AVERAGE	BACT-PSD
*WY-0071	SINCLAIR REFINERY		233 MMBtu/hr	Carbon Monoxide	Good Combustion Practices	0.04 LB/MMBTU	3-HR AVERAGE	BACT-PSD
*WY-0071	SINCLAIR REFINERY		50 MMBtu/hr	Carbon Monoxide	Ultra Low NOx burners/good combustion	0.04 LB/MMBTU	3-HR AVERAGE	BACT-PSD
NM-0050	ARTESIA REFINERY		9.6 MMBTU	Carbon Monoxide	practices GOOD COMBUSTION PRACTICES	0	SEE NOTE	BACT-PSD
WA-0301	BP CHERRY POINT REFINERY		13 MMBTU/H	Carbon Monoxide	GOOD COMBUSTION PRACTICES	70 PPM	7% O2, 24 hr ave	BACT-PSD
*WY-0071	SINCLAIR REFINERY	4	16.3 MMBtu/hr	Carbon Monoxide	Good Combustion Practices	0.04 LB/MMBTU	3-HR AVERAGE	BACT-PSD
LA-0213	ST. CHARLES REFINERY		70 MMBTU/H EA	Carbon Monoxide	PROPER DESIGN AND OPERATION, GOOD COMBUSTION PRACTICES	0.08 LB/MMBTU	THREE ONE HOUR TEST AVERAGE	BACT-PSD
voc								
RBLCID	FACILITY NAME	THROUGHPUT	THROUGHPUT UNIT	POLLUTANT	CONTROL METHOD DESCRIPTION	EMISSION LIMIT EMISSION LIMIT 1 1 UNIT	EMISSION LIMIT 1 AVG TIME CONDITION	CASE-BY-CAS BASIS
NM-0050	ARTESIA REFINERY		337 MMBTU/H	Volatile Organic Compounds (VOC)	GASEOUS FUEL COMBUSTION ONLY	0.005 LB/MMBTU	HOURLY	BACT-PSD
LA-0211	GARYVILLE REFINERY			Volatile Organic Compounds (VOC)	PROPER DESIGN, OPERATION, AND GOOD ENGINEERING PRACTICES	0.0015 LB/MMBTU	3-HOUR AVERAGE	BACT-PSD
NM-0050	ARTESIA REFINERY		120 MMBTU/H	Volatile Organic Compounds (VOC)	GASEOUS FUEL COMBUSTION ONLY.	0.005 LB/MMBTU	HOURLY	BACT-PSD
LA-0211	GARYVILLE REFINERY	15	55.2 MMBTU/H EA.	Volatile Organic Compounds (VOC)	PROPER DESIGN, OPERATION, AND GOOD ENGINEERING PRACTICES	0.0015 LB/MMBTU	2 HOUR AVERAGE	BACT-PSD

## BAY AREA AIR QUALITY MANAGEMENT DISTRICT Best Available Control Technology (BACT) Guideline

## Source Category

		Revision:	3
Source:	Heater - Refinery Process, Forced Draft	Document #:	94.2.1
Class:	5 MMBtu/hr to <50 MMBtu/hr Heat Input	Date:	08/12/94

#### **Determination**

POLLUTANT	BACT 1. Technologically Feasible/ Cost Effective 2. Achieved in Practice	TYPICAL TECHNOLOGY
POC	1. n/d 2. n/s	1. n/d 2. Good Combustion Practice <sup>a</sup>
NOx	1. 10 ppmv @ 3% O <sub>2</sub> Dry <sup>a,b,c,e</sup> 2. 20 ppmv @ 3% O <sub>2</sub> Dry <sup>a,b,e</sup>	1. Selective Catalytic Reduction (SCR) + Low $NO_x$ Burners $^{a,b,c}$ 2. Low $NO_x$ Burners; + Flue Gas Recirculation; or Low $NO_x$ Burners + Selective Non-Catalytic Reduction (SNCR); or Selective Catalytic Reduction (SCR)
$\mathrm{SO}_2$	1. Natural Gas or Treated Refinery Gas Fuel w/ ≤50 ppmv Hydrogen Sulfide and ≤100 ppmv Total Reduced Sulfur <sup>a</sup> 2. Natural Gas or Treated` Refinery Gas Fuel w/ ≤100 ppmv Total Reduced Sulfur <sup>a</sup>	<ul> <li>1. Fuel Selection<sup>a</sup></li> <li>2. Fuel Selection<sup>a</sup></li> </ul>
СО	1. n/d 2. 50 ppmv @ 3% O <sub>2</sub> Dry <sup>a,f</sup>	1. n/d 2. Good Combustion Practice <sup>a</sup>
PM <sub>10</sub>	1. n/d 2. Natural Gas or Treated Refinery Gas Fuel <sup>a,b</sup>	1. n/d 2. Fuel Selection <sup>a,b</sup>
NPOC	1. n/a 2. n/a	1. n/a 2. n/a

## References

- a. BAAQMD
- b. BAAQMD A #30783
- c. BAAQMD A #3318
- d. BAAQMD A #8407
- e.  $NO_x$  determination by BAAQMD Source Test Method ST-13A or B (average of three 30-minute sampling runs); or Continuous Emission Monitor (3-hour average); or BAAQMD approved equivalent.
- f. CO determination by BAAQMD Source Test Method ST-6 (average of three 30 minute sampling runs); or Continuous Emission Monitor (3-hour average); or BAAQMD approved equivalent.

## BAY AREA AIR QUALITY MANAGEMENT DISTRICT Best Available Control Technology (BACT) Guideline

## Source Category

Source	Heater - Refinery Process, Natural or Induced Draft	Revision:	3
Source.	Heater - Refinery Process, Natural or Induced Draft	Document #:	94.1.1
Class:	5 MMBtu/hr to <50 MMBtu/hr Heat Input	Date:	08/12/94

#### **Determination**

POLLUTANT	BACT 1. Technologically Feasible/ Cost Effective 2. Achieved in Practice	TYPICAL TECHNOLOGY
POC	1. n/d 2. n/s	1. n/d 2. Good Combustion Practice <sup>a</sup>
NOx	<ol> <li>10 ppmv @ 3% O<sub>2</sub> Dry<sup>a,b,c,e</sup></li> <li>25 ppmv @ 3% O<sub>2</sub> Dry<sup>a,b,e</sup></li> </ol>	1. Selective Catalytic Reduction (SCR) + Low $NO_x$ Burners $^{a,b,c}$ 2. Low $NO_x$ Burners; or Low $NO_x$ Burners + Selective Non-Catalytic Reduction (SNCR) $^{a,d}$
$\mathrm{SO}_2$	1. Natural Gas or Treated Refinery Gas Fuel w/ ≤50 ppmv Hydrogen Sulfide and ≤100 ppmv Total Reduced Sulfur <sup>a</sup> 2. Natural Gas or Treated` Refinery Gas Fuel w/ ≤100 ppmv Total Reduced Sulfur <sup>a</sup>	<ul> <li>1. Fuel Selection<sup>a</sup></li> <li>2. Fuel Selection<sup>a</sup></li> </ul>
СО	1. n/d 2. 50 ppmv @ 3% O <sub>2</sub> Dry <sup>a,f</sup>	1. n/d 2. Good Combustion Practice <sup>a</sup>
PM <sub>10</sub>	1. n/d 2. Natural Gas or Treated Refinery Gas Fuel <sup>a,b</sup>	1. n/d 2. Fuel Selection <sup>a,b</sup>
NPOC	1. n/a 2. n/a	1. n/a 2. n/a

## References

- a. BAAQMD
- b. BAAQMD A #30783
- c. BAAQMD A #3318
- d. BAAQMD A #8407
- e.  $NO_x$  determination by BAAQMD Source Test Method ST-13A or B (average of three 30-minute sampling runs); or Continuous Emission Monitor (3-hour average); or BAAQMD approved equivalent.
- f. CO determination by BAAQMD Source Test Method ST-6 (average of three 30 minute sampling runs); or Continuous Emission Monitor (3-hour average); or BAAQMD approved equivalent.

# BAY AREA AIR QUALITY MANAGEMENT DISTRICT Best Available Control Technology (BACT) Guideline

## Source Category

		Revision:	4
Source:	Heater - Refinery Process	Document #:	94.3.1
Class:	>50 MMBtu/hr Heat Input	Date:	1/14/08

## Determination

POLLUTANT	BACT 1. Technologically Feasible/ Cost Effective 2. Achieved in Practice	TYPICAL TECHNOLOGY
POC	1. n/d 2. n/s	n/d     Good Combustion     Practice <sup>a</sup>
NOx	1. <i>n/d</i> 2. 5 ppmv @ 3% O <sub>2</sub> Dry <sup>c,d,e</sup>	<ol> <li>n/d</li> <li>Selective Catalytic         Reduction (SCR) + Low         NO<sub>x</sub> Burners<sup>c,d</sup></li> </ol>
SO <sub>2</sub>	<ol> <li>Natural Gas or Treated Refinery Gas Fuel w/ ≤50 ppmv Hydrogen Sulfide and ≤100 ppmv Total Reduced Sulfur<sup>a</sup></li> <li>Natural Gas or Treated` Refinery Gas Fuel w/ ≤100 ppmv Total Reduced Sulfur<sup>a</sup></li> </ol>	<ol> <li>Fuel Selection<sup>a</sup></li> <li>Fuel Selection<sup>a</sup></li> </ol>
со	<ol> <li>n/d</li> <li>10 ppmv @ 3% O<sub>2</sub></li> <li>Dry<sup>c,d,f</sup></li> </ol>	n/d     Good Combustion     Practice in Conjunction w/     Selective Catalytic     Reduction (SCR)     System <sup>c,d</sup>
PM <sub>10</sub>	n/d     Natural Gas or Treated     Refinery Gas Fuel <sup>a,b</sup>	<ol> <li>n/d</li> <li>Fuel Selection<sup>a,b</sup></li> </ol>
NPOC	1. n/a 2. n/a	1. <i>n/a</i> 2. n/a

## References

- a. BAAQMD A #8407
- b. BAAQMD A #30783
- c. ARB BACT Clearinghouse, based on several South Coast AQMD projects. Recommend ammonia slip limit of 10 ppmv at 3% O<sub>2</sub>.
- d. Authority to Construct issued for BAAQMD applications 13424 & 13678 for CononcoPhillips Clean Fuels Expansion Project. For 85 MM BTU/hr furnace, the CO limit only applies at firing rates greater than 30 MM BTU/hr.
- e. NO<sub>x</sub> determination by Continuous Emission Monitor (3-hour average); or BAAQMD approved equivalent.
- f. CO determination by Continuous Emission Monitor (3-hour average); or BAAQMD approved equivalent.

## Attachment H CO Cost Effectiveness Analysis

## Heater Firing Rate Increase Plan Approval

#### CO BACT Analysis

Assumptions for all heaters:

1	Number of Years	10	
I	nterest Rate (%)	21.83	Based on 90% equity cost of the average Carlyle energy funds and 10% after tax debt cost.
1	Annualized Cost factor	0.253	

$$ACF = \frac{i(1+i)^n}{(1+i)^n - 1}$$

EPA Air Pollution Control Cost Manual, Sixth Edition, EPA/452/B-02-001 - Equation 2.8a

Year	Chemical Engineering Cost Index
2002	395.6
2012	582.2
Cost Escalation Factor	1.47

Oxidation Catalyst Costs <sup>1</sup>	EPA, \$/cfm (2002 Basis)	EPA, \$/cfm (2012 Basis)
Capital Cost for Oxidation Catalyst	35.0	51.5
O&M Cost for Oxidation Catalyst	6.0	8.8

<sup>1</sup> Based on EPA Air Pollution Control Technology Fact Sheet for Regenerative Incinerator (EPA-452/F-03-021). Capital costs range from \$35 to \$140 per cfm and O&M costs range from \$6 to \$20 per cfm.

	A	В	C	D	E	F	G	Н	I	J	K	L
Heater	Proposed Hourly Firing Limit (MMBtu/yr) <sup>1</sup>	Projected Actual CO Emissions (TPY) <sup>2</sup>	Control Efficiency (%)	Maximum Potential Post Control Emissions (TPY)	Potential CO Reduced (TPY)		Stack Temp (°F)	Stack Flow (SCFM)	Capital Cost (\$)	O&M Cost (\$)	Annualized Cost <sup>4</sup> (\$)	Cost Effectiveness (\$/Ton)
Unit 231-B101	856,000	34.4	92.0	2.8	31.6	36,560	550.4	19,105	984,081	168,700	418,154	13,214
Unit 865-11H1	699,000	28.5	92.0	2.3	26.2	32,461	600.8	16,157	832,236	142,669	353,632	13,498
Unit 865-11H2	500,000	20.4	92.0	1.6	18.7			9,320	480,049	82,294	203,982	10,884
Unit 210-H101	1,643,000	66.9	92.0	5.4	61.6	76,435	640.4	36,675	1,889,120	323,849	802,722	13,035
Unit 210-H201	2,172,000	88.5	92.0	7.1	81.4	117,282	474.8	66,244	3,412,169	584,943	1,449,894	17,810
Unit 866-12H1	456,000	18.6	92.0	1.5	17.1			8,884	457,617	78,449	194,450	11,377
Unit 868-8H101	480,000	18.9	92.0	1.5	17.4	18,918	500.0	10,405	535,947	91,877	227,734	13,101
	Calculation			= B * (1 - C)	= B - D			= F / ((460 + G)/(460+68))			= (I * ACF) + J	= K / E

#### Notes:

Trace levels of SO<sub>2</sub> will result in deactivation of the catalyst by sulfur-containing compounds. Oxidation catalysts are not typically installed on refinery fuel gas fired process heaters.

Oxidation catalysts typically operate at 650°F to 1,000°F. As shown above, none of the heaters in this analysis achieve stack temperatures within the typical operating range.

<sup>&</sup>lt;sup>1</sup> Consistent with the proposed annual firing rate limits requested in the Plan Approval application.

<sup>&</sup>lt;sup>2</sup> Consistent with the future projected actual emissions in the Plan Approval application.

<sup>&</sup>lt;sup>3</sup> Stack flows (SCFM) for Unit 865-11H2 and Unit 866-12H1 Heaters were estimated using EPA Method 19 factor of 8,710 dscf/MMBtu and the proposed RACT limit.

<sup>&</sup>lt;sup>4</sup> See above for details on the Annualized Cost Factor (ACF).

## Attachment I BAT Cost Effectiveness Analysis

## NOx BAT Control Cost Effectiveness Cost Effectiveness Summary

Control Option	Cost	Cost Effectiveness (\$/Ton)					
Control Option	Unit 865-11H2	Unit 866-12H1	Unit 868-8H101				
ULNB & SCR	38,565	40,951	38,390				
SCR	37,016	39,414	36,992				
ULNB	7,578	7,921	7,377				
LNB & SNCR	12,424	13,322	15,892				
LNB & FGR	9,790	10,534	14,197				
SNCR	14,771	15,729	14,763				

Assumptions for all heaters:

Number of Years (n)	10
Interest Rate, % (i)	21.83
Annualized Cost Factor (ACF)	0.253

Based on 90% equity cost of the average Carlyle energy funds and 10% after tax debt cost.

$$ACF = \frac{i(1+i)^n}{(1+i)^n - 1}$$

EPA Air Pollution Control Cost Manual, Sixth Edition, EPA/452/B-02-001 - Equation 2.8a

Year	Chemical Engineering Cost Index
1986	318.4
1991	361
2012	582.2
Cost Escalation Factor for SCR <sup>1</sup>	1.83
Cost Escalation Factor for LNB,	
SNCR, and FGR <sup>2</sup>	1.61

 $<sup>^1</sup>$  Cost data from Alternative Control Techniques Document - NO  $_{\rm X}$  Emissions from Process Heaters (Revised) - EPA-453/R-93-034 scaled from 1986 to 2012 costs using the Cost Escalation Factor.

 $<sup>^2</sup>$  Cost data from *Alternative Control Techniques Document - NO \_{\rm X} Emissions from Process Heaters (Revised) - EPA-453/R-93-034 scaled from 1991 to 2012 costs using the Cost Escalation Factor.* 

Source		Control Efficiency	Comment
Ultra low-NO <sub>x</sub> burners and Selective Catalytic Reduction	ULNB & SCR	96%	Combining both removal efficiencies of ULNB and SCR.
Selective Catalytic Reduction	SCR	85%	Based on Unit 1332 Performance.
Ultra low-NO <sub>x</sub> burners	ULNB	73%	Based on vendor experience at 0.03 lb/MMBtu.
$Low-NO_x$ burners and Selective Non-Catalytic Reduction	LNB & SNCR	70%	Combining both removal efficiencies. Assumes 50% control efficiency for LNB and 40% control efficiency for SNCR. <i>Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) -</i> EPA-453/R-93-034.
Low-NO <sub>x</sub> burners and Flue Gas Recirculation	LNB & FGR	55%	Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034.
Selective Non-Catalytic Reduction	SNCR	40%	Heater stack temperature below 700°F results in low NOx removal efficiency. EPA Air Pollution Control Technology Fact Sheet - EPA-452/F-03-031.

Source Name	Design Capacity (MMBtu/hr)	New Firing (MMBtu/year)	NO <sub>x</sub> Emission Rate (lb/MMBtu)	Number of Burners
Unit 865-11H2	64.2	500,000	0.113	8
Unit 866-12H1	61.2	456,000	0.113	6
Unit 868-8H101	60.0	480,000	0.113	4

#### Heater Firing Rate Increase Plan Approval

#### NOx BAT Control Cost Effectiveness

Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034 All costs are scaled from 2012 U.S. dollars using the appropriate Cost Escalation Factor.

#### Capital Cost of Low NO<sub>x</sub> Burners (page 6-4 and 6-5):

$$TCI = 30,000 + HQ[5,230 - (622 \times BQ) + (26.1 \times BQ^2)]$$

Where:

TCI = Total Capital Investment

HQ = heater capacity (GJ/hr)

BQ = burner heat release rate (GJ/hr)

 $BQ = HQ/NB \times (1.158 + 8/HQ)$ 

NB = number of burners

#### Capital Cost of Ultra-low NOx Burners:

See the "Refinery ULNB Control Costs" tab for capital cost details for Ultra-low NO<sub>x</sub> Burners

#### Capital Cost of Selective Non-Catalytic Reduction (page 6-7):

$$TCI = 31,850(HQ)^{0.6}$$

HQ = heater capacity (GJ/hr)

#### Operating Cost of Selective Non-Catalytic Reduction (page 6-8):

Where:

Q = heater capacity, MMBtu/hr

$$Electricty\ cost = \left(\frac{0.3\ kWh}{ton\ NH_3}\right) \times \left(\frac{ton\ NH_3}{year}\right) \times \left(\frac{\$0.06}{kWh}\right)$$

Where

## Capital Cost of Selective Catalytic Reduction (page 6-8):

$$TCI = 1,373,000 \times \left(\frac{Q}{48.5}\right)^{0.6} + 49,000 \times \left(\frac{Q}{485}\right)$$

Where:

Q = heater capacity, MMBtu/hr

#### Operating Cost of Selective Catalytic Reduction (page 6-9):

$$NH_{3}\;cost = Q \;\times\; (lb/MMBtu) \times \left(\frac{1\;mole\;NO_{x}}{46\;lb\;NO_{x}}\right) \times \left(\frac{17\;lb\;NH_{3}}{1\;mole\;NH_{3}}\right) \times \left(\frac{1\;mole\;NH_{3}}{1\;mole\;NO_{x}}\right) \times \left(\frac{\$0.125}{lb\;NH_{3}}\right) \times \left(\frac{8,760\;hours}{year}\right)$$

Where:

Q = heater capacity, MMBtu/hr

Note the capacity factor has been assumed to be equal to 1; therefore, the capacity factor term has been omitted

Catalyst Replacement Cost = 
$$49,000 \times \frac{Q}{48.5} / 5$$
 years

$$Electricty \ cost = \ \left(\frac{0.3 \ kWh}{ton \ NH_3}\right) \times \left(\frac{ton \ NH_3}{year}\right) \times \left(\frac{\$0.06}{kWh}\right)$$

Where

$$\frac{ton \ NH_3}{year} = Q \ \times \ (lb \ NO_x/MMBtu) \times \left(\frac{1 \ mole \ NO_x}{46 \ lb \ NO_x}\right) \times \left(\frac{17 \ lb \ NH_3}{1 \ mole \ NH_3}\right) \times \left(\frac{1 \ mole \ NH_3}{1 \ mole \ NO_x}\right) \times \left(\frac{ton}{2000 \ lb}\right) \times \left(8,760 \frac{hours}{year}\right) \times \left(\frac{10 \ NH_3}{1 \ mole \ NH_3}\right) \times \left(\frac{10 \ NH_3}{1 \ mole \ NH_3}\right)$$

#### Capital Cost of Flue Gas Recirculation (page 6-9):

$$TCI = 12,800(HQ)^{0.6}$$

Where:

HQ = heater capacity (GJ/hr)

#### Operating Cost of Flue Gas Recirculation (page 6-10):

$$Electricty\ cost =\ (motor\ hp) \times \left(\frac{0.75\ kW}{hp}\right) \times \left(\frac{8,760\ hours}{year}\right) \times \left(\frac{\$0.06}{kWh}\right)$$

Where:

motor hp = FGR fan motor horsepower,  $(1/5) \times (Q)$ 

Q = heater capacity, MMBtu/hr

## <u>Ultra Low NO<sub>x</sub> Burner Costs</u>

Economic Data	Heater Fired Duty (MMBtu/hr)	Number of Burners	Burner Heat Release (MMBtu/hr/burner)	Base Year ULNB Cost (\$/burner)	Normalized Cost (\$/MMBtu/hr)
1332 H-400/H-401 Heater	419	54	7.8	\$50,000	\$6,444
137 F-3 Heater	60	4	15	\$80,500	\$5,367
				Average	\$5,905

SOURCE NAME	Rated Capacity (MMBtu/hr)	ULNB Capital Cost Using (\$/MMBtu/hr)	ULNB Total Capital Investment
Unit 865-11H2	64.2	\$379,120	\$559,581
Unit 866-12H1	61.2	\$361,404	\$0
Unit 868-8H101	60.0	\$354,317	\$0

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 865-11H2 BAT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	New Firing (MMBtu/yr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ New Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	500,000	0.113	28.3	96%	1.1	27.1	3,631,525	125,523	1,046,078	38,565
SCR	500,000	0.113	28.3	85%	4.2	24.0	3,071,944	110,135	888,841	37,016
ULNB	500,000	0.113	28.3	73%	7.5	20.8	559,581	15,388	157,237	7,578
LNB & SNCR	500,000	0.113	28.3	70%	8.5	19.8	857,483	28,316	245,679	12,424
LNB & FGR	500,000	0.113	28.3	55%	12.7	15.5	512,272	22,250	152,106	9,790
SNCR	500,000	0.113	28.3	40%	17.0	11.3	577,165	20,607	166,913	14,771
	Calculation		= A * B / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Notes:

 $<sup>^{1}</sup>$  Unit 865-11H2 is projected to be above PADEP presumptive RACT firing limits and assumed NO  $_{\rm x}$  emission rate limit of 0.113 lb/MMBtu is used.

<sup>&</sup>lt;sup>2</sup> See "BAT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

Source Unit 865-11H2 Control ULNB & SCR

Rated Heat Input64.2MMBtu/hrRated Heat Input500,000MMBtu/yrNumber of Burners8.0BurnersBaseline Actual Emissions28.3tpyCurrent Emission Rate0.113lb/MMBtu

Control Efficiency 96%

Heater Capacity 67.7 GJ/hr Burner Heat Release Rate 10.8 GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS - ULNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	379,120
	Instrumentation (10% of EC)	37,912
	Sales taxes (5% of EC)	18,956
	Freight (8% of EC)	30,330
	Subtotal - Purchased Equipment Costs (PEC)	466,317
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical;	
	piping; etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC) - ULNB	466,317
INDIRECT INSTALLATI	ON COSTS - ULNB	
	Engineering Costs (5% of PEC)	23,316
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	46.632
	Start-up (1% of PEC)	4,663
	Performance Test (1% of PEC)	4,663
	Contingency (3% of PEC)	13,990
TOTAL INDIRECT COST	TS, IC	93,263
DIRECT COSTS SCR		
DIRECT COSTS - SCR	P 1 15 :	
	Purchased Equipment Costs Equipment Cost (EC)	2,982,470
		2,982,470
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	2,982,470
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical;	
	piping; etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC) - SCR	2,982,470
INDIRECT INSTALLATI	ON COSTS - SCR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	89,474
TOTAL INDIRECT COST	TS, IC - SCR	89,474
TOTAL CAPITAL	INVESTMENT (TCI) - ULNB	559,581
	INVESTMENT (TCI) - SCR	3,071,944
	INVESTMENT (TCI) - SCR INVESTMENT (TCI)	
IOTAL CAPITAL	INVESTIMENT (ICI)	3,631,525

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	99,867 <b>99,867</b>
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,735
Catalyst Replacement Cost	20,921
Electricity Cost	0.3
Subtotal - Utilities	25,656
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	125,523

COST COMPONENT:	COST (\$)
TOTAL ANNUAL O&M COSTS	125,523
Annualized Cost Factor  Equipment Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	0.25
CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT	3,631,525
TOTAL ANNUAL CAPITAL REQUIREMENT	920,555
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)	1,046,078

## **Heater Firing Rate Increase Plan Approval**

## **NOx BAT Control Cost Effectiveness**

Source	Unit 865-11H2	
Control	SCR	
Rated Heat Input	64.2	MMBtu/hr
Rated Heat Input	500,000	MMBtu/yr
Number of Burners	8.0	Burners
<b>Baseline Actual Emissions</b>	28.3	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
<b>Control Efficiency</b>	85%	
Heater Capacity	67.7	GJ/hr
<b>Burner Heat Release Rate</b>	10.8	GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,982,470
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	2,982,470
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC)	2,982,470
INDIRECT INSTALLATIO	ON COSTS	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	89,474
TOTAL INDIRECT COST	S, IC	89,474
TOTAL CAPITAL I	INVESTMENT (TCI)	3,071,944

	COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS Operation an	ANNUAL DIRECT COSTS  Operation and Maintenance Labor			
r	Maintenance Labor and Material (2.75%	of TCI)		84,478 84,478
Annualized Cost Factor	Re	eplacement Life (years) =	10	
	Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
Replacement	cost			
Subtotal - Op	peration and Maintenance Labor			
Utilities				
	Ammonia Cost			4,735
	Catalyst Replacement Cost Electricity Cost			20,921 0.3
Subtotal - Ut	ilities			25,656
TOTAL ANNUAL D	DIRECT COSTS <sup>a</sup>			110,135

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M C	OSTS			110,135
Annualized Cost Factor	Equi	ipment Life (years) = Interest Rate (%) =	10 21.83	0.25
CAPITAL RECOVERY COS	TS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIREME	NT		3,071,944 <b>778,70</b> 7
TOTAL ANNUALIZED CO				888,841

## **Heater Firing Rate Increase Plan Approval**

#### **NOx BAT Control Cost Effectiveness**

Source	Unit 865-11H2	
Control	ULNB	
Rated Heat Input	64.2	MMBtu/hr
Rated Heat Input	500,000	MMBtu/yr
Number of Burners	8.0	Burners
<b>Baseline Actual Emissions</b>	28.3	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	73%	
<b>Heater Capacity</b>	67.7	GJ/hr
<b>Burner Heat Release Rate</b>	10.8	GJ/hr

## **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	379,120
	Instrumentation (10% of EC)	37,912
	Sales taxes (5% of EC)	18,956
	Freight (8% of EC)	30,330
	Subtotal - Purchased Equipment Costs (PEC)	466,317
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	TDC)	466,317
INDIRECT INSTALLATIO	ON COSTS	
	Engineering Costs (5% of PEC)	23,316
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	46,632
	Start-up (1% of PEC)	4,663
	Performance Test (1% of PEC)	4,663
	Contingency (3% of PEC)	13,990
TOTAL INDIRECT COST	TS, IC	93,263
TOTAL CAPITAL	INVESTMENT (TCI)	559,581

TOTAL ANNUAL DIRECT COSTS<sup>a</sup>

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	45.200
Maintenance Labor and Material (2.75% of TCI)	15,388 15,388
Annualized Cost Factor	
Replacement	Life (years) = 10
Intere	est Rate (%) = 21.83
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
None	
Subtotal - Utilities	0.0

C	COST COMPONENT:	COST (\$)
TOTAL ANNUAL O&M COST	'S	15,388
	Equipment Life (years) = 10  Interest Rate (%) = 21.8  Interest Rate (%) = 21.8	
	OTAL CAPITAL REQUIREMENT OTAL ANNUAL CAPITAL REQUIREMENT	559,581 <b>141,848</b>
TOTAL ANNUALIZED COST (Total annual O&M cost and an		157,237

15,388

Heater Firing Rate Increase Plan Approval

NOx BAT Control Cost Effectiveness

Source Unit 865-11H2
Control LNB & SNCR

 Rated Heat Input
 64.2
 MMBtu/hr

 Rated Heat Input
 500,000
 MMBtu/yr

 Number of Burners
 8.0
 Burners

 Baseline Actual Emissions
 28.3
 tpy

 Current Emission Rate
 0.113
 lb/MMBtu

Control Efficiency 70%

Heater Capacity 67.7 GJ/hr Burner Heat Release Rate 10.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	189,917
	Instrumentation (10% of EC)	18,992
	Sales taxes (5% of EC)	9,496
	Freight (8% of EC)	15,193
	Subtotal - Purchased Equipment Costs (PEC)	233,598
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST.	S (TDC) - LNB	233,598
INDIRECT INSTALLAT	TON COSTS - LNB	
	Engineering Costs (5% of PEC)	11,680
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	23,360
	Start-up (1% of PEC)	2,336
	Performance Test (1% of PEC)	2,336
	Contingency (3% of PEC)	7,008
TOTAL INDIRECT CO	STS, IC - LNB	46,720
DIRECT COSTS - SNC	R	
	Purchased Equipment Costs	
	Equipment Cost (EC)	560,355
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	560,355
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST.	S (TDC) - SNCR	560,355
INDIRECT INSTALLAT	TION COSTS - SNCR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	16,811
TOTAL INDIRECT CO	STS, IC - SNCR	16,811
TOTAL CAPITAL	INVESTMENT (TCI) - LNB	280,318
	INVESTMENT (TCI) - SNCR	577,165
TOTAL CAPITAL	INVESTMENT (TCI)	857,483

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	23,581 23,581
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,735
Electricity Cost	0.3
Subtotal - Utilities	4,735
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	28,316

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M	COSTS			28,316
Annualized Cost Factor				
	Equipme	ent Life (years) =	10	
	Int	erest Rate (%) =	21.83	
	Annualized Cost Factor			0.25
CAPITAL RECOVERY CO	STS			
	TOTAL CAPITAL REQUIREMENT			857,483
	TOTAL ANNUAL CAPITAL REQUIREMENT			217,363
TOTAL ANNUALIZED ( (Total annual O&M cost o	OST and annualized capital cost)			245,679

Heater Firing Rate Increase Plan Approval

NOx BAT Control Cost Effectiveness

Source Unit 865-11H2 Control LNB & FGR

 Rated Heat Input
 64.2
 MMBtu/hr

 Rated Heat Input
 500,000
 MMBtu/yr

 Number of Burners
 8.0
 Burners

 Baseline Actual Emissions
 28.3
 tpy

 Current Emission Rate
 0.113
 lb/MMBtu

Control Efficiency 55%

Heater Capacity 67.7 GJ/hr Burner Heat Release Rate 10.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	189,917
	Instrumentation (10% of EC)	18,992
	Sales taxes (5% of EC)	9,496
	Freight (8% of EC)	15,193
	Subtotal - Purchased Equipment Costs (PEC)	233,598
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TI	OC) - LNB	233,598
INDIRECT INSTALLATION	COSTS - LNB	
	Engineering Costs (5% of PEC)	11,680
	Construct. & Field Expenses (Included in above costs)	11,000
	Contractor Fees (10% of PEC)	23,360
	Start-up (1% of PEC)	2,336
	Performance Test (1% of PEC)	2,336
	Contingency (3% of PEC)	7,008
TOTAL INDIRECT COSTS,	IC - LNB	46,720
DIRECT COSTS - FGR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	225,197
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	225,197
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TI	OC) - FGR	225,197
INDIRECT INSTALLATION	COSTS - FGR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	6,756
TOTAL INDIRECT COSTS,	IC - FGR	6,756
TOTAL CAPITAL IN	VESTMENT (TCI) - LNB	280,318
	VESTMENT (TCI) - FGR	231,953
TOTAL CAPITAL IN	· /	512,272

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	14,087 14,087
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83 Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities Electricity Cost	8,163
Subtotal - Utilities	8,163
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	22,250

COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M COSTS			22,250
Annualized Cost Factor			
	Equipment Life (years) =	10	
	Interest Rate (%) =	21.83	
Annualized Cost Factor			0.25
CAPITAL RECOVERY COSTS			
TOTAL CAPITAL REQUIREMEN	TT .		512,272
TOTAL ANNUAL CAPITAL RE	QUIREMENT		129,856
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)			152,106

**Heater Firing Rate Increase Plan Approval** 

#### **NOx BAT Control Cost Effectiveness**

Source	Unit 865-11H2	
Control	SNCR	
Rated Heat Input	64.2	MMBtu/hr
Rated Heat Input	500,000	MMBtu/yr
Number of Burners	8.0	Burners
<b>Baseline Actual Emissions</b>	28.3	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	40%	
Heater Capacity	67.7	GJ/hr
<b>Burner Heat Release Rate</b>	10.8	GJ/hr

## Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	560,355
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	560,355
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S(TDC)	560,355
INDIRECT INSTALLAT	TON COSTS	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	16,811
TOTAL INDIRECT COS	STS, IC	16,811
TOTAL CAPITAI	L INVESTMENT (TCI)	577,165

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	15,872 15,872
Annualized Cost Factor  Replacement Life (years) =  Interest Rate (%) = 2  Annualized Cost Factor	10 :1.83 0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities Ammonia Cost Electricity Cost	4,735 0.3
Subtotal - Utilities	4,735
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	20,607

COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M COSTS			20,607
Annualized Cost Factor  Annualized Cost Factor	Equipment Life (years) = Interest Rate (%) =	10 21.83	0.25
CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQU	UIREMENT		577,165 <b>146,306</b>
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)			166,913

### PES Refinery Heater Firing Rate Increase Plan Approval Unit 866-12H1 BAT Cost Effectiveness Summary

	A	В	С	D	E	F	G	Н	I	J
Control Option	New Firing (MMBtu/yr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ New Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	456,000	0.113	25.8	96%	1.0	24.7	3,518,199	121,208	1,013,036	40,951
SCR	456,000	0.113	25.8	85%	3.9	21.9	2,984,767	106,538	863,147	39,414
ULNB	456,000	0.113	25.8	73%	6.8	18.9	533,432	14,669	149,889	7,921
LNB & SNCR	456,000	0.113	25.8	70%	7.7	18.0	838,966	27,585	240,255	13,322
LNB & FGR	456,000	0.113	25.8	55%	11.6	14.2	503,525	21,628	149,267	10,534
SNCR	456,000	0.113	25.8	40%	15.5	10.3	560,828	19,936	162,101	15,729
	Calculation		= A * B / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Notes:

 $<sup>^{1}</sup>$  Unit 866-12H1 is projected to be above PADEP presumptive RACT firing limits and assumed NO $_{x}$  emission rate limit of 0.113 lb/MMBtu is used.

<sup>&</sup>lt;sup>2</sup> See "BAT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

Source Unit 866-12H1
Control ULNB & SCR

 Rated Heat Input
 61.2
 MMBtu/hr

 Rated Heat Input
 456,000
 MMBtu/yr

 Number of Burners
 6.0
 Burners

 Baseline Actual Emissions
 25.8
 tpy

 Current Emission Rate
 0.113
 lb/MMBtu

 Control Efficiency
 96%

Heater Capacity 64.6 GJ/hr Burner Heat Release Rate 13.8 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - ULNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	361,404
	Instrumentation (10% of EC)	36,140
	Sales taxes (5% of EC)	18,070
	Freight (8% of EC)	28,912
	Subtotal - Purchased Equipment Costs (PEC)	444,527
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC) - ULNB	444,527
INDIRECT INSTALLATI	ON COSTS - ULNB	
	Engineering Costs (5% of PEC)	22,226
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	44,453
	Start-up (1% of PEC)	4,445
	Performance Test (1% of PEC)	4,445
	Contingency (3% of PEC)	13,336
TOTAL INDIRECT COS	TS, IC	88,905
DIRECT COSTS - SCR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,897,832
	Instrumentation (10% of EC)	2,057,032
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	2,897,832
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC) - SCR	2,897,832
INDIRECT INSTALLATI	ON COSTS - SCR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	86,935
TOTAL INDIRECT COS	TS, IC - SCR	86,935
TOTAL CAPITAL	INVESTMENT (TCI) - ULNB	533,432
	INVESTMENT (TCI) - SCR	2,984,767
	INVESTMENT (TCI)	* * *
I OTAL CAPITAL	III V ESTIVIENT (TCI)	3,518,199

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	96,750 96,750
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83 Annualized Cost Factor	0.25
	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,513
Catalyst Replacement Cost	19,943
Electricity Cost	0.3
Subtotal - Utilities	24,457
TOTAL ANNUAL DIRECT COSTS*	121,208

COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M COSTS			121,208
Annualized Cost Factor			
I	Equipment Life (years) =	10	
Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
CAPITAL RECOVERY COSTS			
TOTAL CAPITAL REQUIREMENT			3,518,199
TOTAL ANNUAL CAPITAL REQUIRE	EMENT		891,828
TOTAL ANNUALIZED COST			1,013,036
(Total annual O&M cost and annualized capital cost)			,,

## **Heater Firing Rate Increase Plan Approval**

#### **NOx BAT Control Cost Effectiveness**

Source	Unit 866-12H1	
Control	SCR	
Rated Heat Input	61.2	MMBtu/hr
Rated Heat Input	456,000	MMBtu/yr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	25.8	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	85%	
Heater Capacity	64.6	GJ/hr
<b>Burner Heat Release Rate</b>	13.8	GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,897,832
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	2,897,832
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (T	DC)	2,897,832
INDIRECT INSTALLATION	COSTS	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	86,935
TOTAL INDIRECT COSTS,	IC	86,935
TOTAL CAPITAL IN	IVESTMENT (TCI)	2,984,767

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	82,081 82,081
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,513
Catalyst Replacement Cost	19,943
Electricity Cost	0.3
Subtotal - Utilities	24,457
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	106,538

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M C	OSTS			106,538
Annualized Cost Factor				
	Equipmer	nt Life (years) =	10	
		rest Rate (%) =	21.83	
	Annualized Cost Factor			0.25
CAPITAL RECOVERY COS	TS			
	TOTAL CAPITAL REQUIREMENT			2,984,767
	TOTAL ANNUAL CAPITAL REQUIREMENT			756,608
TOTAL ANNUALIZED CO				863,147

## **Heater Firing Rate Increase Plan Approval**

#### **NOx BAT Control Cost Effectiveness**

Source	Unit 866-12H1	
Control	ULNB	
Rated Heat Input	61.2	MMBtu/hr
Rated Heat Input	456,000	MMBtu/yr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	25.8	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
<b>Control Efficiency</b>	73%	
<b>Heater Capacity</b>	64.6	GJ/hr
<b>Burner Heat Release Rate</b>	13.8	GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	361,404
	Instrumentation (10% of EC)	36,140
	Sales taxes (5% of EC)	18,070
	Freight (8% of EC)	28,912
	Subtotal - Purchased Equipment Costs (PEC)	444,527
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (2	TDC)	444,527
INDIRECT INSTALLATIO	N COSTS	
	Engineering Costs (5% of PEC)	22,226
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	44,453
	Start-up (1% of PEC)	4,445
	Performance Test (1% of PEC)	4,445
	Contingency (3% of PEC)	13,336
TOTAL INDIRECT COSTS	S, IC	88,905
TOTAL CAPITAL I	NVESTMENT (TCI)	533,432

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	14,669 14,669
Annualized Cost Factor  Replacement Life (years) = 10 Interest Rate (%) = 21.83 Annualized Cost Factor	0.25
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities None	
Subtotal - Utilities	0.0
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	14,669

	COST COMPONENT:		COST (\$)
TOTAL ANNUAL O&M C	POSTS		14,669
Annualized Cost Factor	Equipment Life (years) =  Interest Rate (%) =  Annualized Cost Factor	10 21.83	
CAPITAL RECOVERY COS	STS TOTAL CAPITAL REQUIREMENT		533,432
	TOTAL ANNUAL CAPITAL REQUIREMENT		135,220
TOTAL ANNUALIZED CO	OST nd annualized capital cost)		149,889

Burner Heat Release Rate 13.8

Source Unit 866-12H1 LNB & SNCR Control

MMBtu/hr Rated Heat Input 61.2 456,000 **Rated Heat Input** MMBtu/yr Number of Burners 6.0 Burners tpy lb/MMBtu Baseline Actual Emissions 25.8 **Current Emission Rate** 0.113 Control Efficiency 70% GJ/hr **Heater Capacity** 64.6

Evaluated at New Firing Limit at 2012 Cost and Efficiencies
Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034

GJ/hr

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	188,440
	Instrumentation (10% of EC)	18,844
	Sales taxes (5% of EC)	9,422
	Freight (8% of EC)	15,075
	Subtotal - Purchased Equipment Costs (PEC)	231,781
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TI	OC) - LNB	231,781
INDIRECT INSTALLATION	COSTS - LNB	
	Engineering Costs (5% of PEC)	11,589
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	23,178
	Start-up (1% of PEC)	2,318
	Performance Test (1% of PEC)	2,318
	Contingency (3% of PEC)	6,953
TOTAL INDIRECT COSTS,	IC - LNB	46,356
DIRECT COSTS - SNCR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	544,494
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	= = =
	Subtotal - Purchased Equipment Costs (PEC)	544,494
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TI	OC) - SNCR	544,494
NDIRECT INSTALLATION		
	Engineering Costs (5% of PEC)	===
	Construct. & Field Expenses (Included in above costs) Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	16,335
TOTAL INDIRECT COSTS,	IC - SNCR	16,335
	IVESTMENT (TCI) - LNB	278,137
	IVESTMENT (TCI) - SNCR	560,828
FOTAL CAPITAL IN	VESTMENT (TCI)	838,966

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	23,072
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,513
Electricity Cost	0.3
Subtotal - Utilities	4,514
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	27,585

	COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M C	OSTS			27,585
Annualized Cost Factor				
	Eq	uipment Life (years) =	10	
		Interest Rate (%) =	21.83	
	Annualized Cost Factor			0.25
CAPITAL RECOVERY CO.	STS			
	TOTAL CAPITAL REQUIREMENT			838,966
	TOTAL ANNUAL CAPITAL REQUIRE	MENT		212,669
TOTAL ANNUALIZED C (Total annual O&M cost a	OST nd annualized capital cost)			240,255

Burner Heat Release Rate 13.8

Source Unit 866-12H1 LNB & FGR Control MMBtu/hr Rated Heat Input 61.2 456,000 MMBtu/yr Rated Heat Input Number of Burners 6.0 Burners tpy lb/MMBtu Baseline Actual Emissions 25.8 Current Emission Rate 0.113 Control Efficiency 55% GJ/hr **Heater Capacity** 64.6

Evaluated at New Firing Limit at 2012 Cost and Efficiencies
Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034

GJ/hr

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	188,440
	Instrumentation (10% of EC)	18,844
	Sales taxes (5% of EC)	9,422
	Freight (8% of EC)	15,075
	Subtotal - Purchased Equipment Costs (PEC)	231,781
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC) - LNB	231,781
INDIRECT INSTALLATIO		
	Engineering Costs (5% of PEC)	11,589
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	23,178
	Start-up (1% of PEC)	2,318
	Performance Test (1% of PEC)	2,318
	Contingency (3% of PEC)	6,953
TOTAL INDIRECT COSTS	S, IC - LNB	46,356
DIRECT COSTS - FGR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	218,823
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	218,823
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc. Site Preparation / Buildings- Included above	0
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC) - FGR	218,823
INDIRECT INSTALLATIO	ON COSTS - FGR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC) Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	6,565
TOTAL INDIRECT COST	S, IC - FGR	6,565
	NVESTMENT (TCI) - LNB	278,137
	NVESTMENT (TCI) - FGR	225,388
TOTAL CAPITAL I	INVESTMENT (TCI)	503,525

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	13,847 13,847
Annualized Cost Factor Replacement L Interest Annualized Cost Factor	Life (years) = 10 t Rate (%) = 21.83
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities Electricity Cost	7,781
Subtotal - Utilities	7,781
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	21,628

	COST COMPONENT:				
TOTAL ANNUAL O&M	COSTS			21,628	
Annualized Cost Factor	Ec	quipment Life (years) = Interest Rate (%) =	10 21.83	0.25	
CAPITAL RECOVERY CO	APITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT				
	TOTAL ANNUAL CAPITAL REQUIRE.	MENT		127,639	
	OTAL ANNUALIZED COST otal annual O&M cost and annualized capital cost)				

**Heater Firing Rate Increase Plan Approval** 

### **NOx BAT Control Cost Effectiveness**

Source	Unit 866-12H1	
Control	SNCR	
Rated Heat Input	61.2	MMBtu/hr
Rated Heat Input	456,000	MMBtu/yr
Number of Burners	6.0	Burners
<b>Baseline Actual Emissions</b>	25.8	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	40%	
Heater Capacity	64.6	GJ/hr
Burner Heat Release Rate	13.8	GJ/hr

## **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
Ì	Equipment Cost (EC)	544,494
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	544,494
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC)	544,494
INDIRECT INSTALLATIO	ON COSTS	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	16,335
TOTAL INDIRECT COST	S, IC	16,335
TOTAL CADITAL I	NVESTMENT (TCI)	560.828

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	15,423 15,423
Annualized Cost Factor $ \text{Replacement Life (years)} = 10 \\ \text{Interest Rate (\%)} = 21.83 \\ \text{Annualized Cost Factor} $	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities Ammonia Cost Electricity Cost	4,513 0.3
Subtotal - Utilities	4,514
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	19,936

COST COMPONENT:	COST (\$)	
TOTAL ANNUAL O&M COSTS	19,936	
	Life (years) = 10 t Rate (%) = 21.83	
CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT  TOTAL ANNUAL CAPITAL REQUIREMENT	560,828 142,164	
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)	162,101	

## PES Refinery Heater Firing Rate Increase Plan Approval Unit 868-8H101 BAT Cost Effectiveness Summary

	A	В	C	D	E	F	G	H	I	J
Control Option	New Firing (MMBtu/yr)	Current Emission Rate (lb/MMBtu) <sup>1</sup>	Potential Emissions (TPY)	Control Efficiency (%)	Maximum Post Control Emissions @ New Firing (TPY)	Potential NO <sub>x</sub> Reduced (TPY)	2012 Total Capital Cost (\$)	2012 O&M Cost (\$)	2012 Annualized  Cost <sup>2</sup> (\$)	2012 Cost Effectiveness (\$/Ton)
ULNB & SCR	480,000	0.113	27.1	96%	1.1	26.0	3,472,395	119,468	999,686	38,390
SCR	480,000	0.113	27.1	85%	4.1	23.1	2,949,422	105,087	852,736	36,992
ULNB	480,000	0.113	27.1	73%	7.2	19.9	522,973	14,382	146,950	7,377
LNB & SNCR	480,000	0.113	27.1	70%	8.1	19.0	1,057,946	33,519	301,697	15,892
LNB & FGR	480,000	0.113	27.1	55%	12.2	14.9	726,468	27,607	211,759	14,197
SNCR	480,000	0.113	27.1	40%	16.3	10.8	554,204	19,666	160,151	14,763
	Calculation	•	= A * B / 2000		= C * (1 - D)	= C - E			= (G * ACF) + H	= I / F

#### Notes:

 $<sup>^1</sup>$  Unit 868-8H101 is projected to be above PADEP presumptive RACT firing limits and assumed NO  $_{\rm x}$  emission rate limit of 0.113 lb/MMBtu is used.

<sup>&</sup>lt;sup>2</sup> See "BAT Cost Summary" tab for details on the Annualized Cost Factor (ACF).

Source Unit 868-8H101
Control ULNB & SCR
Rated Heat Input 60.0
Rated Heat Input 480,000

 Rated Heat Input
 60.0
 MMBtu/hr

 Rated Heat Input
 480,000
 MMBtu/yr

 Number of Burners
 4.0
 Burners

 Baseline Actual Emissions
 27.1
 tpy

 Current Emission Rate
 0.113
 lb/MBtu

Control Efficiency 96%

Heater Capacity 63.3 GJ/hr Burner Heat Release Rate 20.3 GJ/hr

#### Evaluated at New Firing Limit at 2012 Cost and Efficiencies

	COST COMPONENT:	COST (\$)
DIRECT COSTS - ULN	В	
	Purchased Equipment Costs	
	Equipment Cost (EC)	354,317
	Instrumentation (10% of EC)	35,432
	Sales taxes (5% of EC)	17,716
	Freight (8% of EC)	28,345
	Subtotal - Purchased Equipment Costs (PEC)	435,810
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	S (TDC) - ULNB	435,810
INDIRECT INSTALLAT	TION COSTS - ULNB	
	Engineering Costs (5% of PEC)	21,791
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	43,581
	Start-up (1% of PEC)	4,358
	Performance Test (1% of PEC)	4,358
	Contingency (3% of PEC)	13,074
TOTAL INDIRECT CO	STS, IC	87,162
DIRECT COSTS - SCR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,863,517
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	2,863,517
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above  Subtotal - Direct Installation Costs	
	Subtotal - Direct Installation Costs	U
TOTAL DIRECT COST	S (TDC) - SCR	2,863,517
INDIRECT INSTALLAT	TION COSTS - SCR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	85,906
TOTAL INDIRECT CO	STS, IC - SCR	85,906
TOTAL CAPITAI	INVESTMENT (TCI) - ULNB	522,973
	INVESTMENT (TCI) - SCR	2,949,422
	LINVESTMENT (TCI)	3,472,395
OTAL CALITAL	INVESTMENT (ICI)	3,472,393

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	95,491 95,491
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = $21.83$	3
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,425
Catalyst Replacement Cost	19,552
Electricity Cost	0.3
Subtotal - Utilities	23,978
TOTAL ANNUAL DIRECT COSTS*	119,468

COST COMPONENT:			COST (\$)	
TOTAL ANNUAL O&M	COSTS			119,468
Annualized Cost Factor			10	
	Ec	quipment Life (years) = Interest Rate (%) =	10 21.83	
	Annualized Cost Factor	interest Rate (%) =	21.63	0.25
CAPITAL RECOVERY CO	STS			
	TOTAL CAPITAL REQUIREMENT			3,472,395
	TOTAL ANNUAL CAPITAL REQUIREM	MENT		880,217
TOTAL ANNUALIZED ( (Total annual O&M cost o	OST nd annualized capital cost)			999,686

## **Heater Firing Rate Increase Plan Approval**

#### **NOx BAT Control Cost Effectiveness**

Source	Unit 868-8H101	
Control	SCR	
Rated Heat Input	60.0	MMBtu/hr
Rated Heat Input	480,000	MMBtu/yr
<b>Number of Burners</b>	4.0	Burners
<b>Baseline Actual Emissions</b>	27.1	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	85%	
<b>Heater Capacity</b>	63.3	GJ/hr
<b>Burner Heat Release Rate</b>	20.3	GJ/hr

#### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	2,863,517
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	2,863,517
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (T	TDC)	2,863,517
INDIRECT INSTALLATION	N COSTS	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	85,906
TOTAL INDIRECT COSTS	, IC	85,906
TOTAL CAPITAL II	NVESTMENT (TCI)	2,949,422

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS	
Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	81,109 81,109
Annualized Cost Factor	
Replacement Life (years) = 10 Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,425
Catalyst Replacement Cost	19,552
Electricity Cost	0.3
Subtotal - Utilities	23,978
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	105,087

COST COMPONENT:			COST (\$)
TOTAL ANNUAL O&M COS	STS		105,087
Annualized Cost Factor			
	Equipment Life (years) =	10	
	Interest Rate (%) =	21.83	
	Annualized Cost Factor		0.25
CAPITAL RECOVERY COSTS	S		
	TOTAL CAPITAL REQUIREMENT		2,949,422
	TOTAL ANNUAL CAPITAL REQUIREMENT		747,649
TOTAL ANNUALIZED COS (Total annual O&M cost and			852,736

## **Heater Firing Rate Increase Plan Approval**

### **NOx BAT Control Cost Effectiveness**

Source	Unit 868-8H101	
Control	ULNB	
Rated Heat Input	60.0	MMBtu/hr
Rated Heat Input	480,000	MMBtu/yr
<b>Number of Burners</b>	4.0	Burners
<b>Baseline Actual Emissions</b>	27.1	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
<b>Control Efficiency</b>	73%	
<b>Heater Capacity</b>	63.3	GJ/hr
<b>Burner Heat Release Rate</b>	20.3	GJ/hr

### **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	354,317
	Instrumentation (10% of EC)	35,432
	Sales taxes (5% of EC)	17,716
	Freight (8% of EC)	28,345
	Subtotal - Purchased Equipment Costs (PEC)	435,810
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS	(TDC)	435,810
INDIRECT INSTALLATION	ON COSTS	
	Engineering Costs (5% of PEC)	21,791
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	43,581
	Start-up (1% of PEC)	4,358
	Performance Test (1% of PEC)	4,358
	Contingency (3% of PEC)	13,074
TOTAL INDIRECT COST	TS, IC	87,162
TOTAL CAPITAL	INVESTMENT (TCI)	522,973

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	14,382 14,382
Annualized Cost Factor  Replacement Life (years) = 10 Interest Rate (%) = 21.83 Annualized Cost Factor	0.25
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities None	
Subtotal - Utilities	0.0
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	14,382

	COST COMPONENT:		COST (\$)
TOTAL ANNUAL O&M CO	STS		14,382
Annualized Cost Factor			
	Equipment Life (years) =	10	
	Interest Rate (%) =	21.83	
	Annualized Cost Factor		0.25
CAPITAL RECOVERY COST	S		
	TOTAL CAPITAL REQUIREMENT		522,973
	TOTAL ANNUAL CAPITAL REQUIREMENT		132,568
TOTAL ANNUALIZED COS (Total annual O&M cost and			146,950

Source Unit 868-8H101 LNB & SNCR Control Rated Heat Input 60.0 480,000 Rated Heat Input

MMBtu/yr Number of Burners 4.0 Burners tpy lb/MMBtu Baseline Actual Emissions 27.1 Current Emission Rate 0.113 Control Efficiency 70% GJ/hr **Heater Capacity** 63.3 Burner Heat Release Rate 20.3 GJ/hr

Evaluated at New Firing Limit at 2012 Cost and Efficiencies
Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034

MMBtu/hr

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	341,289
	Instrumentation (10% of EC)	34,129
	Sales taxes (5% of EC)	17.064
	Freight (8% of EC)	27,303
	Subtotal - Purchased Equipment Costs (PEC)	419,785
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	<u> </u>
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC) - LNB	419,785
INDIRECT INSTALLATIO	N COSTS - LNB	
	Engineering Costs (5% of PEC)	20,989
	Construct. & Field Expenses (Included in above costs)	= = =
	Contractor Fees (10% of PEC)	41,979
	Start-up (1% of PEC)	4,198
	Performance Test (1% of PEC)	4,198
	Contingency (3% of PEC)	12,594
TOTAL INDIRECT COSTS	S, IC - LNB	83,957
DIRECT COSTS - SNCR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	538,062
	Instrumentation (10% of EC)	<del>-</del> <del>-</del> <del>-</del> <del>-</del>
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	538,062
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping; etc.	0
	Site Preparation / Buildings- Included above	0
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC) - SNCR	538,062
INDIRECT INSTALLATIO	N COSTS - SNCR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	= = =
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC) Contingency (3% of PEC)	16,142
TOTAL INDIRECT COSTS		16,142
	NVESTMENT (TCI) - LNB	503,742
TOTAL CAPITAL I		554,204

COST COMPONENT:			COST (\$)
ANNUAL DIRECT COSTS			
Operation and Maintenance Labor			
Maintenance Labor and Material (2.75%	of TCI)		29,094
			29,094
Annualized Cost Factor			
	lacement Life (years) =	10	
10)	Interest Rate (%) =	21.83	
Annualized Cost Factor			0.25
Replacement cost			
Subtotal - Operation and Maintenance Labor			
Utilities			
Ammonia Cost			4,425
Electricity Cost			0.3
Subtotal - Utilities			4,425
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>			33,519

COST COMPONENT:		COST (\$)
TOTAL ANNUAL O&M COST	rs	33,519
Annualized Cost Factor	Equipment Life (years) = 10	
Ar	Interest Rate (%) = 21.83	
CAPITAL RECOVERY COSTS		
To	OTAL CAPITAL REQUIREMENT	1,057,946
Te	OTAL ANNUAL CAPITAL REQUIREMENT	268,179
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)		301,697

Source Unit 868-8H101 LNB & FGR Control MMBtu/hr Rated Heat Input 60.0 Rated Heat Input 480,000 MMBtu/yr Number of Burners 4.0 Burners tpy lb/MMBtu Baseline Actual Emissions 27.1 Current Emission Rate 0.113 Control Efficiency 55% GJ/hr **Heater Capacity** 63.3 Burner Heat Release Rate 20.3 GJ/hr

Evaluated at New Firing Limit at 2012 Cost and Efficiencies
Costs derived from Alternative Control Techniques Document - NOx Emissions from Process Heaters (Revised) - EPA-453/R-93-034

	COST COMPONENT:	COST (\$)
DIRECT COSTS - LNB		
	Purchased Equipment Costs	
	Equipment Cost (EC)	341,289
	Instrumentation (10% of EC)	34,129
	Sales taxes (5% of EC)	17,064
	Freight (8% of EC)	27,303
	Subtotal - Purchased Equipment Costs (PEC)	419,785
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping; etc.	0
		0
	Site Preparation / Buildings- Included above  Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (	TDC) - LNB	419,785
		127,100
INDIRECT INSTALLATIO		*****
	Engineering Costs (5% of PEC)	20,989
	Construct. & Field Expenses (Included in above costs)	===
	Contractor Fees (10% of PEC)	41,979
	Start-up (1% of PEC)	4,198
	Performance Test (1% of PEC)	4,198
	Contingency (3% of PEC)	12,594
TOTAL INDIRECT COST	S, IC - LNB	83,957
DIRECT COSTS - FGR		
	Purchased Equipment Costs	
	Equipment Cost (EC)	216,239
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	216,239
	Direct Installation Costs (Based on Vendor Discussion)	
	Foundations & supports; handling & erection; electrical; piping;	_
	etc. Site Preparation / Buildings- Included above	0
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COSTS (TDC) - FGR		216,239
INDIRECT INSTALLATIO	ON COSTS - FGR	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC) Contingency (3% of PEC)	6,487
TOTAL INDIRECT COST		6,487
TOTAL CAPITAL	INVESTMENT (TCI) - LNB	503,742
	INVESTMENT (TCI) - FGR	222,726
	INVESTMENT (TCI)	726,468

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS  Operation and Maintenance Labor  Maintenance Labor and Material (2.75% of TCI)	19,978 19,978
Annualized Cost Factor  Replacement Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	
Replacement cost  Subtotal - Operation and Maintenance Labor	
Utilities Electricity Cost	7,629
Subtotal - Utilities	7,629
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	27,607

COST COMPONENT:		COST (\$)		
TOTAL ANNUAL O&M	COSTS			27,607
Annualized Cost Factor	Ec	quipment Life (years) =	10	
	Annualized Cost Factor	Interest Rate (%) =	21.83	0.25
CAPITAL RECOVERY CO	CAPITAL RECOVERY COSTS			
	TOTAL CAPITAL REQUIREMENT			726,468
	TOTAL ANNUAL CAPITAL REQUIRE	MENT		184,152
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)		211,759		

**Heater Firing Rate Increase Plan Approval** 

#### **NOx BAT Control Cost Effectiveness**

Source	Unit 868-8H101	
Control	SNCR	
Rated Heat Input	60.0	MMBtu/hr
Rated Heat Input	480,000	MMBtu/yr
Number of Burners	4.0	Burners
<b>Baseline Actual Emissions</b>	27.1	tpy
<b>Current Emission Rate</b>	0.113	lb/MMBtu
Control Efficiency	40%	
Heater Capacity	63.3	GJ/hr
Burner Heat Release Rate	20.3	GJ/hr

# **Evaluated at New Firing Limit at 2012 Cost and Efficiencies**

	COST COMPONENT:	COST (\$)
DIRECT COSTS		
	Purchased Equipment Costs	
	Equipment Cost (EC)	538,062
	Instrumentation (10% of EC)	
	Sales taxes (5% of EC)	
	Freight (8% of EC)	
	Subtotal - Purchased Equipment Costs (PEC)	538,062
	Direct Installation Costs (Based on Vendor Discussion) Foundations & supports; handling & erection; electrical; piping;	
	etc.	0
	Site Preparation / Buildings- Included above	
	Subtotal - Direct Installation Costs	0
TOTAL DIRECT COST	TS (TDC)	538,062
INDIRECT INSTALLA	TION COSTS	
	Engineering Costs (5% of PEC)	
	Construct. & Field Expenses (Included in above costs)	
	Contractor Fees (10% of PEC)	
	Start-up (1% of PEC)	
	Performance Test (1% of PEC)	
	Contingency (3% of PEC)	16,142
TOTAL INDIRECT CO	OSTS, IC	16,142
TOTAL CAPITA	L INVESTMENT (TCI)	554,204

COST COMPONENT:	COST (\$)
ANNUAL DIRECT COSTS Operation and Maintenance Labor	
Maintenance Labor and Material (2.75% of TCI)	15,241
Manitenance Labor and Material (2.75% of 1C1)	15,241
Annualized Cost Factor	
Replacement Life (years) = 10	
Interest Rate (%) = 21.83	
Annualized Cost Factor	0.25
Replacement cost	
Subtotal - Operation and Maintenance Labor	
Utilities	
Ammonia Cost	4,425
Electricity Cost	0.3
Subtotal - Utilities	4,425
TOTAL ANNUAL DIRECT COSTS <sup>a</sup>	19,666

COST COMPONENT:	COST (\$)
TOTAL ANNUAL O&M COSTS	19,666
Annualized Cost Factor  Equipment Life (years) = 10  Interest Rate (%) = 21.83  Annualized Cost Factor	
CAPITAL RECOVERY COSTS  TOTAL CAPITAL REQUIREMENT	554,204
TOTAL ANNUAL CAPITAL REQUIREMENT	140,485
TOTAL ANNUALIZED COST (Total annual O&M cost and annualized capital cost)	160,151